

## South Dakota Decennial Interstate Corridor Study

PHASEONE REPORT



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FELSBURG HOLT \& ULLEVIG

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# SOUTH DAKOTA DOT <br> DECENNIAL INTERSTATE CORRIDOR STUDY 

## Phase 1 Report

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## EXECUTIVE SUMMARY

## Introduction

The South Dakota Department of Transportation (SDDOT) retained Felsburg Holt \& Ullevig to conduct an analysis of the Interstate system. The study is focused on:

- Ensuring a mainline Level of Service (LOS) of C or better throughout the Interstate System,
- Ensuring an interchange LOS of D or better for all interchanges throughout the Interstate System, and
- Identification of areas not in compliance with current Interstate design standards.

The study will be conducted in three phases. This report documents Phase 1, which is an assessment of the entire Interstate System looking at geometry, safety and traffic operations. Phase 1 will identify a combination of 15 existing and future interchange locations to be analyzed further in Phase 2. Phase 2 will include the development of detailed geometric layouts of these interchanges, and a review of the projected traffic operations associated with the interchange design. Phase 3 will provide a prioritized plan for implementing the improvements. Figure S-1 illustrates the progression of 3 phases.

Phase 1


Figure S-1 Phased Study Overview

Figure S-2 depicts the Phase 1 contents detailed in this report. The Phase 1 evaluation includes all 678 centerline miles of Interstate mainline in South Dakota and 126 of the 152 total existing interchanges. A statewide inventory was performed to document geometric conditions, traffic safety and Average Daily Traffic (ADT) forecasts. This inventory led to the identification of a shortened list of deficient interchanges, structures and interstate segments. A detailed review of collision patterns and completion of Level of Service (LOS) analyses revealed a need for improvements at 32 interchanges, widening of 6 miles of Interstate triggered by traffic growth and replacement of 99 Structurally deficient or Functionally obsolete Interstate system bridges. The project team developed improvement concepts for the interchanges and provided preliminary cost estimates for interchange improvements, mainline widening and structure replacements.


Figure S-2 Phase 1 Flow Diagram


## Phase 1 Findings

## Geometric

The existing geometric features of the interstate mainline throughout the state and the 126 selected interchanges were reviewed to determine if they meet current design criteria. These design features included such items as the travel lane width, shoulder widths, design speed, degree of curve, clear zone, inslope, superelevation, bridge width, vertical clearance, vertical curves and grades. At the interchanges, the analysis also included cross road features such as stopping sight distance, ramp intersection sight distance and access control. Desirable values for these roadway elements were based on the South Dakota Department of Transportation Roadway Design Manual and A Policy on Geometric Design of Highways and Streets, published by AASHTO.

## Mainline

The interstate mainline segments along I-90, I-190, I-29 and I-229 identified above were reviewed using information available on the as-built plans from when the interstate was originally constructed, reconstructed or otherwise improved.


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Tables summarizing the mainline geometric analysis are included in the Appendix. This review of existing geometric features on the mainline indicated that the most common substandard geometric element based on new construction standards along the interstate is the inslope. Another common finding is having a clear zone less than the desirable 30'. The longitudinal grade along interstate segments was reviewed and determined to have minimal consequence to the interstate system. Therefore, the longitudinal grade is not reported in this study.

The deficiencies identified typically do not warrant immediate correction, but should be reviewed at the time of pavement replacement or other major improvement projects on the interstate mainline.

## Interchanges

The review of existing geometrics for the 126 interchanges selected for this Phase 1 analysis was conducted through a combination of measurements taken in the field, site observations and a review of the design plans provided by SDDOT. This evaluation process identified several design elements that do not meet current design criteria. The most common substandard geometric element was associated with the width provided for the ramp right shoulder. Ramp inslopes were also found to be substandard. These deficiencies do not warrant immediate correction, and can be reviewed at the time of pavement replacement along the ramps. The design features that do not meet the desirable design criteria are summarized in the tables provided in the Appendix along with detailed geometric checklists for selected interchanges. Additional discussion about the geometric deficiencies at specific interchanges is provided for those interchanges where safety issues have been identified through the crash analysis or concepts have been developed to address operations.

## Structural Conditions

Several bridges along and crossing the Interstate System are currently classified as structurally deficient or functionally obsolete according to their National Bridge Inspection Standards (NBIS) rating.. A statement of probable costs was prepared for the removal and reconstruction of these bridges along the study corridors. Structurally deficient bridges are assigned a high priority for reconstruction. Functionally obsolete bridges that demonstrate deficient vertical clearance should be considered a higher priority than correcting inadequate bridge widths when there is no crash history related to the inadequate width. A total of 95 structures ( 93 bridges, 2 tunnels) were identified in this analysis, with a total construction cost estimate of $\$ 80.7$ Million. More detailed information regarding the location and size of each structure are provided in the Appendix.

## Safety

A shortened list of 19 interchanges was designated as high crash locations based on their 3year crash history relative to the other interchanges. The 19 locations include the highest 10 crash rate interchanges and additional locations that experienced more than double the average crash rate. Table S-1 lists these 19 locations.

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Table S-1 19 High Crash Interchange Locations

| Interchange | Number of Crashes by Severity July 2006 to July 2009 |  |  |  | Crash Rate 3-Year (Wtd. Acc/MEV) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal | Injury | PDO | Total |  |
| I-29 Exit 1 | 0 | 5 | 23 | 28 | 0.92 |
| I-29 Exit 77 | 0 | 71 | 103 | 174 | 3.72 |
| I-29 Exit 132 | 1 | 3 | 23 | 27 | 1.45 |
| I-29 Exit 201 | 1 | 4 | 6 | 11 | 4.22 |
| I-90 Exit 12 | 0 | 4 | 24 | 28 | 1.48 |
| I-90 Exit 23 | 0 | 5 | 23 | 28 | 2.36 |
| I-90 Exit 30 | 0 | 12 | 28 | 40 | 2.34 |
| I-90 Exit 40 | 1 | 8 | 23 | 32 | 3.40 |
| I-90 Exit 55 | 1 | 12 | 18 | 31 | 1.39 |
| I-90 Exit 59 | 0 | 31 | 54 | 85 | 2.49 |
| I-90 Exit 172 | 1 | 0 | 4 | 5 | 2.47 |
| I-90 Exit 235 | 1 | 2 | 2 | 5 | 2.45 |
| I-90 Exit 332 | 0 | 11 | 32 | 43 | 2.15 |
| I-90 Exit 390 | 0 | 5 | 24 | 29 | 2.36 |
| I-229 Exit 2 | 0 | 21 | 42 | 63 | 2.03 |
| I-229 Exit 3 | 0 | 25 | 53 | 78 | 1.64 |
| I-229 Exit 4 | 0 | 23 | 49 | 72 | 2.02 |
| I-229 Exit 5 | 0 | 35 | 68 | 103 | 3.25 |
| I-229 Exit 7 | 0 | 10 | 36 | 46 | 1.21 |
| Statewide Average Interchange | 0.11 | 3.57 | 9.68 | 13.36 | 0.94 |

Additional data were gathered to further evaluate these locations, resulting in a refined assessment of actual collision patterns and problems at each interchange. Most of the interchanges demonstrated no identifiable collision pattern, but several of the urban interchanges showed elevated numbers of rear end and approach turn collisions.

## Traffic Forecasts / Operations

## Mainline

Year 2008 mainline daily traffic counts conducted were available in the 2009 Highway Needs and Project Analysis Report (SDDOT, 2009), also known as the Needs Book. The counts provide average annual daily traffic volume (AADT) levels throughout the interstate system, including I-90, I-190, I-29 and I-229. The SDDOT supplied the project team with 20-year growth factors for urban and rural portions of each County in South Dakota. These growth factors, used to develop future mainline Interstate traffic forecasts, varied from 16 percent ( 0.7 percent per year) to 62 percent ( 2.6 percent per year) growth. Year 2030 forecasts for I-29 and I-229 in the Sioux Falls area reach 70,000-80,000 vpd. The Appendix provides a summary of all interstate segments with growth rates and AADT forecasts.


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Mainline Level of Service (LOS) analyses of current and future conditions were performed based on averaged traffic parameters. It was found that most mainline sections would operate acceptably (LOS C or better) through the Year 2030. Several mainline sections of I-29 and I-229 within Sioux Falls demonstrate a need for future widening.

## Interchange

Middle crossroad traffic counts conducted between the Year 2001 and 2007 at each study interchange were provided by SDDOT. Forecasts were developed using localized interchange growth rates gathered from a variety of sources. There are 4 quasi-government agencies that include counties through which interstates pass and three Metropolitan Planning Organizations (MPOs). These agencies provided travel demand model information, population growth and land use forecasts. Population growth between the Year 2000 and 2008 is documented by County in the most recent U.S. Census (www.census.gov). This information was used to develop traffic forecasts for the more rural Interstate sections.

To focus study resources on potential operational problem areas throughout the State, the project team screened out the lower-traffic volume interchanges to reach a list of interchanges where conditions could reach substandard Levels of Service (LOS) currently or in the future. For the purposes of this study, substandard interchange operations occur when and where the ramp terminal intersection LOS reaches LOS D or worse and/or freeway and ramp operations reach LOS C or worse. Based on results from the 2000 Interstate Corridor Study and discussion with the Study Advisory Team, interchanges where the daily crossroad traffic volume between the ramp termini ("middle ADT") exceeds 5,000 Vehicles Per Day (vpd) were designated as candidates for operational evaluation.

Operational analyses were performed for both AM and PM peak hour traffic conditions for each of the 34 candidate interchanges, with the exception of a few where only design hour information was available. Ten of the thirty-four interchanges demonstrated satisfactory operations through the Year 2030, while the majority required improvements to operate acceptably in the future. Improvements have been identified in the form of additional turn lanes, traffic control changes or modified acceleration/deceleration lanes at ramp junctions. Options for interchange reconstruction were also evaluated.

## Improvement Concepts

Upon considering geometric, safety and operational deficiencies, a total of 32 interchanges and approximately 6 miles of mainline interstate were identified as locations where improvements would be needed to meet the goals identified in this Study:

- Ensuring a mainline Level of Service (LOS) of C or better throughout the Interstate System,
- Ensuring an interchange LOS of D or better for all interchanges throughout the Interstate System, and
- Identification of areas not in compliance with current Interstate design standards.



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A statement of probable construction costs was developed for each interchange improvement identified in Phase 1 as well as freeway widening projects. Tables S-2 through S-4 summarizes those probable construction costs by SDDOT Region. The costs shown are based on conceptual design for budgetary purposes. The cost estimate calculations are provided in the Appendix.

Table S-2 Rapid City Region - Summary of Probable Construction Costs

| Interchange |  | Proposed Improvement |
| :--- | :--- | :---: |
| Probable Construction Cost |  |  |
| Interstate 90 |  | Add turn lane - widen bridge |
| Exit 12 | Signalize north intersection | $\$ 50,000$ |
|  | Diamond | $\$ 125,000$ |
|  | Single-Point | $\$ 4.6$ Million |
| Exit 30 | Realign mainline I-90 | $\$ 18.6$ Million |
| Exit 46 | Reconstructed Diamond | $\$ 19.8$ Million |
| Exit 48 | Single-Point | $\$ 8.7$ Million |
|  | Relocated Diamond | $\$ 12.0$ Million |
| Exit 55 | Bridge widening | $\$ 8.1$ Million |
| Exit 59 | Diamond | $\$ 4.2$ Million |
|  | Single-Point | $\$ 7.2$ Million |
| Exit 63 | Diamond | $\$ 14.5$ Million |
|  | Flyover | $\$ 8.7$ Million |
| Interstate 190 |  |  |
| Exit 1 | 2-lane roundabout | $\$ 13.2$ Million |
|  | 1-lane roundabout | $\$ 3.2$ Million |
|  | Signal | $\$ 1.3$ Million |

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## Table S-3 Mitchell Region - Summary of Probable Construction Costs

| Interchange | Proposed Improvement | Probable Construction Cost |
| :---: | :---: | :---: |
| Interstate 29 |  |  |
| I-29 Widening | Additional travel lane in each direction: Exit 75-77 and Exit 78-79 | \$56 Million ${ }^{1}$ |
| Exit 1 | Add turn lane \& Signals | \$410,000 |
| Exit 2 | Signal/relocate Fr. Rd. | \$860,000 |
|  | Roundabout/relocate Fr. Rd. | \$700,000 |
| Exit 26 | Reconstruct NB Ramps/signal | \$1.3 Million |
| Exit 47 | Add turn lanes \& Signals | \$470,000 |
|  | Add roundabouts | \$560,000 |
| Exit 77 | Single-Point | \$9.9 Million |
|  | Diverging Diamond/exist bridge | \$2.5 Million |
|  | Diverging Diamond w/new bridge | \$11.5 Million |
| Interstate 90 |  |  |
| Exit 330 | Add turn lanes \& Signals | \$470,000 |
| Exit 406 | Reconstruct Crossroad/add Signals | \$5.9 Million |
|  | Single-Point | \$9.3 Million |
| Interstate 229 |  |  |
| I-229 Freeway Widening | Additional travel lane in each direction: I-29 to Exit 5, two more lanes Exit 5 to Exit 6 | \$72 Million ${ }^{1}$ |
| Exit 2 | Add turn lane \& re-stripe | \$60,000 |
|  | Single-Point | \$12.6 Million |
| Exit 4 | Add turn lanes | \$240,000 |
| Exit 5 | Offset Single-Point | \$8.8 Million |
| Exit 7 | Crossroad \& Ramp Improvement/add Signal | \$1.2 Million |
| Exit 9 | Add turn lanes \& Signal | \$350,000 |

Assumed conceptual estimated cost of Interstate widening is $\$ 4$ Million per mile per lane. This assumption is based on cost estimates developed for freeway widening projects in the 2004 Interstate 90 Black Hawk - Sturgis Corridor Preservation Study (Felsburg Holt \& Ullevig). Estimated costs did not include Right-of-way. Actual costs would vary widely based on local conditions.

Table S-4 Aberdeen Region - Summary of Probable Construction Costs

| Interchange | Proposed Improvement | Probable Construction Cost |
| :--- | :--- | :---: |
| Interstate 29 | Add turn lanes \& Signals | $\$ 470,000$ |
| Exit 132 | Add turn lane \& Signal | $\$ 240,000$ |
| Exit 177 |  |  |



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### 1.0 INTRODUCTION

The South Dakota Department of Transportation (SDDOT) retained Felsburg Holt \& Ullevig to conduct an analysis of the Interstate system. The study is focused on:

- Ensuring a mainline Level of Service (LOS) of C or better throughout the Interstate System,
- Ensuring an interchange LOS of D or better for all interchanges throughout the Interstate System, and
- Identification of areas not in compliance with current Interstate design standards.


### 1.1 Phase 1 Study Description

The study will be conducted in three phases. Phase 1, summarized in this report, includes a review of the roadway geometrics, crash history, and traffic operations. A screening process utilizes these categories to identify a shortened list of interchanges in need of improvements and / or reconstruction. Conceptual alternative sketches of these potential changes are included.

The result of Phase 1 will be a combination of 15 existing and future interchange locations to be analyzed further in Phase 2. Phase 2 will include the development of detailed geometric layouts of these interchanges, and a review of the projected traffic operations associated with the interchange design. Access management in the vicinity of the interchange will also be considered during Phase 2. The next phase will also include an assessment of the impact of those alternatives on the operating conditions of the mainline and connecting arterial streets. Phase 3 will provide a prioritized plan for implementing the improvements.

### 1.2 2000 SDDOT Interstate Corridor Study

This effort represents an expansion over the First Edition of the study, which was completed in the Year 2000. The Phase 1 portion of that First Edition studied a grouping of 60 existing and 4 proposed interchanges and 148 miles of mainline freeway segments along Interstates 90, 29, and 229. The Phase 2 portion of the study provided a more detailed look at 22

Phase 1



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existing interchanges and 4 new interchanges. The Phase 2 study consisted of the development of detailed geometric layouts of these interchanges, and a review of the projected traffic operations associated with the interchange design. Recommended improvements included such items as the number of lanes required, intersection channelization and traffic control improvements. A capacity analysis to determine the level of service on the mainline, ramps and connecting arterials was also conducted.

### 1.3 Improvements Constructed since Previous Study

The inclusion of an interchange in the Phase 2 report did not automatically indicate that it was a high priority location for reconstruction. The report provided guidance and information to SDDOT and local governments for developing those priorities. Since the time of the 2000 Interstate Corridor Study, several existing interchanges have been reconstructed and three new interchanges have been added to the interstate system. These interchanges are listed below:

## Reconstructed Interchanges

- I-90 Exit 32 - Junction Avenue, Sturgis (2006)
- I-90 Exit 51 - Black Hawk Road, Black Hawk (2009)
- I-90 Exit 57 - I-190 (2000)
- I-90 Exit 58 - Haines Ave. (2000)
- I-90 Exit 60 - East North Street, Rapid City (2006)
- I-90 Exit 61 - Elk Vale Road, Rapid City (2007)
- I-90 Exit 66 - Ellsworth Road, Ellsworth AFB (removed) (2003)
- I-29 Exit 73 - County Road 106, Tea (2005)
- I-29 Exit 79 - 12th Street, Sioux Falls (2007)
- I-29 Exit 81 - Russell Street/Maple Street, Sioux Falls (2003-4)
- I-29 Exit 83 - SD 38 ( $60^{\text {th }}$ Street), Sioux Falls (2003-4)


## New Interchanges

- l-90 Exit 8 - McGuigan Road, Spearfish (2002)
- I-90 Exit 67 - Main Gate Road/Liberty Blvd., Box Elder/Ellsworth AFB (2002)
- I-29 Exit 80 - Madison Street, Sioux Falls (2004)
- I-29 Exit 82 - Benson Road, Sioux Falls (2003-4)


### 1.4 Recent Interchange Studies

Since the completion of the 2000 Interstate Corridor Study, a number of existing and proposed interchange locations have been studied in greater detail. Many of these led to the ultimate construction of new or reconfigured interchanges identified in the previous section and are not


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included with this list. Other locations have much more recent or even current studies underway as a part of the planning and design process associated with future interstate access modifications. Since these detailed studies have been conducted or are underway, these existing and potential new interchange locations were not included in this Phase 1 or Phase 2 analysis. Recent interchange studies include the following:

## Recent Interchange Studies

- I-29/I-229 and I-90/I-229 Interchange Improvements - January 2008
- Environmental Assessment for I-90/I-229 Interchange - September 2008
- I-29 Corridor Study: Exit 73 (Tea Exit) to Exit 77 (41st Street Exit) - Ongoing
- Interstate 29/85 ${ }^{\text {th }}$ Street Interchange Justification Report - Ongoing
- I-90 at Marion Road, Interchange Justification Study - March 2006
- I-90/I-29 Interchange Justification Study - March 2006
- I-90 Exit 399 (Cliff Ave.) Interchange Modification Justification Study - Ongoing
- I-299 and Minnesota Avenue Interchange Justification Report (by City of Sioux Falls) February 2007
- I-90 Blackhawk - Sturgis Corridor Preservation Study - December 2004
- I-90 Environmental Assessment (Exit 40 to Exit 51) - September 2008
- US14A Corridor Study - Ongoing
- I-190 Corridor Study: Silver Street - Ongoing


### 1.5 Phase 1 Study Content

The Interstate in South Dakota is shown by region and Mileage Reference Marker (MRM) as follows:

| SDDOT Region | Interstate | Boundaries |
| :---: | :---: | :---: |
| Rapid City | I-90 | MRM 0.00 to MRM 130.30 |
|  | I-190 | MRM 0.00 to MRM 2.03 |
| Pierre | I-90 | MRM 130.30 to MRM 251.00 |
| Mitchell | I-90 | MRM 251.00 to MRM 412.52 |
|  | I-29 | MRM 0.00 to MRM 124.00 |
|  | I-229 | MRM 0.00 to MRM 10.83 |
|  | 1-29 | MRM 124.00 to MRM 252.65 |



## South Dakota Decennial Interstate Gorridor Study

This report is organized into the following sections:

- Section 2.0: Identification of Deficiencies
- Section 3.0: Analyses of Deficient Interchanges
- Section 4.0: Summary of Interstate Improvements

As shown in the following graphic, the Phase 1 evaluation includes all 678 centerline miles of Interstate mainline in South Dakota and 126 of the 152 total existing interchanges. A statewide inventory was performed to document geometric conditions, traffic safety and Average Daily Traffic (ADT) forecasts.


This inventory led to the identification of a shortened list of deficient interchanges, structures and interstate segments. A detailed review of collision patterns and completion of Level of Service (LOS) analyses revealed a need for improvements at 24 interchanges, widening of 6 miles of Interstate and replacement of 23 structurally deficient bridges. There are 78 functionally obsolete bridges on the interstate system, 30 due to substandard vertical clearance and 48 due to other reasons, typically the width of the shoulders provided on the bridge.


### 2.0 IDENTIFICATION OF DEFICIENCIES

### 2.1 Geometrics and Structures

### 2.1.1 Geometric Condition Measures

The existing geometric features of the interstate mainline throughout the state and the 126 selected interchanges were reviewed to determine if they meet current design criteria. These design features included such items as the travel lane width, shoulder widths, design speed, degree of curve, clear zone, inslope, superelevation, bridge width, vertical clearance, vertical curves and grades. At the interchanges, the analysis also included cross road features such as stopping sight distance, ramp intersection sight distance, vertical curvature through the interchange area, and access control. Desirable values for these roadway elements were based on the South Dakota Department of Transportation Roadway Design Manual and A Policy on Geometric Design of Highways and Streets, published by AASHTO.

### 2.1.2 Interstate Mainline Geometric Conditions

The interstate mainline segments along I-90, I-190, I-29 and I-229 identified above were reviewed using information available on the as-built plans from when the interstate was originally constructed, reconstructed or otherwise improved. Some segments of mainline have been reconstructed since the previous study was conducted in the year 2000. It was assumed that these segments meet current design standards and as such were not included in this review.

The majority of the interstate system in South Dakota consists of two lanes in each direction, with the exception of the segments located in the urban area of Sioux Falls. Three lanes of travel are provided on I-29, from $41^{\text {st }}$ Street (Exit 77) through the $60^{\text {th }}$ Street (Exit 83) interchange. A fourth auxiliary lane is also provided in each direction between the interchange ramps. North of the $60^{\text {th }}$ Street interchange, three lanes are provided in each direction to the I-90 systems interchange (Exit 84).

On I-229, the interstate mainline provides two lanes of travel in each direction, with auxiliary lanes provided between interchanges. The auxiliary lanes begin at the Louise Avenue interchange (Exit 1) and extend to the interchange with Benson Road (Exit 9) with a gap in auxiliary lanes between Exits 5 and 6. The section of I-29, between the Dakota Dunes Boulevard (Exit 1) and River Drive (Exit 2) also consists of two lanes of travel in each direction with auxiliary lanes provided between the interchange ramps.

Tables summarizing the mainline geometric analysis are included in the Appendix. The mainline analysis was generally grouped into the same segments as shown in the design plans since many of the design features were consistently applied within those segments. This review of existing geometric features on the mainline indicated that the most common geometric element that does not meet standards for new construction on the interstate is the inslope. Typically, it ranges from a slope of $3: 1$ to $5: 1$, versus the desirable slope of $6: 1$. Another common element is having a clear zone less than the desirable 30'. As can be seen in the


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summary tables in the Appendix, often this geometric element can be found along several continuous segments of the interstate, likely corresponding with the design criteria at the time of construction.

The longitudinal grade along interstate segments was reviewed and determined to have minimal consequence to the interstate system. Therefore, the longitudinal grade is not reported in this study.

Only a few segments were identified containing grades in excess of the desirable levels of 3.0\% for level terrain and $4.0 \%$ for rolling terrain. On I-90, the only segment exceeding these values is from mile markers 263 and 265, which is located immediately east of the Missouri River bridge near Chamberlain. The maximum grade on this segment is $5.5 \%$. On I-29, between mile markers 208 and 225 north of Summit, the maximum grade present is $4.3 \%$.

Several of the interstate segments on I-90 in the Black Hills region, one segment of I-229 in the Sioux Falls area, and one segment of I-29 near North Sioux City, contain horizontal curves that exceed a desirable $2^{\circ} 15^{\prime}$ curve. These curves range in size from $2^{\circ} 30^{\prime}$ to $4^{\circ} 00^{\prime}$.

The geometric elements identified above typically do not warrant immediate correction, but should be reviewed at the time of pavement replacement or other major improvement projects on the interstate mainline.

The most notable geometric feature on the interstate mainline that does not meet current new construction standards are bridges with substandard widths. In many cases, these bridges are only 30 ' wide. Ninety-nine bridges are classified as structurally deficient or functionally obsolete.. These bridges are discussed in more detail in Section 2.1.4.

### 2.1.3 Interchange Geometric Conditions

The review of existing geometrics for the 126 interchanges selected for this Phase 1 analysis was conducted through a combination of measurements taken in the field, site observations and a review of the design plans provided by SDDOT. This evaluation process identified several design elements that do not meet current design criteria. By far, the most common substandard geometric element was associated with the width provided for the right shoulder. Many locations have a right shoulder width ranging from $1^{\prime}$ to $7.5^{\prime}$, compared to the minimum design criteria of 8'. Several interchange ramps were also noted with lane widths less than $15^{\prime}$ and left shoulder widths less than 2'.

Many of the inslopes on the ramps were typically constructed at a slope of 4:1, which is within the acceptable range of allowable slopes, however, it does not meet the current design criteria of 6:1. This geometric element does not warrant immediate correction, and can be reviewed at the time of pavement replacement along the ramps.

Compliance with the remainder of the geometric features varied from interchange to interchange. The design features that do not meet the desirable design criteria are summarized in the tables provided in the Appendix along with detailed geometric checklists for selected


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interchanges. Additional discussion about the geometric deficiencies at specific interchanges is provided for those interchanges where safety issues have been identified through the crash analysis or concepts have been developed to address operations.

### 2.1.4 Structural Conditions

Several bridges along and crossing the Interstate System are currently classified as functionally obsolete or structurally deficient according to their NBIS rating. It is a high priority for the SDDOT to replace all Structurally deficient bridges. The replacement of Functionally obsolete bridges is considered based on the specific reason for the Functional Obsolescence. Correcting inadequate vertical clearances should be considered a higher priority than widening bridges of inadequate shoulder width when there is no crash history related to the inadequate width.

A statement of probable costs was prepared for the removal and reconstruction of three categories of bridges along the study corridors; 1) Structurally deficient bridges, 2) Functionally obsolete bridges that demonstrate deficient height clearances, and 3) Functionally obsolete bridges for other reasons (i.e. substandard width). The quantities and costs shown in Tables 2.1 through 2.3 are based on conceptual design of the structures and do not include earthwork, mobilization, traffic control, concrete approach slab, or other incidental roadway costs. Bridges that have a structure width of 38 ' were not included in these cost estimates unless they were identified as functionally obsolete or structurally deficient. A total of 95 bridges and tunnels were identified in this analysis, with a total construction cost estimate of $\$ 80.7$ Million. The breakdown of bridges with various roadway segments is shown in the following tables. More detailed information regarding the location and size of each structure is provided in the Appendix.

Table 2.1 Interstate System Structurally Deficient Bridge Replacement Costs

| Region | Interstate | Boundaries | Number of <br> Bridges | Construction <br> Cost |
| :--- | :---: | :--- | :---: | :---: |
| Rapid City | I-90 | MRM 0.00 to MRM 130.30 | 3 | $\$ 1.8$ Million |
| Pierre | I-90 | MRM 130.30 to MRM 251.00 | 5 | $\$ 5.7$ Million |
| Mitchell | I-90 | MRM 251.00 to MRM 412.52 | 4 | $\$ 3.8$ Million |
|  | I-29 | MRM 0.00 to MRM 124.00 | 2 | $\$ 4.0$ Million |
|  | I-229 | MRM 0.00 to MRM 10.83 | 1 | $\$ 1.3$ Million |
| Aberdeen | I-29 | MRM 124.00 to MRM 252.65 | 4 | $\$ 3.6$ Million |

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Table 2.2 Interstate System Low Clearance Functionally Obsolete Bridge Replacement Costs

| Region | Interstate | Boundaries | Number of Bridges | Construction Cost |
| :---: | :---: | :---: | :---: | :---: |
| Rapid City | I-90 | MRM 0.00 to MRM 130.30 | 3 | \$0.69 Million |
|  | I-190 | MRM 0.00 to MRM 2.03 | 2 | \$3.5 Million |
| Pierre | I-90 | MRM 130.30 to MRM 251.00 | 4 | \$1.4 Million |
| Mitchell | I-90 | MRM 251.00 to MRM 412.52 | 13 | \$10.6 Million |
|  | I-29 | MRM 0.00 to MRM 124.00 | 4 | \$1.4 Million |
|  | I-229 | MRM 0.00 to MRM 10.83 | 2 | \$1.6 Million |
| Aberdeen | I-29 | MRM 124.00 to MRM 252.65 | 2 | \$2.0 Million |

Table 2.3 Interstate System Other Functionally Obsolete Bridge Replacement Costs

| Region | Interstate | Boundaries | Number of <br> Bridges | Construction <br> Cost |
| :--- | :---: | :--- | :---: | :---: |
| Rapid City | I-90 | MRM 0.00 to MRM 130.30 | 18 | $\$ 11.9$ Million |
| Mitchell | I-90 | MRM 251.00 to MRM 412.52 | 10 | $\$ 7.2$ Million |
|  | I-29 | MRM 0.00 to MRM 124.00 | 12 | $\$ 8.7$ Million |
|  | I-229 | MRM 0.00 to MRM 10.83 | 1 bridge, 1 tunnel | $\$ 4.0$ Million |
| Aberdeen | I-29 | MRM 124.00 to MRM 252.65 | 6 bridge, 1 tunnel | $\$ 7.4$ Million |



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### 2.2 Traffic Safety

The project team completed a crash analysis of each of the existing 126 interchanges included in this Phase 1 study. Crash information was compiled for the three year period between July 2006 and July 2009. The South Dakota Department of Transportation (SDDOT) provided historical crash information in its Geographic Information Systems (GIS) database. Traffic volume data were also provided by the SDDOT for the calculation of crash rates for each interchange.

The crash rate analysis methodology was first developed for the SDDOT Interstate Corridor Study completed in the Year 2000. The methodology is used to calculate a crash rate per million vehicle trips entering the interchange, similar to the measure typically used to calculate a surface street intersection crash rate. The number of collisions are weighted according to their severity and totaled for the three year time period, then divided by the total number of vehicletrips entering the interchange area.

Crash data were provided in the form of three years of information for each interchange coded by location into the South Dakota Geographic Information System (GIS) database. The data provided a categorization of fatal, injury, and property damage traffic crashes occurring within the interchange area during the time period. A point rating system of 12 points for a fatal crash, 3 points for an injury crash, and 1 point for a property damage only crash was applied to the data. Based on this point system, a 3-year weighted crash sum was established for each interchange. Because of this weighting system, the occurrence of a fatal crash can significantly increase the crash rate, particularly at lower-traffic interchanges. I-29 Exit 201 at Twin Brooks is an example of this influence.

To determine the total number of vehicle-trips associated with a typical interchange, a rectangular cordon line was drawn around the perimeter, extending to 300 feet beyond each ramp terminal intersection and extending along the interstate to just beyond each ramp gore point. The total traffic entering the cordon area was compiled as the sum of the mainline entering volumes, the middle crossroad ADT, and one-half of the total ramp traffic. Traffic volumes were provided by SDDOT Staff. The sum of traffic was calculated to a total number of Millions of Entering Vehicles (MEV) for the three year time period.

By dividing the weighted crash sum by the MEV value, a crash rate was calculated for each interchange. The crash rate calculations are summarized in the Appendix. The study interchanges are ranked according to crash rate. As shown, the top crash rate was found at the I-29 / Twin Brooks interchange (Exit 201) followed by the l-29 / 41 ${ }^{\text {st }}$ Street interchange (Exit 77) in Sioux Falls.

A shortened list of 19 interchanges was designated as high crash locations based on their history relative to the other interchanges. The 19 locations include the highest 10 crash rate interchanges and additional locations that experienced more than double the average crash rate. Table 2.4 lists these 19 locations.

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Table 2.4 19 High Crash Interchange Locations

| Interchange | Rank by Weighted Crash Rate | Number of Crashes by Severity July 2006 to July 2009 |  |  |  | Weighted 3-year Accidents | Crash Rate <br> 3-Year (Wtd. <br> Acc/MEV) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fatal | Injury | PDO | Total |  |  |
| 1-29 Exit 1 | 50 | 0 | 5 | 23 | 28 | 38 | 0.92 |
| I-29 Exit 77 | 2 | 0 | 71 | 103 | 174 | 316 | 3.72 |
| I-29 Exit 132 | 27 | 1 | 3 | 23 | 27 | 44 | 1.45 |
| I-29 Exit 201 | 1 | 1 | 4 | 6 | 11 | 30 | 4.22 |
| I-90 Exit 12 | 25 | 0 | 4 | 24 | 28 | 36 | 1.48 |
| I-90 Exit 23 | 8 | 0 | 5 | 23 | 28 | 39 | 2.36 |
| I-90 Exit 30 | 10 | 0 | 12 | 28 | 40 | 64 | 2.34 |
| I-90 Exit 40 | 3 | 1 | 8 | 23 | 32 | 59 | 3.40 |
| I-90 Exit 55 | 30 | 1 | 12 | 18 | 31 | 66 | 1.39 |
| I-90 Exit 59 | 5 | 0 | 31 | 54 | 85 | 147 | 2.49 |
| I-90 Exit 172 | 6 | 1 | 0 | 4 | 5 | 16 | 2.47 |
| I-90 Exit 235 | 7 | 1 | 2 | 2 | 5 | 20 | 2.45 |
| I-90 Exit 332 | 11 | 0 | 11 | 32 | 43 | 65 | 2.15 |
| I-90 Exit 390 | 9 | 0 | 5 | 24 | 29 | 44 | 2.36 |
| I-229 Exit 2 | 13 | 0 | 21 | 42 | 63 | 105 | 2.03 |
| I-229 Exit 3 | 22 | 0 | 25 | 53 | 78 | 128 | 1.64 |
| I-229 Exit 4 | 14 | 0 | 23 | 49 | 72 | 118 | 2.02 |
| I-229 Exit 5 | 4 | 0 | 35 | 68 | 103 | 173 | 3.25 |
| I-229 Exit 7 | 36 | 0 | 10 | 36 | 46 | 66 | 1.21 |
| Statewide Average Interchange |  | 0.11 | 3.57 | 9.68 | 13.36 | 21.73 | 0.94 |

Additional data were gathered to further evaluate these locations, resulting in a refined assessment of actual collision patterns and problems at each interchange. Table 2.5 summarizes these assessments.

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Table 2.5 Summary of Interchange Safety Evaluations

| Interchange | Collision Patterns |
| :---: | :--- |
| I-29 Exit 1 | No identifiable pattern |
| I-29 Exit 77 | High number of congestion-related collisions, including rear-ends and approach- <br> turn type collisions |
| I-29 Exit 132 | There was one fatal crash but there does not appear to be a correctable pattern |
| I-29 Exit 201 | There was one fatal crash but there does not appear to be a correctable pattern |
| I-90 Exit 12 | No identifiable pattern |
| I-90 Exit 23 | No identifiable pattern |
| I-90 Exit 30 | Overturning crashes are occurring on I-90 in poor roadway conditions |
| I-90 Exit 40 | Of the more severe crashes, 75\% were related to poor roadway conditions |
| I-90 Exit 55 | There was one fatal crash but there does not appear to be an identifiable pattern |
| I-90 Exit 59 | High number of congestion-related collisions, including rear-ends and approach- <br> turn type collisions |
| I-90 Exit 172 | There was one fatal crash but there does not appear to be an identifiable pattern |
| I-90 Exit 235 | There was one fatal crash but there does not appear to be an identifiable pattern |
| I-90 Exit 332 | No identifiable pattern |
| I-90 Exit 390 | No identifiable pattern |
| I-229 Exit 2 | High number of rear ends, typical for signalized urban interchange |
| I-229 Exit 3 | High number of rear ends, typical for signalized urban interchange |
| I-229 Exit 4 | High number of rear ends, typical for signalized urban interchange |
| I-229 Exit 5 | High number of rear ends and congestion-related collisions, pattern of highway <br> sign hits during poor roadway conditions |
| I-229 Exit 7 | No identifiable pattern |



### 2.3 Traffic Forecasts

Traffic counts taken since the 2000 Interstate Corridor Study were provided from various sources. As the year of study initiation, 2009 was chosen as the base forecast year. The Years 2020 and 2030 were designated as future forecast time horizons.

### 2.3.1 Mainline Traffic Forecasts

Year 2008 mainline traffic counts conducted were available in the 2009 Highway Needs and Project Analysis Report (SDDOT, 2009), also known as the Needs Book. The counts provide average annual daily traffic volume (AADT) levels throughout the interstate system, including $\mathrm{I}-90, \mathrm{I}-190, \mathrm{I}-29$ and I-229. The SDDOT supplied the project team with 20-year growth factors for urban and rural portions of each County in South Dakota. These growth factors, used to develop future mainline Interstate traffic forecasts, varied from 16 percent ( 0.7 percent per year) to 62 percent ( 2.6 percent per year) growth. Year 2030 forecasts for I-29 and I-229 in the Sioux Falls area reach 70,000-80,000 vpd. The Appendix provides a summary of all interstate segments with growth rates and AADT forecasts.

### 2.3.2 Interchange Traffic Forecasts

Middle crossroad traffic counts conducted between the Year 2001 and 2007 at each study interchange were provided by the South Dakota Department of Transportation (SDDOT). Forecasts were developed using localized interchange growth rates gathered from a variety of sources. There are 4 quasi-government agencies that include counties through which interstates pass and three Metropolitan Planning Organizations (MPOs). These agencies provided travel demand model information, population growth and land use forecasts. Population growth between the Year 2000 and 2008 is documented by County in the most recent U.S. Census (www.census.gov). This information was used to develop traffic forecasts for the more rural Interstate sections.

To focus study resources on potential operational problem areas throughout the State, the project team screened out the lower-traffic volume interchanges to reach a list of interchanges where conditions could reach substandard Levels of Service (LOS) currently or in the future. For the purposes of this study, substandard interchange operations occur when and where the ramp terminal intersection LOS reaches LOS D or worse and/or freeway and ramp operations reach LOS C or worse. Based on results from the 2000 Interstate Corridor Study and discussion with the Study Advisory Team, interchanges where the daily crossroad traffic volume between the ramp termini ("middle ADT") exceeds 5,000 Vehicles Per Day (vpd) were designated as candidates for operational evaluation.

Table 2.6 depicts the interchanges that, in 2009, exceeded the 5,000 vpd threshold or are projected to exceed 5,000 vpd by the Year 2030. As shown in Table 2.6, a total of 34 interchanges need to be analyzed operationally based on this screening approach. Of these, 21 exceed 5,000 vpd between the ramp terminal intersections based on Year 2009 traffic estimates.


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Table 2.6 Interchanges for Operational Analyses

| Interstate | Exit \# | Location | Projected Year of Exceeding Threshold |
| :---: | :---: | :---: | :---: |
| 29 | 1 | Dakota Dunes | 2009 |
| 29 | 2 | North Sioux City | 2009 |
| 29 | 26 | Vermillion/Yankton | 2009 |
| 29 | 47 | Beresford/Irene | 2009 |
| 29 | 62 | Canton | 2030 |
| 29 | 71 | Harrisburg/Tea | 2030 |
| 29 | 77 | $41^{\text {st }}$ Street | 2009 |
| 29 | 86 | Renner/Crooks | 2030 |
| 29 | 98 | Dell Rapids | 2030 |
| 29 | 132 | Brookings | 2009 |
| 29 | 133 | Brookings/Huron | 2030 |
| 29 | 177 | Watertown | 2009 |
| 29 | 207 | Summit/Aberdeen | 2020 |
| 29 | 232 | Sisseton | 2020 |
| 229 | 2 | Western Ave | 2009 |
| 229 | 3 | Minnesota Ave | 2009 |
| 229 | 4 | Cliff Ave | 2009 |
| 229 | 5 | $26^{\text {th }}$ Street | 2009 |
| 229 | 7 | Rice Street | 2009 |
| 229 | 9 | Benson Road | 2009 |
| 90 | 12 | Jackson Blvd | 2020 |
| 90 | 17 | Lead/Deadwood | 2030 |
| 90 | 30 | Lazelle Street | 2009 |
| 90 | 46 | Elk Creek Road | 2030 |
| 90 | 48 | Stage Stop Canyon | 2020 |
| 90 | 55 | Deadwood Ave | 2009 |
| 90 | 59 | LaCrosse Street | 2009 |
| 90 | 63 | Box Elder/EAFB | 2009 |
| 90 | 330 | Mitchell/Huron | 2009 |
| 90 | 332 | Mitchell/Parkston | 2009 |
| 90 | 387 | Hartford | 2030 |
| 90 | 390 | Hartford | 2009 |
| 90 | 406 | Brandon/Corson | 2009 |
| 190 | 1 | Silver Street | 2009 |

For those interchanges exceeding $5,000 \mathrm{vpd}$ middle ADT, peak hour turning movement traffic forecasts were developed based on the growth rates for each interchange. These peak hour forecasts are included in the Appendix.


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### 2.4 Traffic Operations

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### 2.4.1 Methodology

Analysis of traffic operations in the study area utilized methods documented in the Highway Capacity Manual (HCM), Transportation Research Board (TRB), 2000 Edition. The result of such an analysis is a LOS rating, which is a qualitative assessment of the traffic flow for a given roadway facility. Level of Service is described by a letter designation ranging from "A" to " F ", with LOS A representing essentially uninterrupted flow, and LOS F representing a breakdown of traffic flow with excessive congestion and delay. For analysis of a signalized intersection, a LOS rating is calculated for an intersection as a whole. Level of Service analysis of an unsignalized intersection yields a LOS rating for each critical vehicle movement. A LOS rating may also be calculated for mainline, merge, diverge, or weaving sections along a major freeway using Highway Capacity Software. The Synchro software analysis package and methodology was utilized to calculate LOS ratings for ramp terminal intersections throughout the Interstate system.

The SDDOT seeks to provide LOS C or better operating conditions along mainline sections and LOS D or better conditions at interchange ramp terminal intersections.

The traffic parameters shown in Table 2.7 were used as the basis for the operational analyses of freeway sections and ramp terminal intersections. Traffic parameters were selected based on collected data.

Table 2.7 Traffic Parameters for Operational Analyses

| Traffic Parameter | 1-190 | I-29 |  | 1-229 | 1-90 |  | Ramp <br> Terminal Intersections |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { MRM } \\ 71-127 \end{gathered}$ | Other |  | $\begin{gathered} \hline \text { MRM } \\ 2-67, \\ 406-410 \\ \hline \end{gathered}$ | $\begin{gathered} \text { MRM } \\ 67-406 \\ \hline \end{gathered}$ |  |
| Peak Hour <br> Percentage of AADT | 12\% | 10\% | 10\% | 12\% | 10\% | 10\% | N/A |
| Peak Hour Directional Distribution | 70\% | 65\% | 65\% | 70\% | 65\% | 65\% | N/A |
| \% Heavy Vehicles | 10\% | 15\% | 25\% | 10\% | 15\% | 25\% | 10\% |
| Peak Hour Factor | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.92 |
| Free-Flow Speed ${ }^{1}$ | 55 | 75 | 75 | 65 | 75 | 75 | n/a |
| Terrain/Area Type | Level | Level | Level | Level | Level | Level | Non-CBD |
| Cycle Length | n/a | n/a | n/a | n/a | n/a | n/a | Varies |

Interstate sections posted at 65 Miles Per Hour (mph) include:
I-29 MRM 0-4.64 \& 75.17-86.40; I-90 MRM 57.76-67.15 \& 396.52-402.55


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### 2.4.2 Mainline Interstate Traffic Operations

Mainline Interstate operations were analyzed for 2009, 2020 and 2030 using the growth rates and assumptions previously discussed. The project team found that the entirety of the South Dakota Interstate system operated at LOS C or better in Year 2009. Sections of I-29 and I-229 within the City of Sioux Falls are expected to reach the substandard LOS D by the Year 2020 and LOS F conditions by the Year 2030. Interstate segments through Rapid City are expected to operate at LOS C or better through the Year 2030. Many rural sections are projected to operate at LOS B or better through the Year 2030. The Appendix provides LOS results for mainline Interstates.

The findings of this study indicate that sections of Interstates 29 and 229 through the Sioux Falls area may require widening as early as 2020 to provide acceptable LOS. Changing growth patterns or significant new developments could place capacity pressure on other portions of the South Dakota interstate mainline.

Table 2.8 outlines the performance of substandard mainline segments into the future.
Table 2.8 Mainline Capacity Needs

| Interstate | Section |  | Level of Service |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
|  | 29 |  | $\mathbf{2 0 0 9}$ | $\mathbf{2 0 2 0}$ |  |
|  | Exit 71 to Exit 78 | B | C | D |  |
| 229 | Exit 1 to Exit 2 | B | C | D |  |
|  | Exit 2 to Exit 4 | C | D | F |  |
|  | Exit 4 to Exit 5 | B | D | E |  |
|  | Exit 5 to Exit 6 | C | E | F |  |
|  | Exit 6 to Exit 9 | B | C | D |  |

### 2.4.3 Interchange Traffic Operations

The Appendix provides the results for operational analyses of each of the 34 interchanges analyzed. Freeway merge and diverge sections were analyzed along with ramp terminal intersections. As expected, substandard operations occur at many of the 34 interchanges, and improvements are needed to restore acceptable LOS. Improvements range from the addition of turn lanes at ramp terminal intersections to reconstructed interchanges. Table 2.9 highlights operational issues at each interchange and proposed measures to address these issues.


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Table 2.9 Interchange Capacity Needs


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### 3.0 ANALYSES OF DEFICIENT INTERCHANGES

The Geometric, Safety and Capacity analyses described in Section 2 resulted in the identification of 32 interchanges in need of improvement along the South Dakota Interstate System. Table 3.1 lists these interchanges and the issues contributing to their need. There are no interchanges included in this list based exclusively on geometric deficiencies. It is assumed that geometric deficiencies have been captured in the analysis of crash history.

Table 3.1 Interchange Needs

| SDDOT Region | Interstate | Exit \# | Issues |
| :---: | :---: | :---: | :---: |
| Rapid City | 90 | 12 | Safety, Capacity |
|  | 90 | 17 | Capacity |
|  | 90 | 23 | Safety |
|  | 90 | 30 | Safety |
|  | 90 | 40 | Safety |
|  | 90 | 46 | Capacity |
|  | 90 | 48 | Capacity |
|  | 90 | 55 | Capacity, Safety |
|  | 90 | 59 | Capacity, Safety |
|  | 90 | 63 | Capacity |
|  | 190 | 1 | Capacity, Geometrics |
| Pierre | 90 | 172 | Safety |
|  | 90 | 235 | Safety |
| Mitchell | 29 | 1 | Safety, Capacity |
|  | 29 | 2 | Capacity |
|  | 29 | 26 | Capacity |
|  | 29 | 47 | Capacity |
|  | 29 | 71 | Capacity |
|  | 29 | 77 | Safety, Capacity |
|  | 229 | 2 | Safety, Capacity |
|  | 229 | 3 | Safety, Capacity |
|  | 229 | 4 | Safety, Capacity |
|  | 229 | 5 | Safety, Capacity |
|  | 229 | 7 | Safety, Capacity |
|  | 229 | 9 | Capacity |
|  | 90 | 330 | Capacity |
|  | 90 | 332 | Safety |
|  | 90 | 390 | Safety |
|  | 90 | 406 | Capacity |
| Aberdeen | 29 | 132 | Safety, Capacity |
|  | 29 | 177 | Capacity |
|  | 29 | 201 | Safety |

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Organized by SDDOT Region, the interchange descriptions in Sections 3.1 through 3.4 provide additional information about the needs at each location including geometric, safety, and operational deficiencies. Improvements needed to address these deficiencies have been developed, and the Appendix includes conceptual drawings and cost estimates. Geometric checklists, traffic forecast and Level of Service details.

### 3.1 Rapid City Region

## I-90 Exit 12 (Jackson Blvd)

Of the 28 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 12 animal-vehicle collisions (AVCs) and 6 guardrail crashes. The majority (10 of 12) of the AVCs occurred at night in dry roadway conditions. All of the guardrail crashes occurred during icy or snowy roadway conditions with the majority (4 of 6 ) occurring during daylight. However, no recommendations have been made at this interchange with regard to crash experience since this interchange has an average severity rate and does not demonstrate a crash pattern in need of correction.

The geometric evaluation identified that the grade on the westbound on-ramp of $6.0 \%$ exceeds the maximum amount of $5.0 \%$. In addition, the sag vertical curve on that ramp only provides 276 ' of stopping sight distance, which is considerably less than the $425^{\prime}$ desirable length. Field observations also indicated that the sight distance for eastbound vehicles at the off-ramp intersection may be substandard. Based on information received from SDDOT Staff, unauthorized parking often occurs in the vicinity of the north ramp terminal intersection. As an initial measure, a "No parking" sign may be considered for installation here. Any reconstruction efforts at Exit 12 should also consider the presence of a culvert under I-90 northwest of the interchange. This culvert is currently used by pedestrians navigating the area.

This interchange is located in Spearfish. The ramp terminal intersections are unsignalized and all of the stop controlled movements currently operate at LOS B or better. In addition, both ramp terminals are expected to operate at LOS D or better through the Year 2020. However, by the Year 2030, it is expected that the stop controlled approach at the westbound ramp terminal will operate at LOS F with the current lane geometry. The construction of a second left turn lane on the westbound off-ramp would improve the operations at this ramp terminal to LOS D. An allway STOP intersection would not improve operations, but signalization of this intersection would improve conditions to LOS A.

## I-90 Exit 17 (US Highway 85 to Lead-Deadwood)

This interchange is located just east of Spearfish. The ramp terminal intersections are currently unsignalized and all of the stop controlled movements operate at LOS C or better. A new development named Elkhorn Ridge is being constructed in the vicinity of this interchange. As this development is constructed and nears build-out, traffic volumes at this interchange are expected to dramatically increase. Due to this increase, both ramp terminals are expected to operate at LOS F by the Year 2020 with the existing lane geometry and traffic control. In order to improve this condition, there are two options. In the first option, both ramp terminals will need to be signalized by the Year 2020 and new left and right turn lanes will need to be constructed at both ramp terminals. The addition of these new turn lanes will likely require the existing


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bridges over I-90 to either be widened or reconstructed. If these improvements are constructed, the ramp terminal intersections are expected to operate at LOS B or better. In the second option, a Single-Point Urban Interchange is proposed to take the place of the existing diamond interchange. If this alternative is constructed, the ramp terminal intersection would operate at LOS B by the Year 2030.

## I-90 Exit 23 (Laurel Street - Whitewood)

This interchange ranks $8^{\text {th }}$ of the 126 interchanges evaluated in this study based on weighted crash rate. Of the 28 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 14 AVCs and 5 rear-end crashes. The majority (10 of 14) of the wild animal crashes occurred at night in dry roadway conditions. The majority ( 4 of 5 ) of the rear-end crashes occurred during wet, icy or snowy roadway conditions. No recommendations have been made at this interchange with regard to crash experience since this interchange has an average severity rate and does not demonstrate a crash pattern in need of correction.

Geometric deficiencies at this interchange include the ramp intersection sight distance for both off-ramps. Field observations indicate that less than $425^{\prime}$ is provided at both intersections.

## I-90 Exit 30 (US Highway 14A - Sturgis)

This interchange ranks $10^{\text {th }}$ of the 126 interchanges evaluated in this study based on weighted crash rate. Of the 40 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 9 angle crashes and 5 overturning crashes. All of the angle crashes occurred in the vicinity of the l-90 ramp terminal intersections. All of the overturning crashes occurred in icy / slushy roadway conditions. Several of these crashes occurred along a curved portion of mainline l-90 through the interchange area. In light of this, consideration could be given to realignment of I-90 to soften the curve radii. The number and pattern of crashes at this interchange is not particularly problematic but to help reduce the number of angle type crashes at this interchange consideration could be given to changing the signal phasing to provide protected-only left turns or changing to the clearance interval length.

The geometric evaluation identified several features that do not meet current design standards at this interchange. The westbound off-ramp has a downgrade of $7.5 \%$, which is considerably higher than the $5.0 \%$ desirable. This off-ramp also has a substandard vertical curve, with a k value of 46 , resulting in a stopping sight distance of 317'. The eastbound on-ramp also has some geometric deficiencies, including a superelevation rate of $7.75 \%$, which is higher than the $6.0 \%$ desirable amount, and a minimum radius of 553 ', which is less than the 833 ' desirable radius. To the northeast along Lazelle Street, an adjacent intersection is located on 170 ' from the westbound off-ramp intersection.

This interchange is located in Sturgis. Both ramp terminal intersections are currently signalized and operate at LOS B or better. Even with the growth in traffic in the future both ramp termini are expected to continue to operate at LOS B or better at least to the Year 2030. However, due to the number of roll over crashes at this interchange, a concept has been developed that reduces the horizontal curvature on I-90.


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It should be noted that a project is currently underway to reconstruct the l-90 bridges to soften the horizontal curvature of the mainline freeway. Many of the geometric and safety concerns listed here are being addressed by this project.

## I-90 Exit 40 (Tilford Road - Tilford)

This interchange ranks $3^{\text {rd }}$ of the 126 interchanges evaluated in this study based on weighted crash rate. Of the 32 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 8 guardrail crashes, 7 AVCs and 4 angle crashes. The majority of the guardrail crashes (6 of 8) occurred in icy or snowy conditions. All of the AVCs occurred in dry conditions with most occurring at night. The majority of the angle crashes occurred in icy or snowy conditions with most occurring during the day. The one fatal crash at this interchange was an angle crash that occurred during the day in dry condition. Of the more severe crashes at this interchange, guardrail and angle, 75 percent happened in snowy or icy roadway conditions. A review of snow removal procedures at this location is recommended to determine if something needs to be done to improve roadway conditions during the winter.

The geometric evaluation of this interchange identified that the sag vertical curve on the crossroad immediately north of the bridge (not the crest curve across the bridge) is substandard, with a k value of 60 and a resulting stopping sight distance of 288 ', compared to the 425' desirable stopping sight distance. The intersection west of the westbound off-ramp intersection is located approximately 250 ' from the ramps, which is less than the 300 desirable access spacing.

## I-90 Exit 44 (Deerview Road - Piedmont)

As noted on page A-4 of the Appendix, the eastbound and westbound I-90 interchange bridges over Deerview Road are functionally obsolete (low clearance) and structurally deficient, respectively. Mainline l-90 structures west of this interchange demonstrate similar conditions. In addition, SDDOT staff expressed concern regarding a fatal crash that occurred in 2008 along eastbound mainline I-90 north of the interchange. Reduced pavement skid resistance may have contributed to the crash. Pavement condition should be addressed when the structures are replaced.

## I-90 Exit 46 (Elk Creek Road - Piedmont)

The most distinctive feature of this interchange is its severe crest vertical curve overpass and close accesses. Crash histories do not indicate a safety problem associated with the current design. Growing traffic, though, would trigger the need for bridge reconstruction and signalization to provide acceptable ramp terminal intersection operations by the Year 2030. A realigned diamond interchange was proposed in the 2004 Interstate 90 Black Hawk-Sturgis Corridor Preservation Study (Felsburg Holt \& Ullevig) and would operate acceptably with a 3lane bridge and channelized ramp approaches to intersections.

## I-90 Exit 48 (Stage Stop Canyon Rd. - Piedmont)

This interchange is located northwest of Rapid City, serving a growing urban edge. Substandard operations are projected to occur at the east ramp terminal intersection by the Year 2020 and the west ramp terminal by the Year 2030, requiring signalization of both intersections and


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widening of the westbound off ramp intersection approach. Substandard access spacing adjacent to the interchange hastens the need for improvements. A single-point interchange option was recommended in the Interstate 90 Black Hawk - Sturgis Corridor Preservation Study and demonstrates LOS B intersection operations by the Year 2030.

## I-90 Exit 55 (Deadwood Avenue - Rapid City)

Of the 31 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 7 angle crashes, 6 rear-end crashes and 4 overturn crashes. The majority of the angle crashes occurred in dry daylight conditions. All of the rear-end crashes occurred during the day with most occurring in dry conditions. The majority of the overturn crashes (3 of 4) occurred in dry conditions with a $50-50$ split between day and night. The one fatal crash at this interchange was an overturn crash that occurred during the day in dry conditions. However, no recommendations have been made at this interchange with regard to crash experience since the data for this interchange does not demonstrate a crash pattern in need of correction and this interchange does not have one of the higher crash rates within the state.

The downgrade for the westbound on-ramp contains a maximum grade of $5.6 \%$, which is above the desirable rate of $5.0 \%$. In addition, both the westbound on-ramp and off-ramp provide a sag vertical curve k value below the minimum range, resulting in substandard stopping sight distance. The crest vertical curve on the crossroad also contains a $k$ value below the minimum range. There is a full movement truck stop access located approximately 330 feet south of the interchange. This distance meets minimum spacing criteria but does not meet the desired spacing distance of 660 feet. SDDOT staff has noted operational problems created by this close spacing.

The Deadwood Avenue interchange serves the west edge of Rapid City, and traffic operations at the ramp terminal intersections are shown to deteriorate to LOS E/F by the year 2030. The south ramp terminal, currently unsignalized with a temporary signal during peak motorcycle rally season, would need to be signalized and widened to provide acceptable operations. Deadwood Avenue across I-90 would need to be widened to 4 lanes, necessitating a significant bridge widening project. Movements at the adjacent south truck stop access should be limited to right turns only with a raised 'pork chop' style island to improve traffic safety and operations.

## I-90 Exit 59 (LaCrosse Street - Rapid City)

This interchange ranks $5^{\text {th }}$ of the 126 interchanges evaluated in this study based on weighted crash rate. Of the 85 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 43 rear-end crashes and 31 angle crashes. It is likely that the high number of rear-end crashes is related to congestion in the vicinity of the interchange so there may be little that can be done to reduce the occurrence of this crash type. However, there may be an opportunity to reduce the number of angle type crashes at this interchange, especially if they are related to approach turn type crashes where permitted left turners pull out in front of oncoming traffic or broadside crashes where one vehicle is running the red light and striking a vehicle. Both of these crash types can be reduced with changes to the signal phasing (i.e. protected lefts) or changes to the clearance interval length.


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The downgrade for the westbound on-ramp contains a maximum grade of $5.6 \%$, which is above the desirable rate of $5.0 \%$. The sag vertical curve on the westbound off-ramp contains a $k$ value below the minimum range, as well as stopping sight distance of $262^{\prime}$, compared to the $425^{\prime}$ minimum desired.

This interchange is located at a focal point of activity in Rapid City, straining the capacity of the current diamond interchange. The signalized ramp terminal intersections currently operate at LOS D and E during the PM peak period and are expected to worsen with future growth. Additional turn lanes at the ramp terminal intersections and widening of the LaCrosse Street bridge would improve substandard traffic operations. Providing a free eastbound to southbound right turn movement would substantially improve traffic operations though this action would require widening of LaCrosse Street south of the interchange. A Single-Point Urban Interchange would operate at LOS A/C by the Year 2030 and would serve to increase distance to adjacent accesses along LaCrosse Street. A diverging diamond concept will be investigated for Exit 59 in Phase 2 of the Decennial Interstate Corridor Study.

## I-90 Exit 63 (US Highway 14-16 - Box Elder)

This interchange is located just east of Rapid City near the Town of Box Elder. Both ramp terminal intersections are currently unsignalized and all of the stop controlled movements operate at LOS B or better. Even with the growth in traffic in the future, both ramp termini are expected to operate at LOS C or better through the Year 2030. However, since this interchange in currently only a partial diamond, there is a desire to construct a full diamond interchange at this location. Two full diamond interchange concepts have been developed for this location. If a full diamond is constructed here, the ramp terminal intersections are expected to continue to operate at LOS C or better through the Year 2030.

## I-190 Exit 1 (Silver Street - Rapid City)

This interchange is located in Rapid City. The layout of this interchange is an unconventional split diamond with ramps coming on and off of I-190 at various locations. In addition, the northbound ramp terminal intersection currently has 5 legs. Currently, all stop controlled approaches at the two ramp terminal intersections on Silver and North Streets operate at LOS A. With the growth in traffic in the future, these two intersections are expected to operate at LOS B or better through at least the Year 2030. However, due to the unconventional layout of the existing interchange and northbound ramp terminal intersection there is a desire to standardize the layout of the interchange. Three concepts have been developed in order to do this. The first alternative replaces the existing 5 legged stop controlled northbound ramp terminal with a 5 legged roundabout. This proposed roundabout is expected to operate at LOS A or better in the Year 2030. The second alternative removes the grade separation of I-190 with Silver and North Streets and in its place constructs a signalized intersection. This alternative would remove the majority of the existing ramps and with the proposed lane geometry is expected to operate at LOS C in the Year 2030. The third alternative also removes the grade separation of I-190 with Silver and North Streets but in it place constructs a two lane 5 legged roundabout. This alternative would also remove the majority of the existing ramps and is expected to operate at LOS A in the Year 2030.


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### 3.2 Pierre Region

## I-90 Exit 172 (Stamford Road - Stamford)

This interchange ranks $6^{\text {th }}$ based on weighted crash rate. Even with a low total number of crashes, this interchange is in the top ten due to the one fatal crash that occurred during the study period. The highest occurring crash type at this interchange was overturn crashes, one of which was fatal. The fatal crash occurred during the day in icy conditions. No recommendations have been made at this interchange with regard to crash experience since the data for this interchange does not demonstrate a crash pattern in need of correction. There are so few crashes and the majority of the rates are below the averages for the entire state.

The geometric evaluation determined that the sag vertical curve on the crossroad has k value of 19 , which is well below the minimum desirable amount. An adjacent intersection is located approximately 120 to the north of the westbound ramp intersection.

## I-90 Exit 235 (SD Highway 273 - Kennebec)

Based on weighted crash rate, this interchange ranks $7^{\text {th }}$ of the 126 interchanges evaluated in this study. This interchange ranks in the top ten due to the more severe crashes that occurred during the study period. Of the 5 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 3 overturn crashes, of which one was fatal. The fatal crash occurred during the night in icy conditions. No recommendations have been made at this interchange with regard to crash experience since the data for this interchange do not demonstrate a crash pattern in need of correction.

An existing driveway is located approximately 235' north of the westbound ramp intersection, which is closer than the 300' minimum desirable distance.

### 3.3 Mitchell Region

## I-29 Exit 1 (Dakota Dunes Boulevard - Sioux City)

Of the 28 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 13 animal-vehicle collisions (AVCs) and 5 angle crashes. The majority ( 10 of 13) of the wild animal crashes occurred at night in dry roadway conditions. The majority (3 of 5) of the angle crashes occurred during the day in dry roadway conditions. However, no recommendations have been made at this interchange with regard to crash experience since this interchange is near the average weighted crash rate and does not demonstrate a crash pattern in need of correction.

The primary substandard geometric element at this interchange is the minimum radius of the loop ramps located in the northwest and southeast quadrants of the interchange. The 330' radius provided on these loop ramps is less than the 883 ' desirable radius, although the smaller radius does not appear to contribute to the high number of crashes at this interchange.

This interchange is currently a Parclo A. The unsignalized southbound ramp terminal intersection is expected to operate at LOS F in the AM peak period by 2020. The signalized northbound ramp terminal intersection is expected to operate at LOS E and F during the AM


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and PM peak periods by 2030. The addition of a second northbound right turn lane at the northbound ramp terminal intersection is recommended. Traffic signalization is also recommended at the southbound ramp terminal intersection and at the intersection of Dakota Dunes Boulevard with Sioux Point Road.

The NB off-ramp diverge is expected to operate at LOS F in the AM peak period by 2020. It is recommended that an additional lane be added to the NB off-ramp.

## I-29 Exit 2 (SD Highway 105 River Drive - North Sioux City)

This diamond interchange has a traffic signal at the northbound ramp terminal and the southbound ramp terminal is unsignalized. The southbound ramp terminal is expected to operate at LOS F in both the AM and PM peak periods by 2030. Signalization and the addition of a southbound right-turn lane would improve traffic operations. Another improvement option would be conversion to one-lane roundabouts at both the northbound and southbound ramp terminals.

## I-29 Exit 26 (SD Highway 50 - Vermillion/Yankton)

The existing diamond interchange is unsignalized and the northbound ramp terminal intersection is expected to operate at LOS F by 2030. SDDOT has plans to improve the intersection to add eastbound and northbound left turn lanes. By 2020, traffic signalization is recommended at the northbound ramp terminal intersection.

## I-29 Exit 47 (SD Highway 46 - Beresford/Irene)

This existing diamond interchange is unsignalized at both ramp terminals. Both the northbound and southbound ramp terminal intersections are expected to operate at LOS E or $F$ in both peak periods by 2020. Signalization and the addition of northbound and southbound left-turn lanes would improve traffic operations. Another improvement option would be conversion to one-lane roundabouts at both the northbound and southbound ramp terminals.

## I-29 Exit 71 (SD Highway 110 - Harrisburg/Tea)

This existing diamond interchange is unsignalized at both ramp terminals. The SB off-ramp diverge and SB on-ramp merge are expected to operate at LOS D in the PM peak period by 2030. It is recommended that the deceleration lane be extended to a minimum of 800 ' for the SB off-ramp, and the acceleration lane be lengthened to a minimum of 800 ' for the SB on-ramp.

## I-29 Exit 77 (41 ${ }^{\text {st }}$ Street - Sioux Falls)

This interchange ranks $2^{\text {nd }}$ of the 126 interchanges evaluated in this study in weighted crash rate, primarily due to the high number of total crashes that occurred at this interchange.
Between 2006 and 2009. Of the 174 total crashes during the 3 -year study period, the most frequent crash types at this interchange were 95 rear-end crashes and 56 angle crashes. It is likely that the high number of rear-end crashes is related to congestion on I-29 and the offramps. An alternative interchange configuration may help reduce the occurrence of rear-end crashes. There may also be an opportunity to reduce the number of angle type crashes at this interchange, especially if they are related to approach turn type crashes where permitted left turners pull out in front of oncoming traffic or broadside crashes where one vehicle is running


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the red light and striking a vehicle. Both of these crash types can be reduced with changes to the signal phasing (i.e. protected lefts) or changes to the clearance interval length.

There are a few geometric deficiencies at this interchange that may contribute to some of the crash types experienced. The southbound on-ramp taper rate is only 29:1, compared to the minimum rate of $50: 1$. This ramp also provides substandard stopping sight distance, although it is associated with a sag vertical curve. The adjacent intersections are also located close to the interchange ramps. To the east, South Carolyn Avenue is approximately 200' away, which is closer than the minimum of 300' identified as acceptable and 600' desirable. To the west, South Meadow Avenue is located a little further away at approximately 400', but is still relatively close given the volume of traffic on $41^{\text {st }}$ Street.

The $41^{\text {st }}$ Street interchange is a signalized diamond and currently operates at LOS E in the AM peak period and LOS F in the PM peak at both ramp terminals. By 2020 and 2030, operations are expected to be LOS F. The limited ROW and close spacing of adjacent intersections and driveways present a number of operational and safety problems along the $41^{\text {st }}$ Street corridor. Lane additions to the existing diamond would not be sufficient to improve operations to LOS D. The limited ROW at the interchange prevents the addition of loop ramps at the interchange. Two improvement concepts have been developed for the interchange; a Single Point Urban Interchange, and a Diverging Diamond.

At this interchange the NB off-ramp diverge, and NB and SB on-ramp merges are expected to operate at a LOS D or worse by 2020. By 2030 the SB on-ramp is expected to operate at LOS $F$. It is recommended that an additional lane be added on the mainline for the SB off-ramp, SB on-ramp and NB on-ramp. Also, an additional lane is recommended for the SB on-ramp. For the NB off-ramp it is recommended that the deceleration lane be extended to a minimum of $1275^{\prime}$.

## I-229 Exit 2 (Western Avenue - Sioux Falls)

Of the 63 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 32 rear-end crashes and 12 angle crashes. It is likely that the high number of these crash types is related to congestion in the vicinity of the interchange and the off-ramps. The total number of each of these types is not particularly unusual for an interchange located within an urban area. Therefore, no recommendations are made for safety improvements at this interchange.

A variety of geometric deficiencies were identified at this interchange, mostly dealing with substandard $k$ values and stopping sight distance for sag vertical curves. Every ramp at the interchange had values below the minimum desired levels. The crossroad to the north also has a substandard $k$ value and stopping sight distance for the sag vertical curve. It was also observed that the sight distance provided at the ramp intersections is below the 425' acceptable distance.

The Western Avenue interchange is a signalized diamond and currently operates at LOS F at both ramp terminals in the PM peak period. By 2020 the westbound ramp terminal is also expected to operate at LOS F in the AM peak period. The addition of turn lanes at both of the ramp terminal intersections and the addition of a third southbound through lane at the


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northbound ramp terminal is recommended to improve traffic operations. Another improvement option would be conversion to a Single Point Urban Interchange.

The EB on-ramp merge is expected to operate at LOS D in the AM peak period by 2030. It is recommended that an additional EB and WB lane be added to the mainline, creating three basic lanes through the system.

## I-229 Exit 3 (Minnesota Avenue - Sioux Falls)

Of the 78 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 35 rear-end crashes and 18 angle crashes. It is likely that the high number of these crash types is related to congestion in the vicinity of the interchange and the off-ramps. In addition, the total number of each of these types is not particularly unusual for an interchange located within an urban area. Therefore, no recommendations are made for safety improvements at this interchange.

Deficient geometric conditions at this interchange include a low $k$ value of 76 for the westbound on-ramp. Adjacent access points on both sides of the interchange are located within the 300' minimum spacing. Only $160^{\prime}$ is provided on the north side of the interchange, and 200 ' is provided on the south side.

The Minnesota Avenue interchange is a signalized diamond and is expected to operate at LOS E or F at both ramp terminals by 2020. By 2030 both of the ramp terminal intersections are expected to operate at LOS F in both peak periods. In 2007, an Interchange Justification Report was completed for this interchange. The study recommended the construction of a northbound to westbound loop ramp in the northeast quadrant of the interchange. In order to accommodate the loop ramp, the westbound off ramp would also be relocated approximately 300' further north. This westbound off-ramp would also align with a proposed extension of 49th Street, from Western Avenue to Minnesota Avenue. The southbound to westbound on-ramp would also be reconstructed to provide more distance on the mainline from the new loop ramp. This proposed concept was estimated to cost $\$ 5.6$ million.

The EB on-ramp merge is expected to operate at LOS D in the PM peak period by 2030. The WB on-ramp merge and WB off-ramp diverge are expected to operate at LOS D and F in the AM peak periods by 2030. It is recommended that an additional EB and WB lane be added to the mainline, creating three basic lanes in both directions.

## I-229 Exit 4 (Cliff Avenue - Sioux Falls)

Of the 72 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 31 rear-end crashes and 13 angle crashes. It is likely that the high number of these crash types is related to congestion in the vicinity of the interchange and the off-ramps. In addition, the total number of each of these types is not particularly unusual for an interchange located within an urban area. Therefore, no recommendations are made for safety improvements at this interchange.


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The intersections adjacent to the interchange ramps are located approximately 200' north and 150 ' south of the ramp intersections.

The Cliff Avenue interchange is a modified signalized diamond with the westbound off-ramp terminal forming an intersection via a direct connection with $41^{\text {st }}$ Street. The westbound on-ramp is located to the south of the $41^{\text {st }}$ Street / westbound off-ramp intersection and is unsignalized. The $41^{\text {st }}$ Street / westbound off-ramp intersection is expected to operate at LOS E in the PM peak period by 2030. The addition of an eastbound left-turn lane and another westbound rightturn lane at the $41^{\text {st }}$ Street / westbound off-ramp intersection is recommended to improve traffic operations.

The EB on-ramp merge is expected to operate at LOS D in the PM peak period by 2030. The WB on-ramp merge is expected to operate at LOS D in the AM peak periods by 2030. It is recommended that an additional EB and WB lane be added to the mainline, creating three basic lanes in both directions.

## I-229 Exit 5 (26 ${ }^{\text {th }}$ Street - Sioux Falls)

This interchange ranks $4^{\text {th }}$ of the 126 interchanges evaluated in this study based on weighted crash rate. Of the 103 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 51 rear-end crashes, 18 angle crashes and 7 highway traffic sign post crashes. It is likely that the high number of rear-end and angle crash types are related to congestion in the vicinity of the interchange and the off-ramps. In addition, the total number of each of these types is not particularly unusual for an interchange located within an urban area. A pattern emerges from the data related to the highway traffic sign post crashes since the majority of these crashes occurred in poor roadway conditions on the northbound I-229 onramp. In order to reduce the number of this crash type, the highway traffic sign should be relocated or warning signs should be placed on the ramp to encourage motorists to slow down during slick conditions.

A number of the geometrics at this interchange are substandard, associated with the unconventional configuration. The $26^{\text {th }}$ Street to northbound I-229 on-ramp provides a curve with a radius of 205', which is below the desirable radius of 231' for a loop ramp. The configuration of the southbound off and on-ramps also provide substandard radii, although they do intersect perpendicularly with South Yeager Road. The k values for the southbound on-ramp are also below the desirable levels. Stopping sight distance for the southbound on and offramps are both below the distance required for 50 mph design. A driveway is located only 260 ' east of the northbound on and off-ramp intersection with $26^{\text {th }}$ Street.

The $26^{\text {th }}$ Street interchange is a signalized folded diamond for the northbound ramps and provides unconventional access to South Yeager Road for the southbound ramps. The northbound ramp terminal intersection currently operates at LOS E in the AM peak period and the southbound ramp intersection currently operates at LOS E in the PM peak period. By 2020, all of the ramp terminal Intersections are expected to operate at LOS E or F in both the AM and PM peak periods. The addition of turn lanes at the ramp terminal intersections and the intersection of $26^{\text {th }}$ Street with Yeager Road is recommended to improve traffic operations. The City has proposed the construction of a folded diamond interchange for the southbound ramps,


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which would also include the removal of Yeager Street. The cross section of 26th Street, through the interchange area would also be widened to provide left turn lanes at the ramp intersections.

Another improvement option would be conversion to an offset Single Point Urban Interchange, which would also address the substandard loop ramp geometrics for the northbound on-ramp and permit Yeager Street to remain in service.

## I-229 Exit 7 (Rice Street - Sioux Falls)

Of the 46 total crashes during the 3 -year study period, the most frequent crash types at this interchange were 9 guardrail crashes, 7 AVCs and 7 angle crashes. It is likely that the high number of these crash types is related to congestion or slick road conditions in the vicinity of the interchange so there may be little that can be done to reduce the occurrence of these crash types. In addition, the total number of each of these types is not particularly unusual for an interchange located within an urban area. No recommendations are made for safety improvements at this interchange.

The Rice Street interchange is a folded diamond. The southbound ramp terminal intersection is unsignalized and currently operates at LOS F in the PM peak period. By 2020, both of the ramp terminal intersections are expected to operate at LOS E or $F$ in both the AM and PM peak periods. SDDOT has designed a new signal for the southbound ramp terminal with additional turn lanes. At the signalized northbound ramp terminal intersection, other additional turn lanes are recommended.

## I-229 Exit 9 (Benson Road - Sioux Falls)

The Benson Road diamond interchange has a traffic signal at the northbound ramp terminal and the southbound ramp terminal is unsignalized. The southbound ramp terminal currently operates at LOS F. By 2030, both of the ramp terminal intersections are expected to operate at LOS F in both the AM and PM peak periods. At the southbound ramp terminal intersection, signalization and the addition of turn lanes would improve traffic operations. At the northbound ramp terminal, the addition of an exclusive northbound right turn lane is recommended by 2030.

## I-90 Exit 330 (Ohlman Street (I-90B) - Mitchell/Huron)

The existing diamond interchange is unsignalized. By 2030 in the PM peak hour, the eastbound ramp terminal intersection is expected to operate at LOS E and the westbound ramp terminal is expected to operate at LOS F. Signalization at both of the ramp terminal intersections and the addition of a westbound left-turn lane is recommended to improve traffic operations.

## I-90 Exit 332 (SD Highway 37 - Mitchell / Parkston)

Of the 43 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 16 angle crashes and 15 rear-end crashes. The majority of the angle and rear-end crashes occurred in dry daylight conditions and are likely due to high traffic volumes. It is possible that the number of angle crashes could be reduced by changing the phasing (i.e. protected-only left turns) or lengthening the clearance intervals at the ramp terminals. The crash


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experience is not particularly problematic given the low number of total crashes and the relatively minor severity of most of the crashes.

## I-90 Exit 390 (SD Highway 38 - Hartford)

Based on weighted crash rate, this interchange ranks $9^{\text {th }}$ of the study interchanges. Of the 29 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 6 guardrail crashes and 5 sideswipe-same direction crashes. Half of the guardrail crashes occurred in snowy / icy roadway conditions with most occurring during the day. Nearly all of the sideswipe-same direction crashes occurred during the day in dry conditions. However, no recommendations have been made at this interchange with regard to crash experience since the data for this interchange do not demonstrate a crash pattern in need of correction.

The geometric evaluation identified that the stopping sight distance of 407' for the eastbound on-ramp is slightly below the minimum value of $425^{\prime}$. It is unlikely that this minor reduction in sight distance has contributed to the crash history at this interchange.

## I-90 Exit 406 (SD Highway 11 - Brandon/Corson)

The existing diamond interchange is unsignalized and only provides a two-lane bridge with no left-turn lanes. By 2030 the eastbound ramp terminal is expected to operate at LOS F in both peak periods and the westbound ramp terminal intersection is expected to operate at LOS F in the AM peak period. Signalization at both of the ramp terminal intersections and the addition of left-turn lanes on each approach is recommended to improve traffic operations. Another improvement option would be conversion to a Single Point Urban Interchange.

### 3.4 Aberdeen Region

## I-29 Exit 132 (US Highway 14 - Brookings)

Of the 27 total crashes during the 3-year study period, the highest occurring crash types at this interchange were 7 angle crashes and 6 rear-end crashes. The one fatal crash at this interchange was an angle crash that occurred during the day on a wet surface. However, no recommendations have been made at this interchange with regard to crash experience since this interchange has a relatively low weighted crash rate and there is no correctable pattern evident based on a review of the crash data.

This existing diamond interchange is unsignalized at both ramp terminals. US 14 has a four-lane divided cross section in this location with exclusive eastbound and westbound left-turn lanes. Both the northbound and southbound ramp terminal intersections currently operate at LOS E or F in both peak periods. By 2020 and 2030, operations are expected to be LOS F. Signalization at both of the ramp terminal intersections and the addition of northbound and southbound leftturn lanes is recommended to improve traffic operations.

Information provided by SDDOT Staff indicates that the ramp terminal intersections are planned for signalization by the Year 2010.

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## I-29 Exit 177 (US Highway 212 - Watertown)

This existing diamond interchange is unsignalized at both ramp terminals. US 212 has a fourlane divided cross section in this location with exclusive eastbound and westbound left-turn lanes. The northbound ramp terminal intersection is expected to operate at LOS F in the PM peak periods by 2020. Signalization and the addition of a northbound left-turn lane would improve traffic operations at the northbound ramp terminal intersection.

## I-29 Exit 201 (SD Highway 8 - Twin Brooks)

This interchange ranks $1^{\text {st }}$ of the 126 interchanges evaluated in this study based on weighted crash rate, primarily due to the high number of severe crashes occurring at this interchange and the relatively low traffic volume. Of the 11 total crashes during the 3 -year study period, the highest occurring crash types at this interchange were 4 bridge rail / guardrail crashes and 2 angle crashes. Half of the bridge / guard rail crashes occurred in icy conditions while the other half occurred in dry conditions and 3 of the 4 occurred either in dark or dawn lighting conditions. The one fatal crash at this interchange was an angle crash that occurred during the day on a wet roadway surface. However, no safety enhancement recommendations are made at this interchange since there are a low number of crashes so there is no correctable pattern evident based on a review of the crash data.


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### 4.0 SUMMARY OF INTERSTATE IMPROVEMENTS

As discussed in the Introduction, the focus of this study is to:

- Ensure a mainline Level of Service (LOS) of C or better throughout the Interstate System,
- Ensure an interchange LOS of D or better for all interchanges throughout the Interstate System, and
- Identify areas not in compliance with current Interstate design standards.

The evaluation of geometric, safety and operational conditions throughout the South Dakota Interstate system resulted in a list of mainline freeway sections and interchanges where improvements are needed to reach compliance with the study goals. This section provides that list and conceptualizes the improvements needed.

### 4.1 List of Mainline Interstate Improvements

As discussed in Section 2.4.2, a number of mainline Interstate segments would need to be widened in the future to accommodate traffic growth. It is recommended that Interstate 29 between Exit 75 and Exit 79 be widened from 4 to 6 lanes. Widening is also recommended along I-229 between I-29 and Exit 6 . Table 4.1 outlines the recommended mainline widening efforts through the Year 2030.

Table 4.1 Recommended Interstate Widening Projects

| Interstate | Section | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Current Lanes | Widen to | Year |
| 29 | Exit 71 to Exit 77 | 4 | 6 | 2030 |
|  | Exit 77 to Exit 78 | 6 | 8 | 2030 |
| 229 | Exit 1 to Exit 2 | 6 | 8 | 2030 |
|  | Exit 2 to Exit 3 | 6 | 8 | 2020 |
|  | Exit 3 to Exit 4 | 6 | 8 | 2020 |
|  | Exit 4 to Exit 5 | 6 | 8 | 2020 |
|  | Exit 5 to Exit 6 | 4 | 6 | 2020 |
|  | Exit 5 to Exit 6 | 6 | 8 | 2030 |
|  | Exit 6 to Exit 9 | 6 | 8 | 2030 |

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### 4.2 List of Interchange Improvements

Table 4.2 List of Deficient Interchanges and Improvement Alternatives

| Interstate | Exit |  |
| :---: | :---: | :--- |
| 29 | 1 | Signalize southbound off-ramp terminal and Sioux Point Road Intersection |
| 29 | 2 | Add turn lanes |
| 29 | 26 | Either signalize southbound ramp terminal and provide additional turn lanes or <br> construct a roundabout |
| 29 | 47 | Signalize northbound ramp terminal and provide additional turn lanes |
| 29 | 71 | No capacity improvements identified |
| 29 | 77 | Single Point w/ triple lefts or Diverging Diamond |
| 29 | 132 | Signalize ramp terminals and provide additional turn lanes |
| 29 | 177 | Signalize northbound ramp terminal and provide additional turn lanes |
| 29 | 201 | No safety improvements identified |
| 90 | 12 | Widen westbound off-ramp to accommodate second left turn lane |
| 90 | 17 | Either signalize ramp terminals and provide additional turn lanes or construct a <br> Single-Point Urban Interchange |
| 90 | 23 | No safety improvements identified |
| 90 | 30 | No capacity improvements, realign mainline I-90 |
| 90 | 40 | No physical improvements, enhance snow removal |
| 90 | 46 | Reconstruct realigned diamond interchange east of existing and signalize terminals |
| 90 | 48 | Reconstruct diamond with signalization; consider single-point option |
| 90 | 55 | Permanently signalize south ramp terminal and widen bridge to accommodate turn <br> lanes at intersections |
| 90 | 59 | Widen bridge and ramps to improve operations; consider reconstructing <br> interchange as a Single-Point Urban Interchange |
| 90 | 63 | New Diamond Interchange per Box Elder Transportation Plan |
| 90 | 172 | No safety improvements identified |
| 90 | 235 | No safety improvements identified |
| 90 | 330 | Signalize both ramp terminals and add turn lanes to improve operations |
| 90 | 332 | No improvements identified |
| 90 | 390 | No improvements identified |
| 90 | 406 | Widen bridge and ramps to improve operations; consider reconstructing <br> interchange as a Single-Point Urban Interchange |
| 190 | 1 | In order to bring this interchange closer to standard, options include roundabouts or <br> an at grade signalized intersection that removes the need for an interchange |
| 229 | 2 | Widen bridge and ramps to improve operations; consider reconstructing <br> interchange as a Single-Point Urban Interchange |
| 229 | 3 | Widen Minnesota Ave and Ramps to improve operations; consider reconstructing <br> interchange as a Single-Point Urban Interchange |
| 229 | 4 | Provide additional turn lanes to improve operations |
| 229 | 5 | Consider reconstructing interchange as an offset Single-Point Urban Interchange |
| 229 | 7 | Signalize the west ramp terminal adding turn lanes, reconstruct east terminal to <br> provide addditional capacity |
| 229 | 9 | Signalize the west ramp terminal and add turn lanes to improve operations |
| 9 |  |  |
| 90 |  |  |



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Interchanges demonstrating substandard geometric, safety, and operating characteristics were identified in the previous sections. Table 4.2 provides a listing of these 32 interchanges demonstrating safety or operational issues. Based on the evaluations in Section 3.1, the 32 interchanges listed in were reduced to 24 interchanges where improvements are recommended.

Preliminary design concepts have been prepared for each of the interchange improvements listed in Table 4.2. These concepts, shown in the Appendix, provide solutions to geometric, operational, and safety issues. Multiple alternatives are provided at several of the interchanges.

A statement of probable construction costs was developed for each interchange improvement identified in Phase 1 as well as freeway widening projects. Tables 4.3 through 4.5 summarize those probable construction costs. The costs shown are based on conceptual design for budgetary purposes. The cost estimate calculations are provided in the Appendix.

Table 4.3 Rapid City Region - Summary of Probable Construction Costs

| Interchange | Proposed Improvement | Probable Construction Cost |
| :---: | :---: | :---: |
| Interstate 90 |  |  |
| Exit 12 | Add turn lane-widen bridge | \$50,000 |
|  | Signalize north intersection | \$125,000 |
| Exit 17 | Diamond | \$4.6 Million |
|  | Single-Point | \$18.6 Million |
| Exit 30 | Realign mainline l-90 | \$19.8 Million |
| Exit 46 | Reconstructed Diamond | \$8.7 Million |
| Exit 48 | Single-Point | \$12.0 Million |
|  | Relocated Diamond | \$8.1 Million |
| Exit 55 | Bridge widening | \$4.2 Million |
| Exit 59 | Diamond | \$7.2 Million |
|  | Single-Point | \$14.5 Million |
| Exit 63 | Diamond | \$8.7 Million |
|  | Flyover | \$13.2 Million |
| Interstate 190 |  |  |
| Exit 1 | 2-lane roundabout | \$3.2 Million |
|  | 1-lane roundabout | \$1.3 Million |
|  | Signal | \$1.6 Million |

## South Dakota Decennial Interstate Gorridor Study

Table 4.4 Mitchell Region - Summary of Probable Construction Costs

| Interchange | Proposed Improvement | Probable Construction Cost |
| :---: | :---: | :---: |
| Interstate 29 |  |  |
| I-29 Widening | Additional travel lane in each direction: Exit 75-77 and Exit 78-79 | \$56 Million ${ }^{1}$ |
| Exit 1 | Add turn lane \& Signals | \$410,000 |
| Exit 2 | Signal/relocate Fr. Rd. | \$860,000 |
|  | Roundabout/relocate Fr. Rd. | \$700,000 |
| Exit 26 | Reconstruct NB Ramps/signal | \$1.3 Million |
| Exit 47 | Add turn lanes \& Signals | \$470,000 |
|  | Add roundabouts | \$560,000 |
| Exit 77 | Single-Point | \$9.9 Million |
|  | Diverging Diamond/exist bridge | \$2.5 Million |
|  | Diverging Diamond w/new bridge | \$11.5 Million |
| Interstate 90 |  |  |
| Exit 330 | Add turn lanes \& Signals | \$470,000 |
| Exit 406 | Reconstruct Crossroad/add Signals | \$5.9 Million |
|  | Single-Point | \$9.3 Million |
| Interstate 229 |  |  |
| I-229 Freeway Widening | Additional travel lane in each direction: I-29 to Exit 5, two more lanes Exit 5 to Exit 6 | \$72 Million ${ }^{1}$ |
| Exit 2 | Add turn lane \& re-stripe | \$60,000 |
|  | Single-Point | \$12.6 Million |
| Exit 4 | Add turn lanes | \$240,000 |
| Exit 5 | Offset Single-Point | \$8.8 Million |
| Exit 7 | Crossroad \& Ramp Improvement/add Signal | \$1.2 Million |
| Exit 9 | Add turn lanes \& Signal | \$350,000 |

Assumed conceptual estimated cost of Interstate widening is $\$ 4$ Million per mile per lane. This assumption is based on cost estimates developed for freeway widening projects in the 2004 Interstate 90 Black Hawk - Sturgis Corridor Preservation Study (Felsburg Holt \& Ullevig). Estimated costs did not include Right-of-way. Actual costs would vary widely based on local conditions.

Table 4.5 Aberdeen Region - Summary of Probable Construction Costs

| Interchange | Proposed Improvement | Probable Construction Cost |
| :--- | :--- | :---: |
| Interstate 29 | Add turn lanes \& Signals | $\$ 470,000$ |
| Exit 132 | Add turn lane \& Signal | $\$ 240,000$ |
| Exit 177 |  |  |

PHASEONEREPORT

## APPENDIX

## Contents by SDDOT Region:

Rapid City Region: pp. A-3 through A-96
Pierre Region: pp. A-97 through A-106
Mitchell Region: pp. A-107 through A-276
Aberdeen Region: pp. A-277 through A-313
Summary table of mainline Interstate performance, including:

- Mainline geometrics
- Year 2009, 2020 and 2030 daily volumes and Levels of Service (LOS)
- Summary of structurally deficient and functionally obsolete Bridges

Summary table of interchange performance, including:

- Interchange geometrics
- Crash Information
- Year 2009, 2020 and 2030 Interchange LOS (where analyzed)

Detailed information for deficient interchanges only, including:

- Concept(s) drawn for improvements
- Conceptual Cost Estimate(s)
- Geometric checklist
- Year 2009, 2020 and 2030 peak hour volumes and LOS

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## RAPID CITY REGION

Interstate 90, MRM 0.00 to MRM 130.30
Interstate 190, MRM 0.00 to MRM 2.03
Total Interchanges: 38
Studied Interchanges: 28

| Deficient Interchanges (10): | $\frac{\text { Page }}{}$ |
| :---: | :---: |
| I-90 Exit 12 | A-9 |
| I-90 Exit 17 | A-17 |
| I-90 Exit 30 | A-27 |
| I-90 Exit 40 | A-35 |
| I-90 Exit 46 | A-37 |
| I-90 Exit 48 | A-45 |
| I-90 Exit 55 | A-55 |
| I-90 Exit 59 | A-63 |
| I-90 Exit 63 | A-73 |
| I-190 Exit 1 | A-83 |

## Summary of Mainline Segment Geometric Performance Rapid City Region

| I－90 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MP 0－10 | 12 | 10 | 4 | 70 | $2^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 5.7 | 38 | 40 | n／a | 2.06 | 0．33\％ |
| MP 10－14 | 12 | 10 | 4 | 65 | $3^{\circ} 00^{\prime}$ | 3：1 | 6：1 | 6．0\％ | 38 | 38 | 16＇0＂ | 3．00\％ | 0．30\％ |
| MP 14－20 | 12 | 10 | 4 | 70 | $1^{\circ} 30^{\prime}$ | ＞ 30 | 6：1 | 5．0\％ | 38 | 38 | 16＇6＂ | 1．94\％ | 0．20\％ |
| MP 20－28 | 12 | 10 | 4 | 75 | $2^{\circ} 00^{\prime}$ | ＞ 30 | 5：1 | 6．0\％ | 38 | 38 | 17＇${ }^{\prime \prime}$ | 3．39\％ | 0．40\％ |
| MP 28－38 | 12 | 10 | 4 | 65 | $2^{\circ} 30^{\prime}$ | $>30$ | 5：1 | 5．6\％ | 38 | 40 | 16＇ 7 ＂ | 3．72\％ | 0．00\％ |
| MP 38－44 | 12 | 10 | 4 |  | $1^{\circ} 00^{\prime}$ | $>30$ | 6：1 |  | 38 | n／a | 17＇4＂ | 3．63\％ | 0．38\％ |
| MP 44－53 | 12 | 10 | 4 | 75 | $2^{\circ} 00^{\prime}$ | 3：1 | 6：1 | 6．0\％ | 38 | n／a | 15＇10＇ | 4．00\％ | 0．00\％ |
| MP 53－64 | 12 | 10 | 6 | 65 | $2^{\circ} 30^{\prime}$ | ＞ 30 | 5：1 | 6．9\％ | 40 | 30 | 16＇5＂ | 4．00\％ | 0．00\％ |
| MP 64－69 | 12 | 10 | 4 | 75 | $2^{\circ} 00{ }^{\prime}$ | ＞ 30 | 5：1 | 6．0\％ | 38 | 30 | 16＇6＂ | 2．43\％ | 0．20\％ |
| MP 76－95 | 12 | 10 | 6 | 65 | $1^{\circ} 30{ }^{\prime}$ | ＞ 30 | 5：1 | 4．2\％ | 40 | 30 | 17＇ 2 ＂ | 2．99\％ | 0．00\％ |
| MP 95－102 | 12 | 10 | 4 | 65 | $2^{\circ} 00^{\prime}$ | ＞ 30 | 5：1 | 5．0\％ | 38 | 30 | 18＇ 0 ＂ | 4．00\％ | 0．00\％ |
| MP 102－112 | 12 | 10 | 4 | 75 | $2^{\circ} 15^{\prime}$ | ＞ 30 | 6：1 | 6．0\％ | 38 | 38 | 16＇0＂ | 4．89\％ | 0．13\％ |
| MP 112－125 | 12 | 10 | 4 | 70 | $2^{\circ} 06^{\prime}$ | ＞ 30 | 6：1 | 5．7\％ | 38 | 40 | 17＇1＂ | 2．44\％ | 0．00\％ |
| MP 125－133 | 12 | 10 | 4 |  | $2^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 |  | 38 | n／a | 15＇9＂ | 3．06\％ | 0．26\％ |
| I－190 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 0－1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 1－2 |  |  |  |  |  |  |  |  |  |  |  |  |  |

## LEGEND：

Existing Value does not meet standard criteria
Mainline section recently reconstructed

Summary of Mainline Segments, Traffic Volumes and Levels of Service Rapid City Region

| I-90 Exits: | Current Lanes | Existing |  | 2020 |  | 2030 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AADT | LOS | AADT | LOS | AADT | LOS |
| 0 to 2 | 4 | 5,670 | A | 7,427 | A | 9,300 | A |
| 2 to 8 | 4 | 5,690 | A | 7,108 | A | 8,556 | A |
| 8 to 10 | 4 | 8,400 | A | 10,493 | A | 12,631 | A |
| 10 to 12 | 4 | 8,820 | A | 11,018 | A | 13,263 | A |
| 12 to 14 | 4 | 17,720 | A | 22,136 | B | 26,646 | B |
| 14 to 17 | 4 | 13,380 | A | 17,525 | A | 21,945 | A |
| 17 to 23 | 4 | 11,590 | A | 15,181 | A | 19,009 | A |
| 23 to 30 | 4 | 11,590 | A | 14,364 | A | 17,177 | A |
| 30 to 32 | 4 | 8,930 | A | 11,068 | A | 13,235 | A |
| 32 to 34 | 4 | 16,320 | A | 18,051 | A | 19,634 | A |
| 34 to 37 | 4 | 16,320 | A | 18,051 | A | 19,634 | A |
| 37 to 40 | 4 | 15,290 | A | 16,912 | A | 18,395 | A |
| 40 to 44 | 4 | 15,250 | A | 16,868 | A | 18,346 | A |
| 44 to 46 | 4 | 18,150 | A | 22,495 | B | 26,900 | B |
| 46 to 48 | 4 | 19,940 | A | 24,713 | B | 29,553 | B |
| 48 to 51 | 4 | 20,350 | A | 25,221 | B | 30,160 | B |
| 51 to 55 | 4 | 22,200 | B | 27,825 | B | 33,586 | B |
| 55 to 57 | 4 | 28,740 | B | 32,302 | B | 35,606 | C |
| 57 to 58 | 4 | 32,380 | B | 36,393 | C | 40,115 | C |
| 58 to 59 | 4 | 30,880 | B | 34,707 | B | 38,257 | C |
| 59 to 60 | 4 | 26,570 | B | 29,863 | B | 32,917 | C |
| 60 to 61 | 4 | 25,940 | B | 29,155 | B | 32,137 | C |
| 61 to 63 | 4 | 22,670 | B | 28,414 | B | 34,297 | C |
| 63 to 67 | 4 | 16,850 | A | 21,119 | A | 25,492 | B |
| 67 to 78 | 4 | 8,950 | A | 11,218 | A | 13,540 | A |
| 78 to 84 | 4 | 7,380 | A | 9,250 | A | 11,165 | A |
| 84 to 88 | 4 | 7,150 | A | 8,962 | A | 10,817 | A |
| 88 to 90 | 4 | 7,180 | A | 8,999 | A | 10,863 | A |
| 90 to 98 | 4 | 7,290 | A | 9,137 | A | 11,029 | A |
| 98 to 101 | 4 | 7,450 | A | 9,338 | A | 11,271 | A |
| 101 to 107 | 4 | 7,400 | A | 9,275 | A | 11,195 | A |
| 107 to 109 | 4 | 7,500 | A | 9,400 | A | 11,347 | A |
| 109 to 110 | 4 | 7,080 | A | 8,874 | A | 10,711 | A |
| 110 to 112 | 4 | 7,290 | A | 9,137 | A | 11,029 | A |
| 112 to 116 | 4 | 7,400 | A | 9,275 | A | 11,195 | A |
| 116 to 121 | 4 | 6,020 | A | 7,545 | A | 9,108 | A |
| 121 to 127 | 4 | 5,240 | A | 5,518 | A | 5,761 | A |
| 127 to 131 | 4 | 5,420 | A | 5,708 | A | 5,959 | A |
| I-190 Exits: |  |  |  |  |  |  |  |
| 1-90 to 1\| | 4 | 17,670 | B | 19,860 | B | 21,891 | C |

Structurally Deficient and Functionally Obsolete Mainline Structure Summary- Rapid City Region

| 1-90 MRM 0 to 130.3 | Number of Bridges | Length | $\begin{aligned} & \hline \text { Existing Deck } \\ & \text { Out-to-Out } \\ & \text { Width } \\ & \hline \end{aligned}$ | Existing <br> Area | Unit Price | $\begin{gathered} \text { Removal } \\ \text { Cost } \end{gathered}$ | Proposed Deck Clear Roadway Width | Proposed Area | Unit Price | Bridge Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Highway 34 at MRM 30.28 (Functionally Obsolete-NARROW) | 2 | 182 | 34 | 12,485 | \$9 | \$112,367 | 40 | 14,560 | \$100 | \$1,456,000 |
| I-90 / BH National Cemetary Road at MRM 34.81 (EB - Functionally Obsolete) | 1 | 119 | 44 | 5,272 | \$9 | \$47,445 | 40 | 4,760 | \$100 | \$476,000 |
| Elk Creek at MRM 42.81 (WB - Functionally Obsolete/EB - Structurally Deficient) | 2 | 140 | 34 | 9,604 | \$9 | \$86,436 | 40 | 11,200 | \$100 | \$1,120,000 |
| Little Elk Creek at MRM 44.10 <br> (WB - Functionally Obsolete/EB - Structurally Deficient) | 2 | 129 | 34 | 8,849 | \$9 | \$79,645 | 40 | 10,320 | \$100 | \$1,032,000 |
| WB I-90 over Deerview Road at MRM 44.66 (Structurally Deficient) | 1 | 160 | 34 | 5,488 | \$9 | \$49,392 | 40 | 6,400 | \$100 | \$640,000 |
| EB I-90 over Deerview Road at MRM 44.66 (Functionally Obsolete-LOW CLEARANCE) | 1 | 160 | 34 | 5,440 | \$9 | \$48,960 | 40 | 6,400 | \$100 | \$640,000 |
| I-90 over North Maple Avenue at MRM 58.80 (Functionally Obsolete) | 2 | 119 | 44 | 10,543 | \$9 | \$94,891 | 40 | 9,520 | \$100 | \$952,000 |
| Eastbound I-90 over DM\&E Spur MRM 65.76 (Functionally Obsolete-NARROW) | 2 | 162 | 35 | 11,264 | \$9 | \$101,373 | 40 | 12,984 | \$100 | \$1,298,400 |
| I-90 over 151st Ave at MRM 68.15 (Functionally Obsolete-NARROW) | 2 | 164 | 34 | 11,250 | \$9 | \$101,254 | 40 | 13,120 | \$100 | \$1,312,000 |
| I-90 over 169th Ave at MRM 86.23 (Functionally Obsolete-NARROW) | 2 | 164 | 34 | 11,250 | \$9 | \$101,254 | 40 | 13,120 | \$100 | \$1,312,000 |
| I-90 over 173rd Ave at MRM 90.25 (Functionally Obsolete-NARROW) | 2 | 158 | 34 | 10,839 | \$9 | \$97,549 | 40 | 12,640 | \$100 | \$1,264,000 |
| I-90 WB over 175th Ave at MRM 92.23 (Functionally Obsolete) | 1 | 86 | 44 | 3,810 | \$9 | \$34,288 | 40 | 3,440 | \$100 | \$344,000 |
| I-90 over Bull Creek at MRM 101.4 (Functionally Obsolete-NARROW) | 2 | 189 | 34 | 12,931 | \$9 | \$116,380 | 40 | 15,080 | \$100 | \$1,508,000 |
| 1-190 MRM 0 to 2.03 |  |  |  |  |  |  |  |  |  |  |
| Silver Street at MRM 0.43 NB (Functionally Obsolete-LOW CLEARANCE) | 1 | 394 | 34 | 13,514 | \$9 | \$121,628 | 40 | 15,760 | \$100 | \$1,576,000 |
| Silver Street at MRM 0.43 SB (Functionally Obsolete-LOW CLEARANCE) | 1 | 421 | 34 | 14,440 | \$9 | \$129,963 | 40 | 16,840 | \$100 | \$1,684,000 |


|  |  | Geometric Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Crashes, 2006-2009 |  |  |  |  |  |  | 2009/2020/2030 Level of Service |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-90 | Location |  |  |  |  |  |  |  |  | $\begin{gathered} \overline{\bar{\theta}} \\ \stackrel{\rightharpoonup}{0} \\ \stackrel{\rightharpoonup}{0} \\ \stackrel{\rightharpoonup}{\omega} \end{gathered}$ |  |  |  |  |  |  |  |  |  |  |  | 음 |  |  |  |  |  |  | 0.0 <br> 0.0 <br> 20 <br> 0 <br> 0 <br> 0 <br> 0 | $\begin{aligned} & \stackrel{\otimes}{0} \\ & \sum_{\infty}^{\circ} \\ & \infty \\ & \stackrel{\infty}{\infty} \\ & \sum_{3}^{\infty} \end{aligned}$ |  |  |
| Exit 2 | McNenny Fish Hatchery | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.4\% | 14.0' | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 213 | 898 | > 425 | n/a | >425 | 2.2\% | 250' | 0 | 1 | 9 | 10 | 12 | 1.80 | 15 | Not eva | luated du | e to inter | change s | creening | method |
| Exit 12 | Jackson Blvd. | 5.4\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 6.0\% | $15.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 30 | 52 | 52 | 276 | sub | 120 | 520 | 6.0\% | 360' | 0 | 4 | 24 | 28 | 36 | 1.48 | 25 | A/A/A | B/B/B | A/B/B | A/A/A | b/b/c | $\mathrm{b} / \mathrm{b} / \mathrm{f}$ |
| Exit 17 | Lead/Deadwood | 5.9\% | 955' | $6^{\circ}$ | $>30^{\prime}$ | 5.0\% | $13.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 93 | 490 | $>425$ | 500 | 1039 | 4.5\% | 200' | 0 | 4 | 13 | 17 | 25 | 1.31 | 34 | B/B/C | A/B/B | A/A/B | A/B/B | a/f/f | c/f/f |
| Exit 23 | Whitewood | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 4.1\% | $12.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $0.0{ }^{\prime}$ | 4:1 | 39 | 61 | 104 | 479 | sub | 40 | 238 | 2.8\% | 500' | 0 | 5 | 24 | 29 | 39 | 2.36 | 8 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 30 | Lazelle Street | 7.7\% | 573' | $10^{\circ}$ | $>30^{\prime}$ | 7.5\% | $15.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 4:1 | 40 | 50 | 46 | 317 | $>425$ | 107 | 497 | 3.4\% | 171' | 0 | 12 | 28 | 40 | 64 | 2.34 | 10 | A/A/B | B/B/B | A/A/A | A/A/A | B/B/B | A/A/B |
| Exit 34 | BH National Cemetery | 3.5\% | 2865' | $2^{\circ}$ | $>30^{\prime}$ | 3.4\% | $13.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 4:1 | 39 | 60 | 100 | 509 | sub | 17 | 188 | 6.0\% | 80' | 1 | 2 | 17 | 20 | 35 | 1.77 | 18 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 37 | Pleasant Valley Road | 5.0\% | 1432' | $4^{\circ}$ | $>30^{\prime}$ | 5.6\% | $13.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | 3.0 | 4:1 | 36 | 58 | 70 | 331 | sub | 25 | 178 | 6.3\% | $>660^{\prime}$ | 0 | 8 | 8 | 16 | 32 | 1.76 | 19 |  |  |  |  |  |  |
| Exit 40 | Tilford Road | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.1\% | $15.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 4:1 | 40 | 61 | 198 | $>425$ | $>425$ | 60 | 288 | 6.0\% | 250' | 1 | 8 | 23 | 32 | 59 | 3.40 | 3 |  |  |  |  |  |  |
| Exit 44 | Piedmont | 3.8\% | $310^{\prime}$ |  | < 30 " |  | 15.0' | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 3:1 | 17 | 21 | 40 | 318 | > 425 | 27 | 165 | 7.9\% | $50^{\prime}$ | 1 | 4 | 12 | 16 | 24 | 1.78 | 16 |  |  |  |  |  |  |
| Exit 46 | Elk Creek Road |  | $310^{\prime}$ |  | < 30" |  | 15.0' | $4.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 3:1 | 17 | 21 |  |  | sub |  |  |  |  | 0 | 5 | 15 | 20 | 30 | 1.17 | 39 | B/B/B | B/B/B | B/B/C | B/B/B | b/b/e | b/c/f |
| Exit 48 | Stage Stop Canyon Rd. |  | $310^{\prime}$ |  | < 30 " | 3.9\% | $15.0{ }^{\prime}$ | $3.0^{\prime}$ | $3.0{ }^{\prime}$ | 3:1 | 17 | 21 | 110 | 412 |  | 59 | 393 | 3.03 | 80' | 0 | 5 | 14 | 19 | 29 | 1.02 | 46 | B/B/C | B/B/C | B/CID | B/B/C | b/c/c | c/f/f |
| Exit 55 | Deadwood Avenue | 2.0\% |  | n/a | > $30^{\prime}$ | 5.6\% | $12.0{ }^{\prime}$ | 8.0 | 2.0 | 4:1 |  |  | 46 | 246 | $>425$ | 56 | 460 | 3.8\% | 330' | 1 | 12 | 18 | 31 | 66 | 1.39 | 30 | B/B/B | B/C/C | B/C/D | B/B/C | ff/ff | B/C/E |
| Exit 59 | LaCrosse Street | 2.0\% |  | n/a | $>30^{\prime}$ | 5.6\% | $15.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 4:1 |  |  | 49 | 262 | $>425$ |  |  | 6.0\% | 250' | 0 | 31 | 54 | 85 | 147 | 2.49 | 4 | B/C/C | B/B/C | B/B/B | B/B/B | E/E/E | D/D/E |
| Exit 63 | Box Elder/Ellsworth AFB Commercial | 5.0\% | 955' | $6^{\circ}$ | <30" | 4.0\% | $15.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 |  | 58 | 93 | 414 | n/a | n/a | n/a | n/a | n/a | 1 | 9 | 15 | 25 | 54 | 1.33 | 33 | B/B/B | ---- | ---- | B/B/B | b/b/c | b/b/b |
| Exit 78 | New Underwood |  | 1432' |  | <30" | 4.8\% | $13.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 4:1 | 29 | 29 | 61 | 310 | sub | 114 | 514 | 5.5\% | > 660' | 0 | 3 | 4 | 7 | 13 | 1.22 | 36 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 84 | 167th Avenue |  | 1432' |  | <30" | 4.0\% | $13.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $1.0^{\prime}$ | 4:1 | 29 | 29 | 65 | 318 | $>425$ | 89 | 400 | 4.0\% | $>660^{\prime}$ | 0 | 0 | 1 | 1 | 1 | 0.12 | 119 |  |  |  |  |  |  |
| Exit 88 | 171st Avenue | 5.0\% | 1763' | $3^{\circ} 15^{\prime}$ | <30" | 2.6\% | $15.0{ }^{\prime}$ | $1.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 4:1 | 29 | 29 | 113 | 486 | $>425$ | 140 | 550 | 4.0\% | $>660^{\prime}$ | 0 | 0 | 6 | 6 | 6 | 0.76 | 60 |  |  |  |  |  |  |
| Exit 90 | 173rd Avenue |  | 1432' |  | < 30 " | 4.9\% | $15.0{ }^{\prime}$ | $1.0{ }^{\prime}$ | $1.0{ }^{\prime}$ | 4:1 | 29 | 29 | 106 | 628 | $>425$ | 82 | 655 | 2.3\% | $>660^{\prime}$ | 0 | 0 | 3 | 3 | 3 | 0.37 | 99 |  |  |  |  |  |  |
| Exit 98 | Wasta | 6.0\% | 409' | $14^{\circ}$ | > $30^{\prime}$ | 3.7\% | $15.0{ }^{\prime}$ | $5.0{ }^{\circ}$ | $3.0{ }^{\prime}$ | 4:1 | 41 | 51 | 54 | 447 | $>425$ | 111 | 1017 | 0.9\% | $>660^{\prime}$ | 0 | 2 | 6 | 8 | 12 | 1.36 | 32 |  |  |  |  |  |  |
| Exit 101 | Jensen Road | 6.0\% | 409' | $14^{\circ}$ | > $30^{\prime}$ | 3.4\% | 17.0' | $3.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | 4:1 | 41 | 62 | 149 | 788 | $>425$ | 177 | 470 | 6.0\% | $>660^{\prime}$ | 0 | 0 | 4 | 4 | 4 | 0.49 | 85 |  |  |  |  |  |  |
| Exit 107 | Cedar Butte Road | 6.0\% | 819' | $7{ }^{\circ}$ | $>30^{\prime}$ | 4.1\% | $15.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 98 | 439 | > 425 | 167 | 603 | 4.0\% | $>660$ | 0 | 1 | 2 | 3 | 5 | 0.60 | 74 |  |  |  |  |  |  |
| Exit 109 | Wall | 4.4\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.4\% | $15.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 149 | 449 | > 425 | 125 | 399 | 3.0\% | 250' | 0 | 3 | 6 | 9 | 15 | 1.53 | 23 |  |  |  |  |  |  |
| Exit 110 | Wall / Badlands Loop | 5.9\% | 955' | $6^{\circ}$ | > $30^{\prime}$ | 2.4\% | $15.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 56 | 90 | 443 | > 425 | 46 | 350 | 3.2\% | 250' | 1 | 1 | 4 | 6 | 19 | 1.39 | 29 |  |  |  |  |  |  |
| Exit 112 | Philip/Pierre | 6.0\% | 200 | 28.65 | > $30^{\prime}$ | 2.6\% | $12.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 294 | 597 | n/a | n/a | n/a | n/a | n/a | 0 | 1 | 3 | 4 | 6 | 0.64 | 68 |  |  |  |  |  |  |
| Exit 116 | 239th Street | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.7\% | $15.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 149 | 603 | > 425 | 268 | 1793 | 2.5\% | > 660' | 0 | 0 | 1 | 1 | 1 | 0.13 | 118 |  |  |  |  |  |  |
| Exit 121 | Big Foot Road | 6.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.6\% | $16.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $1.0{ }^{\prime}$ | 6:1 | 40 | 61 | 149 | 579 | > 425 | 225 | 811 | 2.3\% | $>660^{\prime}$ | 0 | 0 | 2 | 2 | 2 | 0.32 | 102 |  |  |  |  |  |  |
| Exit 127 | County Road 23A | 5.4\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.8\% | $15.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0^{\prime}$ | 6:1 | 40 | 60 | 138 | 539 | > 425 | 240 | 1267 | 3.0\% | > 660' | 0 | 0 | 2 | 2 | 2 | 0.34 | 101 |  |  |  |  |  |  |
| 1-190 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Exit 1 | North Street/Silver Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2 | 11 | 13 | 17 | 0.49 | 83 | N/A | A/B/B | A/A/B | N/A | a/b/b | a/b/b |

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# I-90 EXIT 12 JACKSON BOULEVARD 




## Probable Construction Costs

## Exit 12 - Added Left Turn Lane

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
| Mobilization |  |  |  |  |
| Traffic Control | 1 | LUMP SUM | $\$ 153,000.00$ | $\$ 153,000$ |
| Clearing | 1 | LUMP SUM | $\$ 305,000.00$ | $\$ 305,000$ |
| Removal of Concrete Pavement | 1 | LUMP SUM | $\$ 61,000.00$ | $\$ 61,000$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Remove Bridge | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 3,072 | SQ. FT. | $\$ 9.00$ | $\$ 27,648$ |
| Base Course | 564 | CU. YD. | $\$ 5.30$ | $\$ 2,991$ |
| Asphalt Composite | 249 | TON | $\$ 10.64$ | $\$ 2,653$ |
| PCC Pavement 11" (mainline) | 249 | TON | $\$ 80.91$ | $\$ 20,177$ |
| PCC Pavement 8" (ramps) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| Concrete Approach Slab |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Bridges | 6,400 | SQ. YD. | $\$ 188.34$ | $\$ 1,205,389$ |
| Guard Rail | 17,920 | SQ. FT. | $\$ 100.00$ | $\$ 1,792,000$ |
| Permanent Signing/Markings | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Traffic Signal | 1 | LUMP SUM | $\$ 90,000.00$ | $\$ 90,000$ |
| Roadway Lighting | 0 | EACH | $\$ 125,000.00$ | $\$ 0$ |
| Drainage (18" RCP) | 1 | LUMP SUM | $\$ 60,000.00$ | $\$ 60,000$ |
|  | 30 | LF | $\$ 24.53$ | $\$ 736$ |
| Subtotal |  |  |  | $\$ 3,720,000$ |
| Contingencies |  |  |  | $\$ 90,350,000$ |

## INTERCHANGE GEOMETRICS CHECKLIST

## SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 12 (Jackson Blvd.) |
| Analyst: | BDW |
| Date: | $8 / 26 / 2009$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  |  |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 4.9\% | 5.4\% | 4.2\% | 4.2\% |  |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | $833 / 231$ feet | 1910' | 1910' | 1910' | 1910' |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | > 30 | > 30 | $>30$ | > 30 |  |
| Maximum Grade on Ramp (Ascending) | $+3 \%$ to $+5 \%$ | 0.9\% | 3.3\% | 5.0\% | n/a |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.3\% | n/a | n/a | -6.0\% | Supports Impr. |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 15 | 15 | 15 | 15 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 4 | 2 | 2 | 4 | Supports Impr. |
| Left Shoulder | 2 feet | 2 | 2 | 2 | 2 |  |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 |  |
| Minimum Off-Ramp Taper Rate | 20:1 | 38 | n/a | 30 | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 61 | n/a | 52 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ | n/a | n/a | n/a | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 132 | 214 | 174 | 52 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 626' | 990' | 1200' | 276' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  |  |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  |  |  |  |  |
| Ramp Intersection Sight Distance (ISD) (50 mph / 30 mph )*** | 425 / 200 feet | ok | n/a | substandard | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  |  |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  |  |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.), | $300 / 660$ feet |  |  |  |  | Supports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments
Bridge $K$ value tight. Ramp $A$ and $C$ sight distance substandard




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## I-90 EXIT 17 LEAD / DEADWOOD




## Probable Construction Costs

## Exit 17 - Turning Lanes

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 122,000.00$ | $\$ 122,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 243,000.00$ | $\$ 243,000$ |
| Clearing | 1 | LUMP SUM | $\$ 49,000.00$ | $\$ 49,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | 9,864 | SQ. FT. | $\$ 9.00$ | $\$ 88,776$ |
| Borrow, Unclassified Excavation | 5,092 | CU. YD. | $\$ 5.30$ | $\$ 26,996$ |
| Base Course | 943 | TON | $\$ 10.64$ | $\$ 10,029$ |
| Asphalt Composite | 2,512 | TON | $\$ 80.91$ | $\$ 203,252$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Concrete Approach Slab | 3,600 | SQ. YD. | $\$ 188.34$ | $\$ 678,031$ |
| Bridges | 14,248 | SQ. FT. | $\$ 100.00$ | $\$ 1,424,800$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 70,000.00$ | $\$ 70,000$ |
| Traffic Signal | 2 | EACH | $\$ 125,000.00$ | $\$ 250,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 50,000.00$ | $\$ 50,000$ |
| Drainage (18" RCP) | 60 | LF | $\$ 24.53$ | $\$ 1,472$ |
| Subtotal |  |  |  | $\$ 3,220,000$ |
|  |  |  |  |  |
| Contingencies | $25 \%$ |  |  | $\$ 805,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 4,030,000$ |
| Engineering, Administration | $15 \%$ |  |  | $\$ 604,500$ |



## Probable Construction Costs

 Exit 17 - Single Point Interchange| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 502,000.00$ | $\$ 502,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 1,003,000.00$ | $\$ 1,003,000$ |
| Clearing | 1 | LUMP SUM | $\$ 201,000.00$ | $\$ 201,000$ |
| Removal of Concrete Pavement | 10,892 | SQ. YD. | $\$ 3.88$ | $\$ 42,292$ |
| Removal of Asphalt Pavement | 7,261 | SQ. YD. | $\$ 7.39$ | $\$ 53,674$ |
| Remove Bridge | 11,712 | SQ. FT. | $\$ 9.00$ | $\$ 105,408$ |
| Borrow, Unclassified Excavation | 69,591 | CU. YD. | $\$ 5.30$ | $\$ 368,973$ |
| Base Course | 13,200 | TON | $\$ 10.64$ | $\$ 140,409$ |
| Asphalt Composite | 13,772 | TON | $\$ 80.91$ | $\$ 1,114,218$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Concrete Approach Slab | 3,600 | SQ. YD. | $\$ 188.34$ | $\$ 678,031$ |
| Bridges | 75,249 | SQ. FT. | $\$ 100.00$ | $\$ 7,524,900$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Roundabout (Single Lane) | 1 | EACH | $\$ 600,000.00$ | $\$ 600,000$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 300,000.00$ | $\$ 300,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 200,000.00$ | $\$ 200,000$ |
| Drainage (18" RCP) | 180 | LF | $\$ 24.53$ | $\$ 4,415$ |
| Subtotal |  |  |  | $\$ 12,960,000$ |
|  |  |  |  |  |
| Contingencies | $25 \%$ |  |  | $\$ 3,240,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 16,200,000$ |
| Engineering, Administration | $15 \%$ |  |  | $\$ 2,430,000$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

Interstate:<br>I-90<br>Interchange: Exit 17 (Lead/Deadwood)<br>Analyst: BDW<br>Date: 8/26/2009



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 4.4\% | 5.9\% | 5.9\% | 5.9\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833/231 feet | 1910' | 1910' | 955' | 955' |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $3^{\circ}$ | $6^{\circ}$ | $6^{\circ}$ |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30 | > 30 | >30 | >30 |  |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 5.00\% | n/a | 0.56\% | 0.62\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | n/a | 5.00\% | -1.72\% | -3.03\% |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 13 | 13 | 15 | 15 | Supports Impr. |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 4 | 4 | 3 | 4 | Supports Impr. |
| Left Shoulder | 2 feet | 2 | 2 | 3 | 2 |  |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 |  |
| Minimum Off-Ramp Taper Rate | 20:1 | 40 | n/a |  | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 61 | n/a |  |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | n/a | n/a | n/a | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 93 | 209 | 263 | 110 |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 1800 | 1243 | 1662 | 490 |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 00 |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  | /a |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet |  | 39 |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | \% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | \% |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | $0^{\prime}$ |  |  | Supports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

Divided highway makes sight distance less critical (2 stage turns). Future development in vicinity - Elhorn Ridge



SDDOT Decennial Corridor, 09-104-01, 01/06/10


SDDOT Decennial Corridor, 09-104-01, 01/11/10


SDDOT Decennial Corridor, 09-104-01, 01/13/10

# I-90 EXIT 30 LAZELLE STREET 


Figure 1
I-90 Exit 30 - Lazelle Street, Sturgis

## Probable Construction Costs

 Exit 30 - Diamond Interchange| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$565,000.00 | \$565,000 |
| Traffic Control | 1 | LUMP SUM | \$1,130,000.00 | \$1,130,000 |
| Clearing | 1 | LUMP SUM | \$226,000.00 | \$226,000 |
| Removal of Concrete Pavement | 2,942 | SQ. YD. | \$3.88 | \$11,422 |
| Removal of Asphalt Pavement | 35,793 | SQ. YD. | \$7.39 | \$264,583 |
| Remove Bridge | 39,936 | SQ. FT. | \$9.00 | \$359,424 |
| Borrow, Unclassified Excavation | 47,198 | CU. YD. | \$5.30 | \$250,245 |
| Base Course | 4,200 | TON | \$10.64 | \$44,671 |
| Asphalt Composite | - | TON | \$80.91 | \$0 |
| PCC Pavement 11" (mainline) | 16,916 | SQ. YD. | \$33.12 | \$560,275 |
| PCC Pavement 8" (ramps) | 9,194 | SQ. YD. | \$43.40 | \$398,993 |
| Concrete Approach Slab | 18,600 | SQ. YD. | \$188.34 | \$3,503,161 |
| Bridges | 59,042 | SQ. FT. | \$100.00 | \$5,904,200 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$340,000.00 | \$340,000 |
| Traffic Signal | 0 | EACH | \$125,000.00 | \$0 |
| Roadway Lighting | 1 | LUMP SUM | \$230,000.00 | \$230,000 |
| Drainage (18" RCP) | 90 | LF | \$24.53 | \$2,208 |
| Subtotal |  |  |  | \$13,790,000 |
| Contingencies | 25\% |  |  | \$3,447,500 |
| Total Probable Construction Costs |  |  |  | \$17,240,000 |
| Engineering, Administration | 15\% |  |  | \$2,586,000 |
| Total Project Costs |  |  |  | \$19,830,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

Interstate: I-90<br>Interchange: 30 (Lazelle St.)<br>Analyst: BDW<br>Date: 8/26/2009



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ------ |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 2.08\% | 7.70\% | 5.00\% | 2.08\% | Supports Impr. |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | 1910' | 573' | 1910' | 5730' | Supports Impr. |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $10^{\circ}$ | $3^{\circ}$ | $1^{\circ}$ | Supports Impr. |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | > 30 | $>30$ | $>30$ | > 30 |  |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 0.74\% | 3.83\% | 2.00\% | 4.05\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -7.47\% | -3.12\% | -2.68\% | -1.66\% | Supports Impr. |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 21 | 21 | 15 | 18 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 2 | 2 | 6 | 3 | Supports Impr. |
| Left Shoulder | 2 feet | 2 | 2 | 2 | 2 |  |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 55 | n/a | 40 | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 50 | n/a | 58 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ | 46 | 184 | 279 | 99 | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | n/a | n/a | n/a | n/a |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 317 | 696 | 953 | 466 | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 19 |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ |  | 07 |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet |  | 97 |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | 3\% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | 崖\% |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | 71' |  |  | Supports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection
Comments
Recent work on ramps so inslopes should be improved




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# I-90 EXIT 40 TILFORD ROAD 

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 40 (Tilford Road) |
| Analyst: | RDG |
| Date: | $8 / 13 / 2009$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | --------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 4.2\% | 3.0\% | 4.2\% | 3.0\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | 1910' | 1910' | 1910' | 1910' |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | > 30 | >30 | > 30 | $>30$ |  |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 1.49\% | n/a | 1.20\% | n/a |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | n/a | -2.12\% | n/a | -0.16\% |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 15 | 15 | 15 | 15 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 4 | 4 | 5 | 5 | Suports Impr. |
| Left Shoulder | 2 feet | 4 | 3 | 3 | 3 |  |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Suports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 41 | n/a | 40 | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 62 | n/a | 61 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | n/a | n/a | n/a | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 198 | 280 | 200 | 1827 |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | >425 | >425 | >425 | >425 |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 2 |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ |  | 0 |  |  | Suports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  | 88 |  |  | Suports Impr. |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425/200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | \% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | \% |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | ' |  |  | Suports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments
Cross road K value appears substandard. Inslopes substandard as well?

# I-90 EXIT 46 ELK CREEK ROAD 



## Probable Construction Costs

 Exit 46 - Relocated Diamond Interchange| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$247,000.00 | \$247,000 |
| Traffic Control | 1 | LUMP SUM | \$494,000.00 | \$494,000 |
| Clearing | 1 | LUMP SUM | \$99,000.00 | \$99,000 |
| Removal of Concrete Pavement | 5,967 | SQ. YD. | \$3.88 | \$23,169 |
| Removal of Asphalt Pavement | 9,572 | SQ. YD. | \$7.39 | \$70,760 |
| Remove Bridge | 6,360 | SQ. FT. | \$9.00 | \$57,240 |
| Borrow, Unclassified Excavation | 289,249 | CU. YD. | \$5.30 | \$1,533,597 |
| Base Course | 12,119 | TON | \$10.64 | \$128,911 |
| Asphalt Composite | 15,899 | TON | \$80.91 | \$1,286,322 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) |  | SQ. YD. | \$43.40 | \$0 |
| Concrete Approach Slab | 3,600 | SQ. YD. | \$188.34 | \$678,031 |
| Bridges | 11,544 | SQ. FT. | \$100.00 | \$1,154,400 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$150,000.00 | \$150,000 |
| Traffic Signal | 0 | EACH | \$125,000.00 | \$0 |
| Roadway Lighting | 1 | LUMP SUM | \$100,000.00 | \$100,000 |
| Drainage (18" RCP) | 150 | LF | \$24.53 | \$3,680 |
| Subtotal |  |  |  | \$6,030,000 |
| Contingencies | 25\% |  |  | \$1,507,500 |
| Total Probable Construction Costs |  |  |  | \$7,540,000 |
| Engineering, Administration | 15\% |  |  | \$1,131,000 |
| Total Project Costs |  |  |  | \$8,670,000 |

## INTERCHANGE GEOMETRICS CHECKLIST

 SDDOT Interstate Corridor Study| Interstate: | l-90 |
| :--- | :---: |
| Interchange: | Exit 46 (Elk Creek Road) |
| Analyst: | RDG |
| Date: | $8 / 13 / 2009$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% |  |  |  |  |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | $310 '$ | 310' | $310 '$ | $310 '$ | Supports Impr. |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ |  |  |  |  |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 1.00\% | 1.48\% | 1.18\% | 1.13\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.00\% | -0.45\% | -1.00\% | -3.42\% |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 15 | 15 | 15 | 15 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 5 | 4 | 5 | 5 |  |
| Left Shoulder | 2 feet | 2 | 2 | 2 | 2 |  |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 17 | n/a | 17 | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 21 | n/a | 21 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  |  |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  |  |  |  |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  |  |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  |  |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | substandard | n/a | substandard | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  |  |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  |  |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300/660 feet |  |  |  |  |  |
| ** Loop ramp design speed $=30 \mathrm{mph}$ <br> ***Substandard Intersection Sight Distance locations could not be are intersections that demonstrate sight distance limitations based or Stopping Sight Distance along the crossroad approaching the in | mined from the interch general field evaluatio ction. | nge plans. Su or the presen | andard Io of a subs | tions, therefor dard k -value |  |  |

Comments
Very sharp curve on bridge over interstate...site distance from ramps poor.




LEGEND


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# I-90 EXIT 48 STAGE STOP CANYON ROAD 




## Probable Construction Costs

 Exit 48 - Relocated Diamond| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
| Mobilization |  |  |  |  |
| Traffic Control | 1 | LUMP SUM | $\$ 229,000.00$ | $\$ 229,000$ |
| Clearing | 1 | LUMP SUM | $\$ 459,000.00$ | $\$ 459,000$ |
| Removal of Concrete Pavement | 1 | LUMP SUM | $\$ 92,000.00$ | $\$ 92,000$ |
| Removal of Asphalt Pavement | 12,375 | SQ. YD. | $\$ 3.88$ | $\$ 31,103$ |
| Remove Bridge | 11,196 | SQ. FT. | $\$ 7.39$ | $\$ 91,474$ |
| Borrow, Unclassified Excavation | 49,585 | CU. YD. | $\$ 9.00$ | $\$ 100,764$ |
| Base Course | 9,405 | TON | $\$ 5.30$ | $\$ 262,898$ |
| Asphalt Composite | 16,095 | TON | $\$ 10.64$ | $\$ 100,044$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 80.91$ | $\$ 1,302,175$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| Concrete Approach Slab | 5,600 | SQ. YD. | $\$ 43.40$ | $\$ 188.34$ |
| Bridges | 16,416 | SQ. FT. | $\$ 1,054,715$ |  |
| Guard Rail | 0 | LF | $\$ 0.00$ | $\$ 1,641,600$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 140,000.00$ | $\$ 140,000$ |
| Traffic Signal | 0 | EACH | $\$ 125,000.00$ | $\$ 0$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 90,000.00$ | $\$ 90,000$ |
| Drainage (18" RCP) | 120 | LF | $\$ 24.53$ | $\$ 2,944$ |
|  |  |  |  | $\$ 5,600,000$ |
| Subtotal |  |  |  | $\$ 1,400,000$ |
| Contingencies |  |  |  |  |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  | $\$ 7,000,000$ |  |
| Total Project Costs |  |  | $\$ 1,050,000$ |  |



## Probable Construction Costs Exit 48 - Single Point Interchange

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$336,000.00 | \$336,000 |
| Traffic Control | 1 | LUMP SUM | \$671,000.00 | \$671,000 |
| Clearing | 1 | LUMP SUM | \$134,000.00 | \$134,000 |
| Removal of Concrete Pavement | 15,522 | SQ. YD. | \$3.88 | \$60,271 |
| Removal of Asphalt Pavement | 17,948 | SQ. YD. | \$7.39 | \$132,670 |
| Remove Bridge | 9,864 | SQ. FT. | \$9.00 | \$88,776 |
| Borrow, Unclassified Excavation | 62,294 | CU. YD. | \$5.30 | \$330,281 |
| Base Course | 11,816 | TON | \$10.64 | \$125,685 |
| Asphalt Composite | 15,287 | TON | \$80.91 | \$1,236,808 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) |  | SQ. YD. | \$43.40 | \$0 |
| Concrete Approach Slab | 7,200 | SQ. YD. | \$188.34 | \$1,356,062 |
| Bridges | 33,784 | SQ. FT. | \$100.00 | \$3,378,400 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$200,000.00 | \$200,000 |
| Traffic Signal | 1 | EACH | \$125,000.00 | \$125,000 |
| Roadway Lighting | 1 | LUMP SUM | \$130,000.00 | \$130,000 |
| Drainage (18" RCP) | 120 | LF | \$24.53 | \$2,944 |
| Subtotal |  |  |  | \$8,310,000 |
| Contingencies | 25\% |  |  | \$2,077,500 |
| Total Probable Construction Costs |  |  |  | \$10,390,000 |
| Engineering, Administration | 15\% |  |  | \$1,558,500 |
| Total Project Costs |  |  |  | \$11,950,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

Interstate: l-90<br>Interchange: Exit 48 (Stage Stop Canyon Rd)<br>Analyst: RDG<br>Date: 8/13/2009



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% |  |  |  |  |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833/231 feet | 310' | 310' | 310' | 310' | Supports Impr. |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ |  |  |  |  |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 0.34\% | 2.46\% | 2.13\% | n/a |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.73\% | -2.45\% | -0.28\% | -3.90\% |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 15 | 15 | 15 | 15 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3 | 4 | 5 | 3 |  |
| Left Shoulder | 2 feet | 3 | 3 | 4 | 4 |  |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 17 | n/a | 17 | n/a | Supports Impr. |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 21 | n/a | 21 | Supports Impr. |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | n/a | n/a | 235 | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 110 | n/a | n/a | 130 |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 698' | $>425$ | 1,369' | 412' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 59 |  |  | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  | 66 |  |  | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  | 93' |  |  | Supports Impr. |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425/200 feet |  | n/a |  | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | 0\% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | 0\% |  |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | 660 |  |  |  |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments
Inslopes poor?


SDDOT Decennial Corridor, 09-104-01, 12/22/09


$$
x x x(x X X)=A M(P M) \text { Peak Hour Traffic Volumes (vph) }
$$

## LEGEND

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# I-90 EXIT 55 DEADWOOD AVENUE 


$\downarrow$ Əınb!」
I-90 Exit 55 - Deadwood Avenue, Rapid City
Bridge Widening

## Probable Construction Costs

## Exit 55 - Bridge Widening \& Turn Lanes

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$126,000.00 | \$126,000 |
| Traffic Control | 1 | LUMP SUM | \$252,000.00 | \$252,000 |
| Clearing | 1 | LUMP SUM | \$50,000.00 | \$50,000 |
| Removal of Concrete Pavement | - | SQ. YD. | \$3.88 | \$0 |
| Removal of Asphalt Pavement | - | SQ. YD. | \$7.39 | \$0 |
| Remove Bridge | - | SQ. FT. | \$9.00 | \$0 |
| Borrow, Unclassified Excavation | 2,086 | CU. YD. | \$5.30 | \$11,062 |
| Base Course | 1,317 | TON | \$10.64 | \$14,014 |
| Asphalt Composite | 1,317 | TON | \$80.91 | \$106,590 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) | 5,208 | SQ. YD. | \$43.40 | \$226,001 |
| Concrete Approach Slab | 3,600 | SQ. YD. | \$188.34 | \$678,031 |
| Bridges | 14,828 | SQ. FT. | \$100.00 | \$1,482,800 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$80,000.00 | \$80,000 |
| Traffic Signal | 0 | EACH | \$125,000.00 | \$0 |
| Roadway Lighting | 1 | LUMP SUM | \$50,000.00 | \$50,000 |
| Drainage (18" RCP) | 90 | LF | \$24.53 | \$2,208 |
| Subtotal |  |  |  | \$3,080,000 |
| Contingencies | 25\% |  |  | \$770,000 |
| Total Probable Construction Costs |  |  |  | \$3,850,000 |
| Engineering, Administration | 15\% |  |  | \$577,500 |
| Total Project Costs |  |  |  | \$4,430,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 55 |
| Analyst: | RDG |
| Date: | $8 / 13 / 2009$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ----- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 2\% | 2\% | 2\% | 2\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | - | - | - | - |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | - | - | - | - |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | > 30 | >30 | $>30$ | > 30 |  |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 4.95\% | n/a | 1.82\% | 3.00\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | n/a | -5.58\% | -3.00\% | n/a | Supports Impr. |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | 18-20 | 18 | 12 | 18 | Supports Impr. |
| As Single Lane | 15 feet (19 for loops) |  |  |  |  |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 8 | 8 | 8 | 8 |  |
| Left Shoulder | 2 feet | 2 | 2 | 2 | 2 |  |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 |  |  |  |  |  |
| Minimum On-Ramp Taper Rate | 50:1 |  |  |  |  |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | n/a | n/a | n/a | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 76 | 46 | 135 | 141 |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 360' | 246' | 576' | 711' |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 56 |  |  | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ |  | 06 |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $425 / 200$ feet |  | 60 |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | 8\% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | 0\% |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | 50' |  |  |  |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection
Comments
A lot of truck traffic. Thru-left and right turn lanes for off ramps.




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# I-90 EXIT 59 LACROSSE STREET 

<13

8

## Probable Construction Costs

Exit 59 - New Bridge \& Turn Lanes

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$204,000.00 | \$204,000 |
| Traffic Control | 1 | LUMP SUM | \$409,000.00 | \$409,000 |
| Clearing | 1 | LUMP SUM | \$82,000.00 | \$82,000 |
| Removal of Concrete Pavement | - | SQ. YD. | \$3.88 | \$0 |
| Removal of Asphalt Pavement | - | SQ. YD. | \$7.39 | \$0 |
| Remove Bridge | 6,360 | SQ. FT. | \$9.00 | \$57,240 |
| Borrow, Unclassified Excavation | 850 | CU. YD. | \$5.30 | \$4,508 |
| Base Course | 671 | TON | \$10.64 | \$7,139 |
| Asphalt Composite | - | TON | \$80.91 | \$0 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) | 2,193 | SQ. YD. | \$43.40 | \$95,185 |
| Concrete Approach Slab | 8,000 | SQ. YD. | \$188.34 | \$1,506,736 |
| Bridges | 24,160 | SQ. FT. | \$100.00 | \$2,416,000 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$120,000.00 | \$120,000 |
| Traffic Signal | 0 | EACH | \$125,000.00 | \$0 |
| Roadway Lighting | 1 | LUMP SUM | \$80,000.00 | \$80,000 |
| Drainage (18" RCP) | 30 | LF | \$24.53 | \$736 |
| Subtotal |  |  |  | \$4,980,000 |
| Contingencies | 25\% |  |  | \$1,245,000 |
| Total Probable Construction Costs |  |  |  | \$6,230,000 |
| Engineering, Administration | 15\% |  |  | \$934,500 |
| Total Project Costs |  |  |  | \$7,160,000 |



## Probable Construction Costs Exit 59 - Single Point Interchange

|  | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
| Item Description |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 408,000.00$ | $\$ 408,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 817,000.00$ | $\$ 817,000$ |
| Clearing | 1 | LUMP SUM | $\$ 163,000.00$ | $\$ 163,000$ |
| Removal of Concrete Pavement | 6,105 | SQ. YD. | $\$ 3.88$ | $\$ 23,706$ |
| Removal of Asphalt Pavement | 4,070 | SQ. YD. | $\$ 7.39$ | $\$ 30,085$ |
| Remove Bridge | 24,500 | SQ. FT. | $\$ 9.00$ | $\$ 220,500$ |
| Borrow, Unclassified Excavation | 65,558 | CU. YD. | $\$ 5.30$ | $\$ 347,587$ |
| Base Course | 12,435 | TON | $\$ 10.64$ | $\$ 132,271$ |
| Asphalt Composite | - | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) | 28,001 | SQ. YD. | $\$ 43.40$ | $\$ 1,215,103$ |
| Concrete Approach Slab | 8,400 | SQ. YD. | $\$ 188.34$ | $\$ 1,582,073$ |
| Bridges | 46,149 | SQ. FT. | $\$ 100.00$ | $\$ 4,614,900$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 250,000.00$ | $\$ 250,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 160,000.00$ | $\$ 160,000$ |
| Drainage (18" RCP) | 150 | LF | $\$ 24.53$ | $\$ 3,680$ |
| Subtotal |  |  |  | $\$ 10,090,000$ |
|  |  |  |  | $\$ 2,522,500$ |
| Contingencies | $25 \%$ |  |  | $\$ 12,610,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 1,891,500$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

Interstate: I-90<br>Interchange: Exit 59 (Lacrosse St)<br>Analyst: RDG<br>Date: 8/13/2009



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 2\% | 2\% | 2\% | 2\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833/231 feet | - | - | - | - |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | - | - | - | - |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | > 30 | > 30 | > 30 | > 30 |  |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 3.13\% | n/a | 3.00\% | 1.07\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | n/a | -5.58\% | -1.07\% | -2.00\% | Supports Impr. |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | 18 | 15 | 18 | 15 |  |
| As Single Lane | 15 feet (19 for loops) |  |  |  |  |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 2 | 3 | 3 | 5 | Supports Impr. |
| Left Shoulder | 2 feet | 2 | 2 | 3 | 2 |  |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 |  |  |  |  |  |
| Minimum On-Ramp Taper Rate | 50:1 |  |  |  |  |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | n/a | n/a | n/a | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 137$ |  | 85 | 49 | 188 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet |  | 713 | 262 | >425 |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/137 |  |  |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  |  |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425/200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  |  |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  |  |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  |  |  |  | Supports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection.

Busy interchange. It appears no recent changes have been made.


LEGEND

$$
X X X(X X X)=A M(P M) \text { Peak Hour Traffic Volumes (vph) }
$$



SDDOT Decennial Corridor, 09-104-01, 01/14/10


LEGEND

$$
X X X(X X X)=A M(P M) \text { Peak Hour Traffic Volumes (vph) }
$$



SDDOT Decennial Corridor, 09-104-01, 01/14/10


LEGEND

$$
X X X(X X X)=A M(P M) \text { Peak Hour Traffic Volumes (vph) }
$$



SDDOT Decennial Corridor, 09-104-01, 01/14/10

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## I-90 EXIT 63 BOX ELDER / ELLSWORTH AFB




## Probable Construction Costs

Exit 63 - New Diamond

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
| Mobilization |  |  |  |  |
| Traffic Control | 1 | LUMP SUM | $\$ 248,000.00$ | $\$ 248,000$ |
| Clearing | 1 | LUMP SUM | $\$ 496,000.00$ | $\$ 496,000$ |
| Removal of Concrete Pavement | 1 | LUMP SUM | $\$ 99,000.00$ | $\$ 99,000$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Remove Bridge | 5,372 | SQ. YD. | $\$ 7.39$ | $\$ 39,710$ |
| Borrow, Unclassified Excavation | 6,360 | SQ. FT. | $\$ 9.00$ | $\$ 57,240$ |
| Base Course | 298,727 | CU. YD. | $\$ 5.30$ | $\$ 1,583,853$ |
| Asphalt Composite | 9,297 | TON | $\$ 10.64$ | $\$ 98,896$ |
| PCC Pavement 11" (mainline) | 11,751 | TON | $\$ 80.91$ | $\$ 950,720$ |
| PCC Pavement 8" (ramps) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| Concrete Approach Slab |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Bridges | 3,600 | SQ. YD. | $\$ 188.34$ | $\$ 678,031$ |
| Guard Rail | 15,496 | SQ. FT. | $\$ 100.00$ | $\$ 1,549,600$ |
| Permanent Signing/Markings | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Traffic Signal | 1 | LUMP SUM | $\$ 150,000.00$ | $\$ 150,000$ |
| Roadway Lighting | 0 | EACH | $\$ 125,000.00$ | $\$ 0$ |
| Drainage (18" RCP) | 1 | LUMP SUM | $\$ 100,000.00$ | $\$ 100,000$ |
|  | 240 | LF | $\$ 24.53$ | $\$ 5,887$ |
| Subtotal |  |  |  | $\$ 6,060,000$ |
| Contingencies |  |  |  | $\$ 1,515,000$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 7,580,000$ |
| Total Project Costs |  |  |  | $\$ 1,137,000$ |

## Probable Construction Costs

 Exit 63 - Flyover| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 377,000.00$ | $\$ 377,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 754,000.00$ | $\$ 754,000$ |
| Clearing | 1 | LUMP SUM | $\$ 151,000.00$ | $\$ 151,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | 27,680 | SQ. YD. | $\$ 7.39$ | $\$ 204,611$ |
| Remove Bridge | 13,400 | SQ. FT. | $\$ 9.00$ | $\$ 120,600$ |
| Borrow, Unclassified Excavation | 213,484 | CU. YD. | $\$ 5.30$ | $\$ 1,131,895$ |
| Base Course | 8,945 | TON | $\$ 10.64$ | $\$ 95,145$ |
| Asphalt Composite | 18,854 | TON | $\$ 80.91$ | $\$ 1,525,410$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Concrete Approach Slab | 2,400 | SQ. YD. | $\$ 188.34$ | $\$ 452,021$ |
| Bridges | 40,040 | SQ. FT. | $\$ 100.00$ | $\$ 4,004,000$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 230,000.00$ | $\$ 230,000$ |
| Traffic Signal | 0 | EACH | $\$ 125,000.00$ | $\$ 0$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 150,000.00$ | $\$ 150,000$ |
| Drainage (18" RCP) | 240 | LF | $\$ 24.53$ | $\$ 5,887$ |
| Subtotal |  |  |  | $\$ 9,200,000$ |
|  |  |  |  | $\$ 2,300,000$ |
| Contingencies | $25 \%$ |  |  | $\$ 11,500,000$ |
|  |  |  |  | $\$ 1,725,000$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 63 (Dusters corner) |
| Analyst: | RDG |
| Date: | $8 / 13 / 2009$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph} * *$ |  |  |  |  |  |
| Number of Lanes |  | - | - |  |  |  |
| Right Turn Storage Length |  | - | - |  |  |  |
| Left Turn Storage Length |  | - | - |  |  |  |
| Superelevation (e max) | 6\% | - | - | 4.0\% | 5.0\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | - | - | 2589' | 955' |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | - | - | $2^{\circ} 12^{\prime}$ | $6^{\circ}$ |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | - | - | 3:1 | 3:1 |  |
| Maximum Grade on Ramp (Ascending) | $+3 \%$ to $+5 \%$ | - | - | n/a | 4.00\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | - | -0.67\% | -4.00\% |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - |  |  |  |
| As Single Lane | 15 feet (19 for loops) | - | - | 15 | 15-18 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | - | - | 8 | 2 to 8 | Supports Impr. |
| Left Shoulder | 2 feet | - | - | 8 | 2 to 8 | Supports Impr. |
| Inslope | 6:1 | - | - | 6:1 | 6:1 |  |
| Minimum Off-Ramp Taper Rate | 20:1 | - | - |  | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | - | - | n/a | 58 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | - | - | n/a | n/a |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 137$ | - | - | 563 | 93 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | - | - | >425 | 414' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/137 |  |  |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  |  |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425/200 feet |  |  |  |  |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  |  |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  |  |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  |  |  |  |  |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection
Comments




## LEGEND

XXX = Design Hour Traffic Volumes (vph)


# I-190 EXIT 1 NORTH STREET / SILVER STREET 



## Probable Construction Costs

 Exit 1 - Roundabout| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$13,000.00 | \$13,000 |
| Traffic Control | 1 | LUMP SUM | \$27,000.00 | \$27,000 |
| Clearing | 1 | LUMP SUM | \$5,000.00 | \$5,000 |
| Removal of Concrete Pavement | - | SQ. YD. | \$3.88 | \$0 |
| Removal of Asphalt Pavement | 21,760 | SQ. YD. | \$7.39 | \$160,850 |
| Remove Bridge | - | SQ. FT. | \$9.00 | \$0 |
| Borrow, Unclassified Excavation | 5,217 | CU. YD. | \$5.30 | \$27,662 |
| Base Course |  | TON | \$10.64 | \$0 |
| Asphalt Composite | 950 | TON | \$80.91 | \$76,863 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) |  | SQ. YD. | \$43.40 | \$0 |
| Concrete Approach Slab | - | SQ. YD. | \$188.34 | \$0 |
| Bridges | - | SQ. FT. | \$100.00 | \$0 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Roundabout (Single Lane) | 1 | EACH | \$600,000.00 | \$600,000 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Traffic Signal | 0 | EACH | \$125,000.00 | \$0 |
| Roadway Lighting | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Drainage (18" RCP) | 120 | LF | \$24.53 | \$2,944 |
| Subtotal |  |  |  | \$930,000 |
| Contingencies | 25\% |  |  | \$232,500 |
| Total Probable Construction Costs |  |  |  | \$1,160,000 |
| Engineering, Administration | 15\% |  |  | \$174,000 |
| Total Project Costs |  |  |  | \$1,330,000 |



## Probable Construction Costs

## Exit 1 - Signal \& Bridge Removal

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 36,000.00$ | $\$ 36,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 72,000.00$ | $\$ 72,000$ |
| Clearing | 1 | LUMP SUM | $\$ 14,000.00$ | $\$ 14,000$ |
| Removal of Concrete Pavement | 6,127 | SQ. YD. | $\$ 3.88$ | $\$ 23,790$ |
| Removal of Asphalt Pavement | 9,679 | SQ. YD. | $\$ 7.39$ | $\$ 71,548$ |
| Remove Bridge | 21,600 | SQ. FT. | $\$ 9.00$ | $\$ 194,400$ |
| Borrow, Unclassified Excavation | 5,719 | CU. YD. | $\$ 5.30$ | $\$ 30,322$ |
| Base Course | - | TON | $\$ 10.64$ | $\$ 0$ |
| Asphalt Composite | 2,049 | TON | $\$ 80.91$ | $\$ 165,797$ |
| PCC Pavement 11" (mainline) | 7,080 | SQ. YD. | $\$ 33.12$ | $\$ 234,497$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 20,000.00$ | $\$ 20,000$ |
| Traffic Signal | 2 | EACH | $\$ 125,000.00$ | $\$ 250,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Drainage (18" RCP) | 120 | LF | $\$ 24.53$ | $\$ 2,944$ |
| Subtotal |  |  |  | $\$ 1,130,000$ |
|  |  |  |  |  |
| Contingencies | $25 \%$ |  |  | $\$ 282,500$ |
| Total Probable Construction Costs |  |  |  | $\$ 1,410,000$ |
| Engineering, Administration | $15 \%$ |  |  | $\$ 211,500$ |



## Probable Construction Costs

## Exit 1 - Two Lane Roundabout

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$23,000.00 | \$23,000 |
| Traffic Control | 1 | LUMP SUM | \$47,000.00 | \$47,000 |
| Clearing | 1 | LUMP SUM | \$9,000.00 | \$9,000 |
| Removal of Concrete Pavement | 6,127 | SQ. YD. | \$3.88 | \$23,790 |
| Removal of Asphalt Pavement | 4,938 | SQ. YD. | \$7.39 | \$36,500 |
| Remove Bridge | 21,600 | SQ. FT. | \$9.00 | \$194,400 |
| Borrow, Unclassified Excavation | 17,239 | CU. YD. | \$5.30 | \$91,404 |
| Base Course | - | TON | \$10.64 | \$0 |
| Asphalt Composite | 1,473 | TON | \$80.91 | \$119,138 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) |  | SQ. YD. | \$43.40 | \$0 |
| Concrete Approach Slab | - | SQ. YD. | \$188.34 | \$0 |
| Bridges | - | SQ. FT. | \$100.00 | \$0 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Roundabout (2 Lane) | 1 | EACH | \$1,500,000.00 | \$1,500,000 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Traffic Signal | 1 | EACH | \$125,000.00 | \$125,000 |
| Roadway Lighting | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Drainage (18" RCP) | 120 | LF | \$24.53 | \$2,944 |
| Subtotal |  |  |  | \$2,190,000 |
| Contingencies | 25\% |  |  | \$547,500 |
| Total Probable Construction Costs |  |  |  | \$2,740,000 |
| Engineering, Administration | 15\% |  |  | \$411,000 |
| Total Project Costs |  |  |  | \$3,150,000 |








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## PIERRE REGION

Interstate 90, MRM 130.0 to MRM 251.00
Total Interchanges: 22
Studied Interchanges: 22

| Deficient Interchanges (2): | $\underline{\text { Page }}$ |
| :---: | :---: |
| I-90 Exit 172 | A-103 |
| I-90 Exit 235 | A-105 |

## Summary of Mainline Segment Geometric Performance Pierre Region

| 1－90 |  | 言 <br> 言 <br> 苟 <br> 立 |  |  |  | $\begin{aligned} & 0 \\ & \underset{\Sigma}{\hat{E}} \\ & \text { N } \\ & \text { む̀ } \\ & \text { O} \\ & 0 \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MP 142－149 | 12 | 10 | 4 |  | $1^{\circ} 00^{\prime}$ | 3：1 | 5：1 |  | 38 | n／a | n／a | 3．00\％ |
| MP 149－159 | 12 | 10 | 4 |  | $0^{\circ} 45^{\prime}$ | 3：1 | 5：1 |  | 38 | 38 | 16＇7＂ | 1．71\％ |
| MP 159－165 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | 3：1 | 5：1 | 3．7\％ | 38 | 38 | n／a | 2．92\％ |
| MP 165－174 | 12 | 10 | 4 | 65 | $0^{\circ} 45^{\prime}$ | 3：1 | 5：1 | 2．7\％ | 38 | 38 | n／a | 2．83\％ |
| MP 174－182 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．7\％ | 38 | 38 | 16＇5＂ | 3．00\％ |
| MP 182－189 | 12 | 10 | 4 | 75 | $0^{\circ} 45^{\prime}$ | ＞ 30 | 6：1 | 3．0\％ | 38 | 38 | n／a | 3．00\％ |
| MP 189－198 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．7\％ | 38 | n／a | 15＇ 6 ＂ | 3．00\％ |
| MP 198－206 | 12 | 10 | 4 | 65 | n／a | ＞ 30 | 6：1 | n／a | 38 | 38 | n／a | 2．21\％ |
| MP 206－213 | 12 | 10 | 4 |  | $0^{\circ} 06^{\prime}$ | ＞ 30 | 6：1 |  | 38 | 38 | 17＇2＂ | 3．00\％ |
| MP 213－219 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．7\％ | 38 | 38 | n／a | 3．00\％ |
| MP 219－227 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．7\％ | 38 | 38 | n／a | 2．13\％ |
| MP 227－236 | 12 | 10 | 4 | 75 | $0^{\circ} 45^{\prime}$ | $>30$ | 6：1 | 3．0\％ | 38 | 38 | n／a | 2．75\％ |
| MP 236－243 | 12 | 10 | 4 |  | $0^{\circ} 45^{\prime}$ | ＞ 30 | 6：1 |  | 38 | 38 | n／a | 3．00\％ |
| MP 243－251 | 12 | 10 | 4 | 65 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．1\％ | 38 | 38 | n／a | 1．24\％ |

## LEGEND：

Existing Value does not meet standard criteria
Mainline section recently reconstructed

Summary of Mainline Segments, Traffic Volumes and Levels of Service Pierre Region

| I-90 Exits: | Current Lanes | Existing |  | 2020 |  | 2030 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AADT | LOS | AADT | LOS | AADT | LOS |
| 131 to 143 | 4 | 5,920 | A | 6,234 | A | 6,509 | A |
| 143 to 150 | 4 | 6,170 | A | 6,497 | A | 6,784 | A |
| 150 to 152 | 4 | 6,220 | A | 6,550 | A | 6,838 | A |
| 152 to 163 | 4 | 6,070 | A | 6,392 | A | 6,674 | A |
| 163 to 170 | 4 | 5,920 | A | 6,234 | A | 6,509 | A |
| 170 to 172 | 4 | 5,990 | A | 6,308 | A | 6,586 | A |
| 172 to 177 | 4 | 5,680 | A | 5,697 | A | 5,711 | A |
| 177 to 183 | 4 | 5,990 | A | 6,008 | A | 6,023 | A |
| 183 to 191 | 4 | 5,980 | A | 5,998 | A | 6,013 | A |
| 191 to 192 | 4 | 6,110 | A | 6,128 | A | 6,144 | A |
| 192 to 201 | 4 | 6,550 | A | 6,570 | A | 6,586 | A |
| 201 to 208 | 4 | 5,250 | A | 5,266 | A | 5,279 | A |
| 208 to 212 | 4 | 5,260 | A | 5,367 | A | 5,457 | A |
| 212 to 214 | 4 | 6,260 | A | 6,387 | A | 6,495 | A |
| 214 to 220 | 4 | 6,120 | A | 6,244 | A | 6,349 | A |
| 220 to 225 | 4 | 5,960 | A | 6,081 | A | 6,183 | A |
| 225 to 226 | 4 | 6,260 | A | 6,387 | A | 6,495 | A |
| 226 to 235 | 4 | 6,470 | A | 6,601 | A | 6,712 | A |
| 235 to 241 | 4 | 6,010 | A | 6,132 | A | 6,235 | A |
| 241 to 248 | 4 | 6,180 | A | 6,305 | A | 6,412 | A |
| 248 to 251 | 4 | 6,630 | A | 6,764 | A | 6,878 | A |

Structurally Deficient and Functionally Obsolete Mainline Structure Summary- Pierre Region

| I-90 MRM 130.3 to 251 | Number of Bridges | Length | $\begin{aligned} & \hline \text { Existing Deck } \\ & \text { Out-to-Out } \\ & \text { Width } \end{aligned}$ | Existing Area | Unit Price | $\begin{aligned} & \text { Removal } \\ & \text { Cost } \\ & \hline \end{aligned}$ | Proposed Deck Clear Roadway Width | $\begin{gathered} \text { Proposed } \\ \text { Area } \\ \hline \end{gathered}$ | Unit Price | Bridge Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cactus Flat Interchange (Exit 131) over I-90 at MRM 131.27 (Structurally Deficient) | 1 | 307 | 47 | 14,342 | \$9 | \$129,074 | 40 | 12,284 | \$100 | \$1,228,400 |
| I-90 over Brave Bull Road at MRM 164.43 (Functionally Obsolete-LOW CLEARANCE) | 2 | 80 | 41 | 6,512 | \$9 | \$58,608 | 40 | 6,400 | \$100 | \$640,000 |
| 256 th Ave over I-90 at MRM 177.48 (Structurally Deficient) | 2 | 304 | 31 | 18,938 | \$9 | \$170,446 | 32 | 19,424 | \$100 | \$1,942,400 |
| SD 248 (Murdo Exit 191) over I-90 at MRM 191.15 (Structurally Deficient) | 1 | 432 | 39 | 16,707 | \$9 | \$150,361 | 32 | 13,814 | \$100 | \$1,381,440 |
| I-90 over 242nd St at MRM 194.81 (Functionally Obsolete-LOW CLEARANCE) | 2 | 80 | 41 | 6,512 | \$9 | \$58,608 | 40 | 6,400 | \$100 | \$640,000 |
| I-90 WB over 300th Ave (Exit 220) at MRM 220.31 (Structurally Deficient) | 1 | 158 | 41 | 6,443 | \$9 | \$57,985 | 40 | 6,332 | \$100 | \$633,200 |


|  |  | Geometric Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Crashes, 2006-2009 |  |  |  |  |  |  | 2009/2020/2030 Level of Service |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-90 | Location |  |  |  |  |  |  |  |  | $\begin{gathered} \overline{\stackrel{\rightharpoonup}{e}} \\ \stackrel{\rightharpoonup}{\circ} \\ \stackrel{\stackrel{\rightharpoonup}{0}}{\stackrel{\omega}{0}} \end{gathered}$ |  |  |  |  |  |  |  |  |  |  | $\underset{\underline{E}}{\stackrel{\rightharpoonup}{E}}$ | 음 | $\begin{array}{\|l\|} \hline \stackrel{y}{\circ} \\ \stackrel{y}{\circ} \end{array}$ |  |  |  |  |  |  | $\begin{aligned} & \stackrel{\otimes}{0} \\ & \sum_{\infty}^{\infty} \\ & \underset{\infty}{\infty} \\ & \stackrel{\infty}{\infty} \end{aligned}$ |  |  |
| Exit 131 | Cactus Flat/Badlands Loop |  |  |  |  |  | 15.0' | $1.0{ }^{\prime}$ | $2.0{ }^{\prime}$ |  |  |  |  |  |  |  |  |  |  | 0 | 0 | 3 | 3 | 3 | 0.39 | 97 |  |  |  |  |  |  |
| Exit 143 | Philip | 4.4\% | 1910' | $3^{\circ} 00^{\prime}$ | < 30 " | 3.2\% | 15.0' | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 4:1 | 40 | 60 | 143 | 666 | $>425$ | 365 | 879 | 1.1\% | $228{ }^{\prime}$ | 0 | 0 | 5 | 5 | 5 | 0.70 | 65 |  |  |  |  |  |  |
| Exit 150 | Kadoka | 3.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.4\% | 18.0' | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 5:1 | 40 | 61 | 163 | 975 | $>425$ | 78 | 819 | 2.9\% | 354' | 0 | 1 | 1 | 2 | 4 | 0.43 | 94 |  |  |  |  |  |  |
| Exit 152 | Kadoka | 3.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.0\% | 19.0' | $2.0{ }^{\prime}$ | 1.0 | 5:1 | 40 | 61 | 134 | 561 | $>425$ | n/a | n/a | 0.4\% | $467{ }^{\prime}$ | 0 | 0 | 0 | 0 | 0 | 0.00 | 124 |  |  |  |  |  |  |
| Exit 163 | Belvidere | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.5\% | 15.0' | 0.0 | $1.0^{\prime}$ | 5:1 | 40 | 61 | 159 | 729 | $>425$ | 696 | 1339 | 0.9\% | 250' | 0 | 1 | 5 | 6 | 8 | 1.13 | 41 |  |  |  |  |  |  |
| Exit 170 | Midand | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > $0^{\prime}$ | 3.4\% | 14.0' | $1.0^{\prime}$ | 1.0' | 5:1 | 40 | 61 | 242 | 799 | $>425$ | n/a | n/a | n/a | 270' | 0 | 1 | 5 | 6 | 8 | 1.05 | 43 |  |  |  |  |  |  |
| Exit 172 | Midland | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.5\% | 15.0' | $1.0^{\prime}$ | 1.0' | 5:1 | 32 | 60 | 127 | 528 | $>425$ | 19 | 538 | 4.1\% | 120' | 1 | 0 | 4 | 5 | 16 | 2.47 | 5 |  |  |  |  |  |  |
| Exit 177 | Stanford Rd | 5.4\% | 1910' | $3^{\circ} 00^{\prime}$ | > $0^{\prime}$ | 4.3\% | 16.0' | $2.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 42 | 63 | 134 | 574 |  |  |  |  | 470' | 0 | 1 | 1 | 2 | 4 | 0.62 | 72 |  |  |  |  |  |  |
| Exit 183 | Okaton | 4.4\% | 1910' | $3^{\circ} 00^{\prime}$ | > $0^{\prime}$ | 2.4\% | 17.0' | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 80 | 439 | > 425 | 69 | 366 | 7.3\% | 180' | 0 | 0 | 2 | 2 | 2 | 0.29 | 105 |  |  |  |  |  |  |
| Exit 191 | Murdo | 4.6\% | 1910' | $3^{\circ} 00^{\prime}$ | > $0^{\prime}$ | 3.4\% | 18.0' | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 148 | 775 | sub | 163 | 592 | 3.9\% | > 660' | 0 | 0 | 2 | 2 | 2 | 0.27 | 108 |  |  |  |  |  |  |
| Exit 192 | Murdo/White River | 4.4\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.2\% | 19.0' | $2.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 94 | 420 | $>425$ | 286 | 819 | 3.7\% | 250' | 0 | 0 | 5 | 5 | 5 | 0.38 | 98 | Not | uated | o in | hang | creen | ethod |
| Exit 201 | Draper | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.9\% | 16.0' | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 112 | 503 | $>425$ | n/a | n/a | 1.3\% | 334' | 0 | 1 | 3 | 4 | 6 | 0.87 | 55 |  |  |  |  |  |  |
| Exit 208: | 286th Ave | 4.4\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.4\% | 15.0' | $3.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | 6:1 |  |  | 150 | 568 |  | 294 | 797 | 3.7\% | > 660' | 0 | 0 | 0 | 0 | 0 | 0.00 | 125 |  |  |  |  |  |  |
| Exit 212 | Pierre/Ft. Pierre | 5.6\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 4.2\% | 15.0' | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 131 | 576 | $>425$ | 591 | >425 | 1.5\% | $>660^{\prime}$ | 0 | 1 | 3 | 4 | 6 | 0.63 | 71 |  |  |  |  |  |  |
| Exit 214 | Vivian | 4.4\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.5\% | 19.0' | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 111 | 489 | $>425$ | 197 | 791 | 5.5\% | 400' | 0 | 1 | 7 | 8 | 10 | 1.45 | 26 |  |  |  |  |  |  |
| Exit 220 | 300th Ave | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 4.1\% | 17.0' | 2.0 | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 98 | 464 | $>425$ | 93 | 598 | 6.0\% | 190' | 0 | 0 | 3 | 3 | 3 | 0.44 | 91 |  |  |  |  |  |  |
| Exit 225 | Presho | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 4.4\% | 18.0' | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 134 | 537 | $>425$ | 383 | 14215 | 2.1\% | 450' | 0 | 0 | 2 | 2 | 2 | 0.27 | 107 |  |  |  |  |  |  |
| Exit 226 | Presho/Winner |  |  | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ |  | 19.0' | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 |  |  | $>425$ |  |  |  | 250' | 0 | 1 | 1 | 2 | 4 | 0.49 | 84 |  |  |  |  |  |  |
| Exit 235 | Kennebec | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > ${ }^{\prime}$ ' | 4.7\% | 14.0' | $5.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 61 | 90 | 442 | $>425$ | 112 | 500 | 5.4\% | $235{ }^{\prime}$ | 1 | 2 | 2 | 5 | 20 | 2.45 | 6 |  |  |  |  |  |  |
| Exit 241 | Lyman |  | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ |  | 17.0' | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 |  |  | $>425$ | 529 | $>425$ | 0.7\% | $>660^{\prime}$ | 0 | 1 | 2 | 3 | 5 | 0.73 | 62 |  |  |  |  |  |  |
| Exit 248 | Reliance/Lower Brule | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 3.0\% | 15.0' | $3.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 |  |  |  |  | $>425$ | 299 | 1246 | 2.1\% |  | 0 | 0 | 4 | 4 | 4 | 0.48 | 86 |  |  |  |  |  |  |
| Exit 251 | Gregory/Winner | 4.2\% |  | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.9\% | $15.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | 6:1 | 40 | 58 | 77 | 427 | $>425$ | n/a | n/a | 0.7\% | 250' | 0 | 0 | 3 | 3 | 3 | 0.31 | 103 |  |  |  |  |  |  |

Legend
Existing value does not meet standard criteria

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South Dakota Decennial Interstate Corridor Study

PHASEONE REPORT

## I-90 EXIT 172 STAMFORD

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 172 |
| Analyst: | BDW |
| Date: | $8 / 28 / 2009$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 4.2\% | 4.2\% | 4.2\% | 4.2\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | 1910' | 1910' | 1910' | 1910' |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | > 30 | > 30 | >30 | $>30$ |  |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 1.26\% | 1.00\% | 1.86\% | 2.28\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.48\% | -1.63\% | -0.28\% | -2.20\% |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 15 | 17 | 17 | 17 |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 1 | 1 | 2 | 4 | Supports Impr. |
| Left Shoulder | 2 feet | 1 | 2 | 2 | 4 | Supports Impr. |
| Inslope | 6:1 | 5:1 | 5:1 | 5:1 | 5:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 32 | n/a | 42 | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 87 | n/a | 60 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | 127 | 190 | 280 | 179 |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | n/a | n/a | n/a | n/a |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 528 | 659 | 803 | 641 |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 34 |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  | 19 |  |  | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $425 / 200$ feet |  | 38 |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | 1\% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | 9\% |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | 20' |  |  | Supports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection
Comments
Paved shoulders have steep slope
Inslopes a little steep
Sight distance not good from stop bars on off ramps but ok if pull forward


South Dakota Decennial Interstate Corridor Study

PHASEONE REPORT

## I-90 EXIT 235 KENNEBEC

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

Interstate:<br>1-90<br>Interchange: Exit 235 (Kennebec)<br>Analyst: BDW<br>Date: 8/31/2009



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  |  |  |  |  |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 5.0\% | 3.0\% | 5.0\% | 3.0\% |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $833 / 231$ feet | 1910' | 1910' | 1910' | 1910' |  |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ |  |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30 | $>30$ | $>30$ | > 30 |  |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 0.65\% | n/a | n/a | 4.74\% |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -1.78\% | -1.31\% | -1.68\% | n/a |  |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 14 | 16 | 15 | 14 | Supports Impr. |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 6 | 6 | 6 | 5 | Supports Impr. |
| Left Shoulder | 2 feet | 4 | 3 | 4 | 4 |  |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 |  |
| Minimum Off-Ramp Taper Rate | 20:1 | 40 | n/a | 40 | n/a |  |
| Minimum On-Ramp Taper Rate | 50:1 | n/a | 61 | n/a | 61 |  |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | 206 | 382 | 332 | 90 |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | n/a | n/a | n/a | n/a |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 645 | 954 | 967 | 442 |  |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  | 32 |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ |  | 12 |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $425 / 200$ feet |  | 00 |  |  |  |
| Ramp Intersection Sight Distance (ISD) ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok | n/a | ok | n/a |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | 4\% |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | 0\% |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | 35' |  |  | Supports Impr. |

** Loop ramp design speed $=30 \mathrm{mph}$
${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k -value or Stopping Sight Distance along the crossroad approaching the intersection
Comments
On cross road, guard rail ends are buried in ground. This is probably a substandard design for end treatment.


## MITCHELL REGION

Interstate 90, MRM 251.00 to MRM 412.52
Interstate 29, MRM 0.00 to MRM 124.00
Interstate 229, MRM 0.00 to MRM 10.83
Total Interchanges: 74
Studied Interchanges: 58

| Deficient Interchanges (20): |  |  |  |
| :--- | :---: | :--- | :---: |
| Interchange | Page | Interchange | Page |
| I-29 Exit 1 | A-117 | I-229 Exit 3 | A-201 |
| I-29 Exit 2 | A-125 | I-229 Exit 4 | A-207 |
| I-29 Exit 26 | A-135 | I-229 Exit 5 | A-215 |
| I-29 Exit 47 | A-143 | I-229 Exit 7 | A-223 |
| I-29 Exit 62 | A-153 | I-229 Exit 9 | A-233 |
| I-29 Exit 71 | A-159 | I-90 Exit 330 | A-245 |
| I-29 Exit 77 | A-165 | I-90 Exit 332 | A-253 |
| I-29 Exit 86 | A-179 | I-90 Exit 387 | A-259 |
| I-29 Exit 98 | A-185 | I-90 Exit 390 | A-265 |
| I-229 Exit 2 | A-191 | I-90 Exit 406 | A-267 |

## Summary of Mainline Segment Geometric Performance Mitchell Region

|  |  |  | 듳彥悉 |  |  | $\begin{aligned} & 0 \\ & \grave{\delta} \\ & \text { N } \\ & \text { む̀ } \\ & \text { む̀ } \\ & \text { O M } \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1－90 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 251－263 | 12 | 10 | 4 | 70 | $1^{\circ} 30^{\prime}$ | ＞ 30 | 6：1 | 5．00\％ | 38 | 38 | n／a | 3．95\％ |
| MP 263－265 | 12 | 10 | 4 | 75 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．70\％ | 38 | 26 | 15＇11＂ | 5．50\％ |
| MP 265－272 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | 2．80\％ | 38 | － | 16＇${ }^{\prime \prime}$ | 1．98\％ |
| MP 272－284 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 5：1 | 2．80\％ | 38 | 30 | 16＇10＂ | 2．80\％ |
| MP 284－292 | 12 | 10 | 4 | 70 | $0^{\circ} 14^{\prime}$ | ＜ 30 | 3：1 | － | 38 | 38 | 15＇11＂ | 1．59\％ |
| MP 292－297 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | 2．80\％ | 38 | 38 | 15＇11＂ | 1．59\％ |
| MP 297－306 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 306－316 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 316－325 | 12 | 10 | 4 | 70 | $0^{\circ} 10^{\prime}$ | ＜ 30 | ＜6：1 | － | 38 | － | 16＇0＂ | 1．20\％ |
| MP 325－334 | 12 | 10 | 4 | 70 | $0^{\circ} 30^{\prime}$ | ＜ 30 | 3：1 | － | 38 | 30 | 16＇10＂ | 2．54\％ |
| MP 334－344 | 12 | 10 | 4 | 70 | $0^{\circ} 45^{\prime}$ | ＞ 30 | 4：1 | － | 38 | 38 | 16＇9＇ | 2．15\％ |
| MP 344－352 | 12 | 10 | 4 | 70 | $<2^{\circ} 15^{\prime}$ | ＞ 30 | 4：1 | － | 38 | 38 | 16＇4＂ | 2．10\％ |
| MP 352－362 | 12 | 10 | 4 | 70 | $<2^{\circ} 15^{\prime}$ | ＜ 30 | 3：1 | － | 38 | － | 17＇1＇ | ＜3\％ |
| MP 362－369 | 12 | 10 | 4 | 70 | $<2^{\circ} 15^{\prime}$ | ＜ 30 | 3：1 | 4．00\％ | 38 | 30 | 16＇0＂ | 1．68\％ |
| MP 369－377 | 12 | 10 | 4 | 70 | $0^{\circ} 06^{\prime}$ | ＜ 30 | 3：1 | － | 38 | 30 | 15＇9＂ | 3．00\％ |
| MP 377－389 | 12 | 10 | 4 | 70 | $1^{\circ} 30^{\prime}$ | ＜ 30 | 3：1 | － | 38 | 30 | 15＇11＂ | 2．98\％ |
| MP 389－395 | 12 | 10 | 4 | 70 | $0^{\circ} 30^{\prime}$ | ＜30 | 3：1 | － | 38 | 30 | 16＇3＂ | 3．00\％ |
| MP 395－399 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 399－407 | 12 | 10 | 6 | 70 | $1^{\circ} 00^{\prime}$ | $>30$ | 4：1 | 2．40\％ | 40 | 30 | 15＇2＂ | 2．36\％ |
| MP 407－MIN | 12 | 10 | 6 | 70 | $0^{\circ} 28^{\prime}$ | ＞ 30 | 4：1 | 1．04\％ | 40 | 30 | 16＇8＂ | 3．00\％ |
| 1－29 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 0－2 | 12 | 10 | 6 | 70 | $3^{\circ} 00^{\prime}$ | $>30$ | 4：1 | n／a | 40 | 30 | 16＇2＂ | 1．40\％ |
| MP 2－4 | 12 | 10 | 6 | 70 | $1^{\circ} 00^{\prime}$ | $>30$ | 4：1 | n／a | 41 | 41 | n／a | 2．00\％ |
| MP 4－9 | 12 | 8 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | n／a | 16＇2＂ | 0．25\％ |
| MP 9－15 | 12 | 8 | 4 | 70 | $1^{\circ} 30^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | n／a | n／a | 0．80\％ |
| MP 15－18 | 12 | 10 | 4 | 65 | $1^{\circ} 30^{\prime}$ | $>30$ | 4：1 | n／a | 38 | n／a | 16＇${ }^{\prime}$ | 0．67\％ |
| MP 18－26 | 12 | 10 | 6 | 70 | $1^{\circ} 30^{\prime}$ | ＞ 30 | 4：1 | n／a | 40＇ | 40 | n／a | 3．00\％ |
| MP 26－31 | 13 | 10 | 6 | 70 | $1^{\circ} 30^{\prime}$ | $>30$ | 4：1 | n／a | 42 | 42 | 16＇0＂ | 1．38\％ |
| MP 31－38 | 12 | 10 | 6 | 70 | $0^{\circ} 03^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | n／a | n／a | 3．00\％ |
| MP 38－42 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 42－47 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 47－50 | 12 | 10 | 6 | 70 | $1^{\circ} 43^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | n／a | 17＇ 0 ＂ | 2．68\％ |
| MP 50－53 | 12 | 10 | 6 | 70 | $0^{\circ} 15^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | n／a | n／a | 0．81\％ |
| MP 53－56 | 12 | 10 | 6 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | n／a | 18＇1＂ | 0．52\％ |
| MP 56－59 | 12 | 10 | 6 | 70 | $0^{\circ} 01^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | 40 | n／a | 0．52\％ |
| MP 59－62 | 12 | 10 | 6 | 70 | $0^{\circ} 00^{\prime}$ | $>30$ | 4：1 | n／a | 40 | 40 | 15＇8＂ | 0．60\％ |
| MP 62－64 | 12 | 10 | 6 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | n／a | n／a | 0．59\％ |

## Summary of Mainline Segment Geometric Performance Mitchell Region

|  |  |  |  |  |  | $\begin{aligned} & 0 \\ & \underset{\sim}{\circ} \\ & \text { N } \\ & \text { む } \\ & \text { む̀ } \\ & \text { O} \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MP 64－68 | 12 | 10 | 6 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | 30 | 16＇4＂ | 3．00\％ |
| MP 68－71 | 12 | 10 | 6 | 70 | $0^{\circ} 30^{\prime}$ | ＞ 30 | 4：1 | 2．00\％ | 40 | n／a | n／a | 1．14\％ |
| MP 71－73 | 12 | 10 | 6 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | 2．80\％ | 40 | n／a | 16＇5＂ | 1．79\％ |
| MP 73－75 | 12 | 10 | 6 | 70 | $0^{\circ} 30^{\prime}$ | ＞ 30 | 4：1 | 2．08\％ | 40 | n／a | n／a | 1．12\％ |
| MP 75－77 | 12 | 10 | 6 | 70 | $1^{\circ} 30^{\prime}$ | ＞ 30 | 4：1 | 4．20\％ | 40 | 30 | 16＇3＂ | 3．00\％ |
| MP 77－78 | 12 | 10 | 6 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 40 | n／a | n／a | ＜3．00\％ |
| MP 78－79 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 79－80 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 80－81 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 81－82 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 82－83 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 83－84 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 84－86 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 86－94 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | 2．80\％ | 38 | 38 | n／a | 2．83\％ |
| MP 94－98 | 12 | 10 | 4 | 70 | $0^{\circ} 10^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | 38 | 15＇ 9 ＂ | 2．96\％ |
| MP 98－104 | 12 | 10 | 4 | 70 | $1^{\circ} 00^{\prime}$ | $>30$ | 4：1 | n／a | 38 | 38 | n／a | 2．60\％ |
| MP 104－109 | 12 | 10 | 4 | 70 | $0^{\circ} 12^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | 30 | 16＇3＂ | 2．99\％ |
| MP 109－114 | 12 | 10 | 4 | 70 | $0^{\circ} 00^{\prime}$ | $>30$ | 4：1 | n／a | 38 | n／a | n／a | 0．42\％ |
| MP 114－121 | 12 | 10 | 4 | 70 | $0^{\circ} 06^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | 38 | 16＇11＂ | 1．54\％ |
| I－229 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 1－2 | 12 | 10 | 6 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | － | 40 | 30＇ | 16＇5＂ | 2．77\％ |
| MP 2－3 | 12 | 10 | 6 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 6：0 | － | 40 | － | 16＇3＂ | 0．18\％ |
| MP 3－4 | 12 | 10 | 6 | 70 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．30\％ | 40 | － | 17＇ 2 ＂ | 2．73\％ |
| MP 4－5 | 12 | 10 | 6 | 70 | $3^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 6．00\％ | 52 | － | 17＇4＂ | 2．80\％ |
| MP 5－6 | 12 | 10 | 6 | 70 | $4^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 6．00\％ | 40 | － | 16＇1＂ | 2．68\％ |
| MP 6－7 | 12 | 10 | 4 | 70 | $0^{\circ} 30^{\prime}$ | ＞ 30 | 6：1 | － | 50 | － | 16＇3＂ | 3．00\％ |
| MP 7－9 | 12 | 10 | 4 | 70 | $0^{\circ} 30^{\prime}$ | ＞30 | 6：1 | 1．04\％ | 50 | － | 17＇6＂ | 3．00\％ |
| MP 9－10 |  |  |  |  |  |  |  |  |  |  |  |  |

LEGEND：

| Existing Value does not meet standard criteria |
| :--- |
| Mainline section recently reconstructed |

Summary of Mainline Segments, Traffic Volumes and Levels of Service
Mitchell Region

| I-29 Exits: | Current Lanes | Existing |  | 2020 |  | 2030 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AADT | LOS | AADT | LOS | AADT | LOS |
| 0 to 1 | 4 | 28,820 | B | 33733 | C | 38462 | C |
| 1 to 2 | 6 | 19,930 | A | 23328 | B | 26598 | B |
| 2 to 4 | 4 | 14,550 | A | 17031 | A | 19418 | B |
| 4 to 9 | 4 | 12,280 | A | 14374 | A | 16388 | A |
| 9 to 15 | 4 | 10,290 | A | 12044 | A | 13733 | A |
| 15 to 18 | 4 | 10,600 | A | 12407 | A | 14146 | A |
| 18 to 26 | 4 | 10,200 | A | 11939 | A | 13612 | A |
| 26 to 31 | 4 | 11,370 | A | 13308 | A | 15174 | A |
| 31 to 38 | 4 | 11,970 | A | 14011 | A | 15975 | A |
| 38 to 42 | 4 | 11,730 | A | 13730 | A | 15654 | A |
| 42 to 47 | 4 | 11,650 | A | 13636 | A | 15548 | A |
| 47 to 50 | 4 | 14,790 | A | 16524 | A | 18124 | A |
| 50 to 53 | 4 | 14,960 | A | 16714 | A | 18333 | A |
| 53 to 56 | 4 | 15,520 | A | 17340 | A | 19019 | A |
| 56 to 59 | 4 | 17,060 | A | 19061 | A | 20906 | B |
| 59 to 62 | 4 | 17,890 | A | 19988 | A | 21923 | B |
| 62 to 64 | 4 | 18,150 | A | 20279 | A | 22242 | B |
| 64 to 68 | 4 | 18,230 | A | 20368 | B | 22340 | B |
| 68 to 71 | 4 | 22,410 | B | 27960 | B | 33622 | B |
| 71 to 73 | 4 | 31,670 | B | 39514 | C | 47515 | D |
| 73 to 75 | 4 | 31,560 | B | 39377 | C | 47350 | D |
| 75 to 77 | 4 | 32,180 | B | 43648 | C | 56270 | D |
| 77 to 78 | 6 | 39,640 | B | 53767 | C | 69315 | D |
| 78 to 79 | 8 | 47,480 | B | 64401 | C | 83024 | C |
| 79 to 80 | 8 | 40,400 | B | 54797 | B | 70644 | C |
| 80 to 81 | 8 | 36,990 | B | 50172 | B | 64681 | B |
| 81 to 82 | 8 | 34,360 | B | 46605 | B | 60082 | B |
| 82 to 83 | 8 | 31,980 | B | 43377 | B | 55921 | B |
| 83 to 84 | 8 | 27,560 | A | 37382 | A | 48192 | B |
| 84 to 86 | 4 | 18,340 | A | 23429 | B | 28732 | B |
| 86 to 94 | 4 | 16,690 | A | 21321 | A | 26147 | B |
| 94 to 98 | 4 | 16,500 | A | 21078 | A | 25850 | B |
| 98 to 104 | 4 | 13,750 | A | 15720 | A | 17575 | A |
| 104 to 109 | 4 | 13,080 | A | 14954 | A | 16719 | A |
| 109 to 114 | 4 | 12,550 | A | 14348 | A | 16041 | A |
| 114 to 121 | 4 | 12,660 | A | 14474 | A | 16182 | A |
| 121 to 127 | 4 | 12,240 | A | 13463 | A | 14575 | A |

Summary of Mainline Segments, Traffic Volumes and Levels of Service
Mitchell Region

| I-90 Exits: | Current Lanes | Existing |  | 2020 |  | 2030 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AADT | LOS | AADT | LOS | AADT | LOS |
| 251 to 260 | 4 | 7,230 | A | 7,377 | A | 7,501 | A |
| 260 to 263 | 4 | 7,630 | A | 8,017 | A | 8,355 | A |
| 263 to 265 | 4 | 7,640 | A | 8,028 | A | 8,366 | A |
| 265 to 272 | 4 | 7,650 | A | 8,038 | A | 8,377 | A |
| 272 to 284 | 4 | 7,270 | A | 7,639 | A | 7,961 | A |
| 284 to 289 | 4 | 7,480 | A | 7,860 | A | 8,191 | A |
| 289 to 296 | 4 | 6,810 | A | 6,992 | A | 7,148 | A |
| 296 to 308 | 4 | 7,530 | A | 7,732 | A | 7,904 | A |
| 308 to 310 | 4 | 8,180 | A | 8,399 | A | 8,586 | A |
| 310 to 319 | 4 | 8,630 | A | 8,922 | A | 9,173 | A |
| 319 to 325 | 4 | 8,850 | A | 9,149 | A | 9,406 | A |
| 325 to 330 | 4 | 9,090 | A | 9,247 | A | 9,380 | A |
| 330 to 332 | 4 | 9,090 | A | 9,247 | A | 9,380 | A |
| 332 to 335 | 4 | 9,090 | A | 9,101 | A | 9,110 | A |
| 335 to 344 | 4 | 9,120 | A | 9,131 | A | 9,140 | A |
| 344 to 350 | 4 | 9,300 | A | 9,311 | A | 9,320 | A |
| 350 to 353 | 4 | 9,310 | A | 9,954 | A | 10,525 | A |
| 353 to 357 | 4 | 9,130 | A | 9,762 | A | 10,322 | A |
| 357 to 364 | 4 | 9,680 | A | 10,350 | A | 10,944 | A |
| 364 to 368 | 4 | 9,630 | A | 10,297 | A | 10,887 | A |
| 368 to 374 | 4 | 9,840 | A | 10,521 | A | 11,125 | A |
| 374 to 379 | 4 | 10,480 | A | 13,388 | A | 16,419 | A |
| 379 to 387 | 4 | 11,180 | A | 15,164 | A | 19,550 | A |
| 387 to 390 | 4 | 12,070 | A | 16,371 | A | 21,106 | B |
| 390 to 396 | 4 | 13,480 | A | 18,284 | A | 23,571 | B |
| 396 to 399 | 4 | 18,270 | A | 24,781 | B | 31,947 | C |
| 399 to 400 | 4 | 20,710 | A | 28,090 | B | 36,214 | C |
| 400 to 402 | 4 | 21,080 | B | 28,592 | B | 36,861 | C |
| 402 to 406 | 4 | 18,260 | A | 23,326 | B | 28,607 | B |
| 406 to 410 | 4 | 14,020 | A | 17,910 | A | 21,964 | B |
| I-229 Exits: |  |  |  |  |  |  |  |
| 0 to 1 | 4 | 24,100 | A | 30,069 | B | 36,158 | C |
| 1 to 2 | 6 | 35,190 | B | 47,731 | C | 61,534 | D |
| 2 to 3 | 6 | 41,840 | C | 56,751 | D | 73,162 | F |
| 3 to 4 | 6 | 44,030 | C | 59,721 | D | 76,992 | F |
| 4 to 5 | 6 | 40,400 | B | 54,797 | D | 70,644 | E |
| 5 to 6 | 4 | 34,330 | C | 46,564 | E | 60,030 | F |
| 6 to 7 | 6 | 32,040 | B | 43,458 | C | 56,026 | D |
| 7 to 9 | 6 | 30,160 | B | 40,908 | C | 52,738 | D |

Structurally Deficient and Functionally Obsolete Mainline Structure Summary- Mitchell Region

Mitchell Region (continued)

| I-29 MRM 0 to 124 | Number of Bridges | Length | Existing Deck Out-to-Out Width | Existing Area | Unit Price | Removal Cost | Proposed Deck Clear Roadway Width | $\begin{gathered} \text { Proposed } \\ \text { Area } \\ \hline \end{gathered}$ | Unit Price | Bridge Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| River Drive at MRM 2.48 (Functionally Obsolete) | 2 | 126 | 43 | 10,760 | \$9 | \$96,844 | 40 | 10,080 | \$100 | \$1,008,000 |
| Westshore Dr over I-29 at MRM 4.35 (Functionally Obsolete-NARROW) | 1 | 293 | 34 | 10,060 | \$9 | \$90,542 | 40 | 11,732 | \$100 | \$1,173,200 |
| 484th Ave over I-29 at MRM 5.88 (Functionally Obsolete-NARROW) | 1 | 365 | 34 | 12,530 | \$9 | \$112,768 | 32 | 11,690 | \$100 | \$1,168,960 |
| I-29 over SD owned RR at MRM 18.49 (Functionally Obsolete) | 2 | 185 | 46 | 17,112 | \$9 | \$154,012 | 52 | 19,219 | \$100 | \$1,921,920 |
| WB US 18 over I-29 (Exit 62) at MRM 62.37 (Functionally Obsolete) | 1 | 293 | 34 | 10,060 | \$9 | \$90,542 | 36 | 10,559 | \$100 | \$1,055,880 |
| 281st St over I-29 at MRM 63.34 (Structurally Deficient) | 1 | 254 | 28 | 7,112 | \$9 | \$64,008 | 32 | 8,128 | \$100 | \$812,800 |
| Twin Structures over Creek at MRM 67.13 (Functionally Obsolete-NARROW) | 2 | 192 | 34 | 13,171 | \$9 | \$118,541 | 40 | 15,360 | \$100 | \$1,536,000 |
| 248th St over I-29 at MRM 96.48 (Structurally Deficient) | 1 | 254 | 32 | 8,204 | \$9 | \$73,838 | 32 | 8,128 | \$100 | \$812,800 |
| SD 115 over I-29 (Exit 98) at MRM 98.48 (Functionally Obsolete) | 1 | 254 | 32 | 8,204 | \$9 | \$73,838 | 40 | 10,160 | \$100 | \$1,016,000 |
| I-29 over Bachelor Creek at MRM 106.02 <br> (Functionally Obsolete-NARROW) | 2 | 152 | 34 | 10,413 | \$9 | \$93,721 | 40 | 12,144 | \$100 | \$1,214,400 |
| I-29 over 233rd St at MRM 111.84 (Functionally Obsolete-LOW CLEARANCE) | 2 | 80 | 41 | 6,512 | \$9 | \$58,608 | 40 | 6,400 | \$100 | \$640,000 |
| I-29 over 232nd St at MRM 112.83 (Functionally Obsolete-LOW CLEARANCE) | 2 | 80 | 41 | 6,512 | \$9 | \$58,608 | 40 | 6,400 | \$100 | \$640,000 |
| I-229 MRM 0 to 10.83 |  |  |  |  |  |  |  |  |  |  |
| Cliff Avenue at MRM 4.16 (Functionally Obsolete-LOW CLEARANCE) | 2 | 183 | 35 | 12,714 | \$9 | \$114,427 | 40 | 14,656 | \$100 | \$1,465,600 |
| I-229 over 57th Street at MRM 1.66 <br> TUNNEL - (Functionally Obsolete-NARROW) | 1 | 415 | 85 | 35,068 | \$15 | \$526,013 | 85 | 35,068 | \$100 | \$3,506,750 |
| 60th St over I-229 at MRM 10.47 (Structurally Deficient) | 1 | 238 | 34 | 8,167 | \$9 | \$73,501 | 52 | 12,381 | \$100 | \$1,238,120 |


|  |  | Geometric Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Crashes, 2006-2009 |  |  |  |  |  |  | 2009/2020/2030 Level of Service |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Location |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\mid \underset{\mid}{\underset{\underline{E}}{\underline{E}}}$ | 음 | $\begin{aligned} & \stackrel{\text { ¢ }}{\stackrel{1}{\circ}} \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & \stackrel{0}{0} \\ & \sum_{\infty}^{2} \\ & \infty \\ & \stackrel{\infty}{\infty} \\ & \frac{\infty}{3} \end{aligned}$ |  |  |
| 1-29 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Exit 1 | Dakota Dunes | 4.0\% | 330' | $6^{\circ} 21^{\prime}$ | > $30^{\prime}$ | 4.00\% | $20.5{ }^{\prime}$ | $2.5{ }^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 25 | 50 | 110 | 493' | >425 | 217 | 964' | 3.0\% | 489' | 0 | 5 | 23 | 28 | 38 | 0.92 | 50 | B/F/F | A/B/B | B/B/B | A/A/A | C/C/F | c/fff |
|  | Loop Ramps |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | N/A | A/A/B | N/A | B/B/B |  | /A |
| Exit 2 | North Sioux City | - | 1432' | 00' | <30' | 2.70\% | 18.5' | 1.5' | $1.5{ }^{\prime}$ | 3:1 | 35 | 62 | 74 | 446' | $>425$ | 73 | 649' | 0.9\% | $70^{\prime}$ | 0 | 5 | 12 | 17 | 27 | 0.78 | 58 | A/A/A | B/B/B | A/B/B | A/AB | B/B/B | c/d/f |
| Exit 4 | McCook Lake | - | 955' | $6^{\circ} 00^{\prime}$ | <30' | 3.17\% | $18.5{ }^{\text {' }}$ | $1.5{ }^{\prime}$ | $2.0{ }^{\prime}$ | 3:1 | 41 | 62 | 105 | 488' | $265^{\prime}$ | 45 | 356' | 4.0\% | 300' | 0 | 2 | 10 | 12 | 16 | 0.78 | 59 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 9 | Jefferson | - | 955' | $6^{\circ} 00^{\prime}$ | <30' | 3.51\% | 19.5' | 1.0 | $1.0{ }^{\prime}$ | 3:1 | 41 | 62 | 74 | 350' | sub | 75 | 356' | 4.0\% | 530' | 0 | 1 | 3 | 4 | 6 | 0.41 | 95 |  |  |  |  |  |  |
| Exit 15 | Elk Point | - | 1432' | $4^{\circ} 00^{\prime}$ | <30' | 2.99\% | $18.5{ }^{\prime}$ | $2.0{ }^{\circ}$ | $1.5{ }^{\prime}$ | 3:1 | 27 | 29 | 72 | 349' | sub | 74 | $348^{\prime}$ | 4.1\% | 300 | 0 | 0 | 0 | 0 | 0 | 0.00 | 126 |  |  |  |  |  |  |
| Exit 26 | Vermillion/Yankton | - | 955' | $6^{\circ} 00^{\prime}$ | <30' | 3.77\% | $19.0{ }^{\prime}$ | $2.0{ }^{\circ}$ | $2.5{ }^{\prime}$ | 3:1 | 28 | 29 | 59 | 299' | sub | 67 | 400' | 4.0\% | 570' | 0 | 2 | 12 | 14 | 18 | 0.69 | 66 | A/A/A | A/A/A | A/A/A | A/A/A | c/d | b/b/c |
| Exit 31 | Spink/Akron | 6.0\% | 1910' | $3^{\circ} 00^{\prime}$ | <30' | 1.54\% | 17.5' | $2.5{ }^{\prime}$ | 3.0 | 3:1 | 42 | 63 | 124 | 1345' | $>425$ | 115 | 521' | 3.2\% | $>660^{\prime}$ | 0 | 0 | 10 | 10 | 10 | 0.72 | 63 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 38 | Volin | 6.0\% | 1910' | $3^{\circ} 00^{\prime}$ | <30' | 1.75\% | $18.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 3.0 | 3:1 | 42 | 63 | 122 | $758^{\prime}$ | sub | 82 | 421' | 4.0\% | $>660^{\prime}$ | 0 | 0 | 8 | 8 | 8 | 0.59 | 75 |  |  |  |  |  |  |
| Exit 42 | Alcester/Wakonda | 6.0\% | 1910' | $3^{\circ} 00^{\prime}$ | <30' | 2.67\% | $18.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 3.0 | 3:1 | 42 | 63 | 54 | 290' | >425 | 99 | $500 \cdot$ | 3.2\% | > 660' | 0 | 1 | 4 | 5 | 7 | 0.51 | 80 |  |  |  |  |  |  |
| Exit 47 | Beresford/rene | 6.2\% | 1432' | $4^{\circ} 00^{\prime}$ | <30' | 3.77\% | $15.0{ }^{\prime}$ | 6.5' | 1.0 | 3:1 | 42 | 63 | 90 | 439' | sub | 81 | 386' | 3.1\% | 410' | 0 | 0 | 3 | 3 | 3 | 0.12 | 120 | A/A/B | A/A/A | A/B/B | A/A/A | b/ef | c/ff |
| Exit 50 | Centerville/Hudson | 6.2\% | 1432' | $4^{\circ} 00^{\prime}$ | <30' | 3.77\% | 15.5' | 3.5 | $2.5{ }^{\prime}$ | 3:1 | 42 | 63 | 50 | 368' | sub | 72 | 337 | 4.3\% | 330' | 0 | 0 | 1 | 1 | 1 | 0.06 | 123 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 53 | Viborg | 6.2\% | 1432' | $4^{\circ} 00^{\prime}$ | <30' | 2.72\% | $14.0{ }^{\prime}$ | 4.5' | 4.0 | 3:1 | 42 | 63 | 64 | 333' | sub | 73 | $347^{\prime}$ | 5.0\% | $380^{\prime}$ | 0 | 2 | 2 | 4 | 8 | 0.46 | 87 |  |  |  |  |  |  |
| Exit 56 | Fairview | 6.2\% | 1432' | $4^{\circ} 00^{\prime}$ | < $30^{\circ}$ | 1.11\% | $13.0{ }^{\circ}$ | $3.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | 3:1 | 29 | 42 | 182 | 1699' | sub | 63 | 305' | 4.0\% | 350' | 0 | 3 | 2 | 5 | 11 | 0.60 | 73 |  |  |  |  |  |  |
| Exit 59 | Davis | 6.2\% | 1432' | $4^{\circ} 00^{\prime}$ | <30' | 3.42\% | 14.0' | 3.5' | $2.0{ }^{\prime}$ | 3:1 | 29 | 42 | 106 | 577' | sub | 84 | 406' | 1.0\% | 406' | 1 | 1 | 4 | 6 | 19 | 0.91 | 51 |  |  |  |  |  |  |
| Exit 62 | Canton | 8.0\% | 955' | $6^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.60\% | $16.5{ }^{\text {' }}$ | 3.5' | $2.5{ }^{\prime}$ | 4:1 | 28 | 29 | 77 | 375' | $>425$ | 100 | $561{ }^{\prime}$ | 3.0\% | 550' | 0 | 2 | 10 | 12 | 16 | 0.64 | 69 | B/B/B | B/B/B | B/B/B | B/B/B | b/b/b | b/b/c |
| Exit 64 | Worthing/ Lennox | - | 1432' | $4^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.97\% | $18.0{ }^{\prime}$ | $1.5{ }^{\prime}$ | 3.0 | 4:1 | 29 | 29 | 59 | $330^{\prime}$ | >425 | 98 | 434' | 3.0\% | 420' | 0 | 4 | 10 | 14 | 22 | 0.96 | 48 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 68 | Lennox/Parker | - | 1432' | $4^{\circ} 00^{\prime}$ | > $0^{\prime}$ | 4.08\% | $15.5{ }^{\prime}$ | 3.5' | $2.5{ }^{\prime}$ | 4:1 | 29 | 29 | 71 | 336' | sub | 75 | 356' | 4.0\% | 330' | 0 | 4 | 10 | 14 | 22 | 0.83 | 56 |  |  |  |  |  |  |
| Exit 71 | Harrisburg/Tea | - | 955' | $6^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.24\% | 15.5' | 3.0 | $2.0{ }^{\prime}$ | 4:1 | 29 | 29 | 79 | 538' | sub | 76 | 414' | 4.0\% | 150' | 0 | 1 | 7 | 8 | 10 | 0.29 | 104 | B/B/C | B/B/C | C/D/D | C/C/D | b/b/b | b/b/c |
| Exit 77 | 41st Street | - | 955' | $6^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.00\% | 16.5' | 4.5 | 2.0 | 4:1 | 23 | 29 | 80 | $367^{\prime}$ | $>425$ | 100 | 444' | 4.0\% | 200' | 0 | 71 | 103 | 174 | 316 | 3.72 | 2 | C/E/F | C/D/F | C/E/F | D/F/F | F/F/F | F/F/F |
| Exit 86 | Renner/Crooks | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | <30' | 4.61\% | $15.0^{\prime}$ | 4.0' | $1.0^{\prime}$ | 4:1 | 41 | 62 | 117 | $547^{\prime}$ | $>425$ | 141 | 551' | 4.2\% | 250' | 1 | 2 | 11 | 14 | 29 | 1.14 | 40 | B/B/B | A/B/B | B/B/B | B/B/B | b/b/c | b/b/c |
| Exit 94 | Baltic | 4.2\% | 1910 | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.46\% | 15.0' | 3.5 | 2.5 | 4:1 | 40 | 61 | 53 | $337^{\prime}$ | $>425$ | 173 | 611' | 5.1\% | 380' | 0 | 3 | 9 | 12 | 18 | 0.89 | 53 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 98 | Dell Rapids | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.10\% | 15.5' | 3.0 | 3.0 | 4:1 | 40 | 61 | 90 | 537' | $>425$ | 220 | 689' | 3.7\% | 250' | 0 | 4 | 8 | 12 | 20 | 0.89 | 54 | A/B/B | A/B/B | A/A/B | A/B/B | $\mathrm{b} / \mathrm{h} / \mathrm{c}$ | b/c/c |
| Exit 104 | Trent | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.97\% | 15.0' | 4.5' | $2.0{ }^{\prime}$ | 4:1 | 40 | 61 | 101 | 514' | sub | 170 | 637' | 2.1\% | $>660^{\prime}$ | 0 | 0 | 4 | 4 | 4 | 0.26 | 109 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 109 | Madison/Colman | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.20\% | 18.0' | 3.0 | $2.0{ }^{\prime}$ | 4:1 | 40 | 61 | 118 | 534' | >425 | 180 | 725' | 2.7\% | 660' | 0 | 4 | 7 | 11 | 19 | 0.91 | 52 |  |  |  |  |  |  |
| Exit 114 | Flandreau | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.00\% | $18.0{ }^{\prime}$ | 3.0 | 3.0 | 4:1 | 40 | 61 | 89 | 470' | $>425$ | 143 | 596' | 3.0\% | 610' | 0 | 1 | 6 | 7 | 9 | 0.54 | 78 |  |  |  |  |  |  |
| Exit 121 | Nunda/Ward | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.66\% | $18.0{ }^{\prime}$ | 3.0 | 3.0 | 4:1 | 40 | 61 | 139 | $640^{\prime}$ | $>425$ | 167 | 625' | 2.5\% | $330{ }^{\prime}$ | 0 | 1 | 13 | 14 | 16 | 1.05 | 44 |  |  |  |  |  |  |


|  |  | Geometric Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Crashes, 2006-2009 |  |  |  |  |  |  | 2009/2020/2030 Level of Service |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Location |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \underline{\rightharpoonup} \\ \underline{\underline{E}} \end{gathered}$ | 음 | $\stackrel{\text { 厄̈ }}{\stackrel{\text { ® }}{\circ}}$ |  |  |  |  |  | $\begin{aligned} & \stackrel{\otimes}{0} \\ & \stackrel{y}{0} \\ & \stackrel{y}{0} \\ & \stackrel{\infty}{\infty} \\ & \frac{\infty}{3} \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \sum_{\infty}^{\infty} \\ & \infty \\ & \frac{\infty}{\infty} \\ & \frac{\infty}{3} \end{aligned}$ |  |  |
| 1-90 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Exit 260 | Oacoma/Chamberlain | - | 1910' | $3^{\circ} 00^{\prime}$ | >30" | 4.4\% | 16.5' | 3.0 | 4.0 | 6:1 | 42 | 63 | 118 | 505' | sub | 28 | 349' | 4.8\% | 220' | 0 | 0 | 1 | 1 | 1 | 0.07 | 0.7122 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 263 | Chamberlain | 6.0\% | 236' | $24^{\circ} 17^{\prime}$ | > 301 | 4.0\% | 16.5' | $1.5{ }^{\prime}$ | 0.0 | 6:1 | 39 | $>50$ | 42 | 303' | $>425$ | 1721 | >425' | 0.7\% | 0 | 0 | 2 | 2 | 4 | 8 | 0.74 | 461 |  |  |  |  |  |  |
| Exit 265 | Chamberlain | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 2.4\% | 15.0' | 4.5' | $3.5{ }^{\prime}$ | 4:1 | 40 | 61 | 91 | $588{ }^{\prime}$ | $>425$ | 138 | 600' | 3.0\% | 150' | 0 | 0 | 6 | 6 | 6 | 0.46 | 690 |  |  |  |  |  |  |
| Exit 272 | Pukwana |  | 1910' | $3^{\circ} 00^{\prime}$ | > 30 " | 3.4\% | $15.0{ }^{\prime}$ | 6.5' | $2.0{ }^{\prime}$ | 4:1 | 40 | 61 | 96 | 493' | $>425$ | 258 | 899' | 3.0\% | $>30^{\circ} 0^{\prime}$ | 0 | 0 | 2 | 2 | 2 | 0.22 | 22112 |  |  |  |  |  |  |
| Exit 284 | Kimball | 3.5\% | 2865' | $2^{\circ} 00^{\prime}$ | > 301 | 2.9\% | 13.5' | 5.0' | $2.0{ }^{\prime}$ | 4:1 | 39 | 58 | 115 | 550' | $>425$ | 568 | > 425' | 1.0\% | 200' | 0 | 0 | 5 | 5 | 5 | 0.46 | 689 |  |  |  |  |  |  |
| Exit 289 | Platte | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 301 | 1.7\% | $14.0{ }^{\circ}$ | 5.5' | $3.5{ }^{\prime}$ | 4:1 | 40 | 61 | 131 | 805' | $>425$ | 108 | 471' | 3.0\% | $>30^{\circ} 0^{\prime}$ | 0 | 1 | 4 | 5 | 7 | 0.81 | 1 57 |  |  |  |  |  |  |
| Exit 296 | White Lake | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30 " | 1.7\% | $13.0{ }^{\prime}$ | $7.0^{\prime}$ | 4.5' | 4:1 | 40 | 61 | 196 | 856' | $>425$ | 167 | 600' | 3.0\% | 120' | 0 | 1 | 2 | 3 | 5 | 0.54 | 477 |  |  |  |  |  |  |
| Exit 308 | Plankinton | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | <30" | 1.3\% | 18.0' | 3.0 | 3.0 | 3:1 | 40 | 61 | 144 | 1483' | sub | 74 | $345^{\prime}$ | 4.0\% | 400' | 0 | 0 | 1 | 1 | 1 | 0.09 | 9 121 |  |  |  |  |  |  |
| Exit 310 | Stickney/Aberdeen | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | <30" | 1.6\% | 14.0' | 6.5' | 4.0 | 3:1 | 40 | 61 | 139 | 1092' | $>425$ | 175 | $747^{\prime}$ | 3.0\% | 400' | 0 | 0 | 2 | 2 | 2 | 0.15 | 5117 |  |  |  |  |  |  |
| Exit 319 | Mount Vernon | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | <30" | 1.7\% | 14.0' | 7.5' | 3.0 | 3:1 | 40 | 61 | 213 | 819' | $>425$ | 167 | 600' | 3.0\% | 250' | 0 | 0 | 3 | 3 | 3 | 0.25 | 25110 |  |  |  |  |  |  |
| Exit 325 | Betts Road | 4.0\% | 1910' | $3^{\circ} 00^{\prime}$ | <30" | 2.9\% | 14.5' | 6.5' | 3.0 | 3:1 | 40 | 61 | 104 | 560' | $>425$ | 115 | 495' | 3.8\% | > 30 ${ }^{\prime}{ }^{\prime}$ | 0 | 1 | 2 | 3 | 5 | 0.46 | 688 |  |  |  |  |  |  |
| Exit 330 | Mitchell/Huron | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 2.3\% | $18.0{ }^{\prime}$ | $4.0{ }^{\circ}$ | 4.0 | 4:1 | 40 | 61 | 176 | 830' | $>425$ | 175 | 754' | 3.0\% | 420' | 0 | 2 | 4 | 6 | 10 | 0.50 | 5082 | A/A/A | A/A/A | A/A/A | A/A/A | c/d/f | c/d/e |
| Exit 332 | Mitchell/Parkston | 6.0\% | 1910' | $5^{\circ} 00^{\prime}$ | > 301 | 4.3\% | $12.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | 4:1 | 40 | 60 | 134 | 539' | $>425$ | 418 | 949' | 2.6\% | 400' | 0 | 11 | 32 | 43 | 65 | 2.15 | 1511 | A/A/A | A/A/A | A/A/A | A/A/A | A/A/A | A/A/A |
| Exit 335 | Riverside Road | 4.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 301 | 2.3\% | $18.0{ }^{\prime}$ | 4.5' | 4.0 | 4:1 | 40 | 55 | 104 | 560' | $>425$ | 225 | 960' | 1.4\% | 350' | 0 | 1 | 3 | 4 | 6 | 0.51 | 5181 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 344 | Alexandria | 4.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 301 | 2.2\% | $14.0{ }^{\prime}$ | 6.5 ${ }^{\prime}$ | $2.5{ }^{\prime}$ | 4:1 | 40 | 53 | 224 | 1118' | $>425$ | 253 | 749' | 2.5\% | 300' | 0 | 0 | 5 | 5 | 5 | 0.40 | 40 96 |  |  |  |  |  |  |
| Exit 350 | Emery/Farmer | 4.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 2.0\% | 14.0' | 7.5' | $2.5{ }^{\prime}$ | 4:1 | 40 | 61 | 212 | 913' | $>425$ | 262 | 754' | 2.0\% | 300' | 0 | 2 | 6 | 8 | 12 | 1.11 | 1.1142 |  |  |  |  |  |  |
| Exit 353 | Spencer/Emery | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 2.2\% | 14.5' | 5.0' | 3.0 | 4:1 | 41 | 61 | 125 | 861' | $>425$ | 115 | 665' | 2.6\% | 300' | 0 | 0 | 2 | 2 | 2 | 0.17 | 17114 |  |  |  |  |  |  |
| Exit 357 | Bridgewater | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 301 | 2.7\% | $14.0{ }^{\prime}$ | 5.0' | $2.5{ }^{\prime}$ | 4:1 | 41 | 61 | 128 | 599' | $>425$ | 120 | 434' | 4.0\% | 400' | 0 | 2 | 5 | 7 | 11 | 1.03 | 103 45 |  |  |  |  |  |  |
| Exit 364 | Salem/Yankton | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 3.8\% | 15.0 | 6.5' | $3.5{ }^{\prime}$ | 4:1 | 40 | 61 | 128 | 600' | $>425$ | 132 | 759' | 3.0\% | 300' | 0 | 1 | 7 | 8 | 10 | 0.71 | 71.64 |  |  |  |  |  |  |
| Exit 368 | Canistota | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > 301 | 3.0\% | 14.5' | 7.5' | $3.5{ }^{\prime}$ | 4:1 | 39 | 61 | 179 | $754{ }^{\prime}$ | $>425$ | 105 | 569' | 3.8\% | $>30^{\prime} 0^{\prime}$ | 0 | 5 | 5 | 10 | 20 | 1.77 | 17717 |  |  |  |  |  |  |
| Exit 374 | Montrose | - | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 2.0\% | 14.5' | 4.5' | 3.5' | 4:1 | 40 | 61 | 169 | 802' | sub | 83 | 376' | 3.7\% | 300' | 0 | 4 | 6 | 10 | 18 | 1.50 | 1.7717 <br> 150 |  |  |  |  |  |  |
| Exit 379 | Humboldt/Madison | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > 30" | 2.2\% | 14.0' | 5.5' | 1.5' | 4:1 | 39 | 61 | 131 | 820' | $>425$ | 202 | 807' | 3.1\% | 200' | 0 | 8 | 9 | 17 | 33 | 2.15 | 1512 |  |  |  |  |  |  |
| Exit 387 | Hartford | 4.2\% | 1910' | $3^{\circ} 00^{\prime}$ | > 301 | 1.5\% | 14.0' | $5.0^{\prime}$ | $1.0^{\prime}$ | 4:1 | 38 | 61 | 191 | 2820' | $>425$ | 150 | 569' | 4.0\% | 300' | 0 | 1 | 3 | 4 | 6 | 0.34 | 34100 | A/A/A | A/A/A | A/A/B | A/A/B | a/b/b | b/b/b |
| Exit 390 | Hartford | 6.0\% | 252' | $22^{\circ} 34^{\prime}$ | > 30" | 3.5\% | 14.5' | 4.5' | 2.0 | 3:1 | 41 | 61 | 77 | 407' | - | - | - | - | 400' | 0 | 7 | 23 | 30 | 44 | 2.36 | 36 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 406 | Brandon/Corson | 6.0\% | 1432 | $4^{\circ} 00^{\prime}$ | <30" | 6.0\% | $15.0{ }^{\prime}$ | 4.5' | $1.5{ }^{\prime}$ | 3:1 | 27 | 29 | 96 | 427' | >425 | 249 | 871' | 1.1\% | 400' | 1 | 3 | 12 | 16 | 33 | 1.02 | 1.247 | A/B/B | A/B/B | A/A/A | A/B/B | cle/f | $\mathrm{c} / \mathrm{d} / \mathrm{f}$ |
| Exit 410 | Valley Springs/Garretson | - | $1432 \cdot$ | $4^{\circ} 00^{\prime}$ | > 30" | 4.6\% | 15.5' | $2.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | 4:1 | 27 | 29 | 67 | $321{ }^{\prime}$ | sub | 100 | 465' | 4.9\% | $>30^{\prime} 0^{\prime}$ | 0 | 0 | 7 | 7 | 7 | 0.44 | 44 92 | Not evaluated due to interchange screening method |  |  |  |  |  |
| 1-229 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Exit 2 | Western Avenue | - | 716' | $8^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.35\% | 25.5' | $1.5{ }^{\prime}$ | 1.5 | 4:1 | 1 | - | 61 | 289' | sub | 74 | 344' | 3.6\% | 350' | 0 | 21 | 42 | 63 | 105 | 195 | 3931 | B/B/C | B/B/C | B/C/C | A $/$ / $/ C$ | F/F/F | F/F/F |
| Exit 3 | Minnesota Avenue | 5.6\% | 1637' | $3^{\circ} 30^{\prime}$ | > $30^{\prime}$ | 2.90\% | 17.5' | $3.0^{\prime}$ | 1.5' | 4:1 | 1 - |  | 76 | 506' | - | . |  |  | 160' | 0 | 25 | 53 | 78 | 128 | 1.54 | 15422 | B/B/C | B/C/C | B/C/C | B/C/C | D/F/F | D/E/F |
| Exit 4 | Cliff Avenue | 6.0\% | 1848' | $3^{\circ} 06^{\prime}$ | > $30^{\prime}$ | 3.29\% | $12.0{ }^{\prime}$ | 3.5' | $1.5{ }^{\prime}$ | 3:1 | 1 - | - | 87 | 508' | - | - | - | - | 150' | 0 | 23 | 49 | 72 | 118 | 1181.97 | 19713 | B/C/C | B/B/C | B/B/C | B/C/C | B/C/C | C/C/E |
| Exit 5 | 26th Street | 5.6\% | 205' | $28^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.57\% | 19.0' | 1.5' | $0.0{ }^{\prime}$ | 6:1 | 1 - | - | 30 | 257' | - | - | - | - | 260' | 0 | 35 | 68 | 103 | 173 | 173.41 | 241 | B/B/C | B/C/C | B/C/C | B/B/C | E/F/F | ffff |
| Exit 7 | Rice Street | 6.0\% | 160' | $35^{\circ} 48^{\prime}$ | > $30^{\prime}$ | 3.57\% | $15.0{ }^{\prime}$ | 3.0 | $2.5{ }^{\prime}$ | 4:1 | 1 - | - | 30 | 257' | - | - | - | - | 350' | 0 | 10 | 36 | 46 | 66 | 1.22 | 12237 | B/B/C | B/B/C | A/B/B | B/B/C | C/E/F | ff/ff |
| Exit 9 | Benson Road | 4.0\% | 2291' | $2^{\circ} 30^{\prime}$ | > $30^{\prime}$ | 3.25\% | 15.0 | 1.0 | 0.0 | 6:1 | 20 | 50 | 101 | 446' | ok | 224 | 859' | 0.8\% | >300' | 0 | 6 | 14 | 20 | 32 | 0.69 | 6967 | B/B/C | A/A/A | B/B/B | A/B/B | B/C/F | f/f/f |

## Legend

## Existing value does not meet standard criteria

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## I-29 EXIT 1 DAKOTA DUNES


Figure 1
I-29 Exit 1 - Dakota Dunes

## Probable Construction Costs

I-29 Exit 1 - Lane Addition and Signalization Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$2,000.00 | \$2,000 |
| Traffic Control | 1 | LUMP SUM | \$3,000.00 | \$3,000 |
| Clearing | 1 | LUMP SUM | \$1,000.00 | \$1,000 |
| Removal of Concrete Pavement | - | SQ. YD. | \$3.88 | \$0 |
| Removal of Asphalt Pavement | - | SQ. YD. | \$7.39 | \$0 |
| Remove Bridge | - | SQ. FT. | \$9.00 | \$0 |
| Borrow, Unclassified Excavation | 1,343 | CU. YD. | \$5.30 | \$7,120 |
| Base Course | 213 | TON | \$10.64 | \$2,267 |
| Asphalt Composite |  | TON | \$80.91 | \$0 |
| PCC Pavement 11" (mainline) | - | SQ. YD. | \$33.12 | \$0 |
| PCC Pavement 8" (ramps) | 467 | SQ. YD. | \$43.40 | \$20,251 |
| Concrete Approach Slab | - | SQ. YD. | \$188.34 | \$0 |
| Bridges | - | SQ. FT. | \$100.00 | \$0 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$0.00 | \$0 |
| Traffic Signal | 2 | EACH | \$125,000.00 | \$250,000 |
| Roadway Lighting | 1 | LUMP SUM | \$0.00 | \$0 |
| Drainage (18" RCP) | 30 | LF | \$24.53 | \$736 |
| Subtotal |  |  |  | \$290,000 |
| Contingencies | 25\% |  |  | \$72,500 |
| Total Probable Construction Costs |  |  |  | \$360,000 |
| Engineering, Administration | 15\% |  |  | \$54,000 |
| Total Project Costs |  |  |  | \$410,000 |

## INTERCHANGE GEOMETRICS CHECKLIST

 SDDOT Interstate Corridor Study| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 1 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Partial Cloverleaf |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 2 | 1 | 2 |  |
| Right Turn Storage Length |  | - | - | - | 300' |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 4.00\% | 4.00\% | 4.00\% | 4.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 330' | 600' | 900' | 600' | Supports Impr. |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $17^{\circ} 21^{\prime}$ | $9^{\circ} 32^{\prime}$ | $6^{\circ} 21^{\prime}$ | $9^{\circ} 32{ }^{\prime}$ | Supports Impr. |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 4.00\% | 0.98\% | 0.16\% | 0.71\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.63\% | - | -1.30\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | 26 |  | 32 | Acceptable |
| As Single Lane | 15 feet (19 for loops) | 22 | - | 24.5 |  | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.5 | 2.5 | 4' | 3 | Supports Impr. |
| Left Shoulder | 2 feet | 3.5 | 7 | $2^{\prime}$ | 2 | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 25:1 | - | 20:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 50:1 | - | 50:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 |  | 307 | 137 | 422 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 110 | 504 | 111 | 563 | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 493' | 1253' | 839' | 1,670' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | East |  | West |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 217 |  | 217 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 246 |  | 246 |  | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 964' |  | 964' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 3.0\% |  | 3.0\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.25\% |  | 0.25\% |  | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 510' |  | 489' |  | Acceptable |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection
Comments

## INTERCHANGE GEOMETRICS CHECKLIST

 SDDOT Interstate Corridor Study| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 1 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | F | H |  | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Partial Cloverleaf |  |  |  | --------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |
| Number of Lanes |  | 1 | 1 |  |  |
| Right Turn Storage Length |  | - | - |  |  |
| Left Turn Storage Length |  | - | - |  |  |
| Superelevation (e max) | 6\% | 4.00\% | 4.00\% |  | Acceptable |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833/231 feet | 330' | 330' |  | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $17^{\circ} 21^{\prime}$ | $17^{\circ} 21^{\prime}$ |  | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' |  | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | - | - |  |  |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.25\% | -3.25\% |  | Acceptable |
| Minimum Lane Width |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - |  |  |
| As Single Lane | 15 feet (19 for loops) | 21.5 | 20.5 |  | Acceptable |
| Shoulder Width |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 5 | 3.5 |  | Acceptable |
| Left Shoulder | 2 feet | 4' | 4' |  | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 |  | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | - |  |  |
| Minimum On-Ramp Taper Rate | 50:1 | Aux. | 50:1 |  | Acceptable |
| Ramp Features |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | - | - |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/137 | 290 | 290 |  | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 2566' | 2566' |  | Acceptable |
| Cross Road Features |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/137 |  |  |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet |  |  |  |  |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )/*** | 425 / 200 feet |  |  |  |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  |  |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  |  |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  |  |  |  |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

F Taper onto Auxillary Lane





# I-29 EXIT 2 NORTH SIOUX CITY 



## Probable Construction Costs

I-29 Exit 2 - Signalization and Access Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 19,000.00$ | $\$ 19,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 39,000.00$ | $\$ 39,000$ |
| Clearing | 1 | LUMP SUM | $\$ 8,000.00$ | $\$ 8,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | 5,640 | SQ. YD. | $\$ 7.39$ | $\$ 41,691$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 15,143 | CU. YD. | $\$ 5.30$ | $\$ 80,287$ |
| Base Course | 681 | TON | $\$ 10.64$ | $\$ 7,239$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (frontage rd) | 5,960 | SQ. YD. | $\$ 43.40$ | $\$ 258,634$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Drainage (18" RCP) | 30 | LF | $\$ 24.53$ | $\underline{9736}$ |
| Subtotal |  |  |  | $\$ 600,000$ |
| Contingencies |  |  |  |  |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 150,000$ |
| Total Project Costs |  |  |  | $\$ 750,000$ |



## Probable Construction Costs

I-29 Exit 2 - Roundabout and Access Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$20,000.00 | \$20,000 |
| Traffic Control | 1 | LUMP SUM | \$40,000.00 | \$40,000 |
| Clearing | 1 | LUMP SUM | \$8,000.00 | \$8,000 |
| Removal of Concrete Pavement | 333 | SQ. YD. | \$3.88 | \$1,294 |
| Removal of Asphalt Pavement | 5,862 | SQ. YD. | \$7.39 | \$43,334 |
| Remove Bridge | - | SQ. FT. | \$9.00 | \$0 |
| Borrow, Unclassified Excavation | 18,310 | CU. YD. | \$5.30 | \$97,079 |
| Base Course | 808 | TON | \$10.64 | \$8,599 |
| Asphalt Composite |  | TON | \$80.91 | \$0 |
| PCC Pavement 8" (cross street) | 7,447 | SQ. YD. | \$33.12 | \$246,641 |
| PCC Pavement 8" (ramps) |  | SQ. YD. | \$43.40 | \$0 |
| Concrete Approach Slab | - | SQ. YD. | \$188.34 | \$0 |
| Bridges |  | SQ. FT. | \$100.00 | \$0 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Traffic Signal | 0 | EACH | \$125,000.00 | \$0 |
| Roadway Lighting | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Drainage (18" RCP) | 180 | LF | \$24.53 | \$4,415 |
| Subtotal |  |  |  | \$490,000 |
| Contingencies | 25\% |  |  | \$122,500 |
| Total Probable Construction Costs |  |  |  | \$610,000 |
| Engineering, Administration | 15\% |  |  | \$91,500 |
| Total Project Costs |  |  |  | \$700,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 2 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 3 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | 150 | - | - |  |
| Superelevation (e max) | 6\% | - | - | - | - |  |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1432' | 1432' | 1432' | 1432' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Supports Impr. |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 0.47\% | 2.08\% | 2.11\% | - | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% |  | -2.70\% | -2.09\% | -0.89\% | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  | 37.0' |  |  | Acceptable |
| As Single Lane | 15 feet (19 for loops) | 19.5' |  | 18.5' | 19.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 1.5' | $4.0{ }^{\prime}$ | 3.0 ' | 2.5' | Supports Impr. |
| Left Shoulder | 2 feet | 2.5' | 5.0' | 2.5' | 1.5' | Supports Impr. |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 35:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 62:1 | - | 70:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 531 | 92 | 95 | 112 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 425 | 74 | 95 | 112 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 2962' | 446' | 457' | 1262' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To East |  | To West |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | - |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 73 |  | 73 |  | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 649 ' |  | 649 ' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 0.90\% |  | 0.90\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.00\% |  | 0.00\% |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 70' |  | 2201 |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Auxillary lane exits on to ramp $B$ and becomes right turn lane. Mainlne lane has option to exit which becomes a right turn lane Clear Zone meets 30' criteria but slopes are non recoverable within this distance
East ramp terminals are signalized


SDDOT Decennial Corridor, 09-104-01, 01/11/10


SDDOT Decennial Corridor, 09-104-01, 02/22/10


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# I-29 EXIT 26 VERMILLION/YANKTON 

North $\downarrow$ ป.nn6!!

## Probable Construction Costs I-29 Exit 26 - Signalization and Ramp Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 32,000.00$ | $\$ 32,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 65,000.00$ | $\$ 65,000$ |
| Clearing | 1 | LUMP SUM | $\$ 13,000.00$ | $\$ 13,000$ |
| Removal of Concrete Pavement |  | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | 7,684 | SQ. YD. | $\$ 7.39$ | $\$ 56,803$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 29,960 | CU. YD. | $\$ 5.30$ | $\$ 158,850$ |
| Base Course | 3,740 | TON | $\$ 10.64$ | $\$ 39,785$ |
| Asphalt Composite | 4,818 | TON | $\$ 80.91$ | $\$ 389,817$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) |  | SQ. YD. | $\$ 43.40$ | $\$ 0$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 20,000.00$ | $\$ 20,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Drainage (18" RCP) | 90 | LF | $\$ 24.53$ | $\$ 2,208$ |
| Subtotal |  |  |  | $\$ 910,000$ |
| Contingencies |  |  |  |  |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 227,500$ |
| Total Project Costs |  |  |  | $\$ 1,140,000$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 26 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | - | - | - | - |  |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 955' | 955' | 955' | 955' | Acceptable |
| Maximum Degree of Curvature (50 mph / 30 mph ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | <30' | <30' | <30' | <30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% |  | 3.77\% |  | 2.14\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.10\% |  | -2.01\% |  | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 20.0' | 19.0' | 26.0' | $22.0{ }^{\prime}$ | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 4.5' | 7.0' | 5.5' | 2.0 ' | Supports Impr. |
| Left Shoulder | 2 feet | 2.5' | 3.0' | 2.5 ' | 3.0' | Acceptable |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 28:1 | - | 28:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 29:1 | - | 30:1 | - | Supports Impr. |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - | 59 | - | - | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 175 | 55 | 90 | 68 | Supports Impr. |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 1219' | 299' | 913' | 419' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 185 |  | 185 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 110 |  | 67 |  | Supports Impr. |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 478' |  | 400' |  | Supports Impr. |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | ok |  | substandard |  | Supports Impr. |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 3.60\% |  | 4.00\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 1.00\% |  | 1.00\% |  | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300 / 660 feet | 570' |  | 570' |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

No superelevation in plans
Clear Zone meets 30' criteria but slopes are non recoverable within this distance
Ramp sight distance is limited by bridge rail.





SDDOT Decennial Corridor, 09-104-01, 01/21/10

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# I-29 EXIT 47 BERESFORD/IRENE 



## Probable Construction Costs <br> I-29 Exit 47 - Lane Addition and Signalization Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 3,000.00$ | $\$ 3,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 7,000.00$ | $\$ 7,000$ |
| Clearing | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 1,206 | CU. YD. | $\$ 5.30$ | $\$ 6,392$ |
| Base Course | 571 | TON | $\$ 10.64$ | $\$ 6,073$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) | 1,250 | SQ. YD. | $\$ 43.40$ | $\$ 54,244$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 0.00$ | $\$ 125,000.00$ |
| Traffic Signal | 2 | EACH | $\$ 250,000$ |  |
| Roadway Lighting | 1 | LUMP SUM | $\$ 0.00$ | $\$ 0$ |
| Drainage (18" RCP) | 60 | LF | $\$ 24.53$ | $\$ 1,472$ |
| Subtotal |  |  |  | $\$ 330,000$ |
|  |  |  |  | $\$ 82,500$ |
| Contingencies | $25 \%$ |  |  | $\$ 410,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 61,500$ |
| Engineering, Administration |  |  |  |  |
| Total Project Costs | $15 \%$ |  |  | $\$ 470,000$ |



## Probable Construction Costs I-29 Exit 47 - Roundabout Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 16,000.00$ | $\$ 16,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 32,000.00$ | $\$ 32,000$ |
| Clearing | 1 | LUMP SUM | $\$ 6,000.00$ | $\$ 6,000$ |
| Removal of Concrete Pavement | 5,716 | SQ. YD. | $\$ 3.88$ | $\$ 22,196$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 2,258 | CU. YD. | $\$ 5.30$ | $\$ 11,974$ |
| Base Course | 1,070 | TON | $\$ 10.64$ | $\$ 11,377$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 4,944 | SQ. YD. | $\$ 43.40$ | $\$ 214,564$ |
| PCC Pavement 8" (ramps) | 1,250 | SQ. YD. | $\$ 43.40$ | $\$ 54,244$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Traffic Signal | 0 | EACH | $\$ 125,000.00$ | $\$ 0$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Drainage (18" RCP) | 80 | LF | $\$ 24.53$ | $\$ 1,962$ |
| Subtotal |  |  |  | $\$ 390,000$ |
| Contingencies |  |  |  |  |
|  |  |  |  | $\$ 97,500$ |
| Total Probable Construction Costs |  |  |  | $\$ 490,000$ |
| Engineering, Administration | $15 \%$ |  |  | $\$ 73,500$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 47 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 6.20\% | 6.20\% | 6.20\% | 6.20\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | $833 / 231$ feet | 1432' | 1432' | 1432' | 1432' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00{ }^{\prime}$ | $4^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | <30' | <30' | <30' | <30' | Supports Impr. |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 2.99\% | - | 3.77\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.74\% | - | -2.97\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 16.0' | 16.0' | 16.0' | 15.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 6.5' | 7.5' | 7.0' | 8.0' | Supports Impr. |
| Left Shoulder | 2 feet | 2.5 | 1.0' | $2.5{ }^{\prime}$ | 2.0 ' | Supports Impr. |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 42:1 | - | 42:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 63:1 | - | 63:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 90 | 136 | 138 | 89 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 122 | 90 | 90 | 122 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 586' | 439' | 440' | 580' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 150 |  | 150 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 165 |  | 81 |  | Supports Impr. |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 569' |  | 386' |  | Supports Impr. |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | OK |  | Sub |  | Supports Impr. |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 3.14\% |  | 3.14\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 1.33\% |  | 0.57\% |  | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | >660' |  | 410' |  | Acceptable |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Plans show a curve not a taper so the taper is an estimate


SDDOT Decennial Corridor, 09-104-01, 03/02/10


SDDOT Decennial Corridor, 09-104-01, 02/22/10


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South Dakota Decennial Interstate Gorridor Study

PHASEONEREPORT

## I-29 EXIT 62 CANTON

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 62 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | - | 7.6\% | - | 8.0\% | Supports Impr. |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 955' | 955' | 955' | 955' | Acceptable |
| Maximum Degree of Curvature (50 mph / 30 mph ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 3.60\% | - | 3.33\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -1.60\% | - | -2.73\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 17.0' | 17.5' | 16.5' | 18.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.5' | 6.0' | 4.0' | 5.0' | Supports Impr. |
| Left Shoulder | 2 feet | 3.0' | 6.0' | 2.5 ' | 2.5' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 28:1 | - | 28:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 29:1 | - | 29:1 | - | Supports Impr. |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 256 | 101 | 140 | 100 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 98 | 77 | 98 | 82 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 366' | 375' | 461' | 371' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | East |  | West |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 150 |  | 150 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 148 |  | 100 |  | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 561' |  | 561' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 3.00\% |  | 3.00\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.00\% |  | 0.30\% |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300 / 660 feet | 550' |  | >660' |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments


SDDOT Decennial Corridor, 09-104-01, 02/22/10


SDDOT Decennial Corridor, 09-104-01, 01/11/10


SDDOT Decennial Corridor, 09-104-01, 02/22/10

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## I-29 EXIT 71 HARRISBURG/TEA

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 71 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | - | - | - | - |  |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1432' | 955' | 955' | 1432' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $4^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 2.17\% | - | 1.57\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -1.26\% | - | -3.24\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  |  |  |  |  |
| As Single Lane | 15 feet (19 for loops) | 17.5' | 17.0' | 15.5' | 18.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.0' | 3.5' | 4.0 ' | 3.0' | Supports Impr. |
| Left Shoulder | 2 feet | 3.5' | 2.5' | 4.0 ' | 2.0' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 29:1 | - | 29:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 29:1 | - | 29:1 | - | Supports Impr. |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - | 230 | 197 | - | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 156 | 79 | 102 | 99 | Supports Impr. |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | >425' | 583' | 538' | 1459' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 76 |  | 101 |  | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 80 |  | 80 |  | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 414' |  | 415' |  | Supports Impr. |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | substandard |  | substandard |  | Supports Impr. |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 4.00\% |  | 4.00\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.86\% |  | 0.34\% |  | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 150' |  | 460' |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments


SDDOT Decennial Corridor, 09-104-01, 01/11/10


SDDOT Decennial Corridor, 09-104-01, 02/22/10


SDDOT Decennial Corridor, 09-104-01, 02/22/10

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South Dakota Decennial Interstate Gorridor Study

PHASEONEREPORT

## I-29 EXIT 77 41 ${ }^{\text {ST }}$ STREET



## Probable Construction Costs <br> I-29 Exit 77 - Single Point Urban Interchange

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 275,000.00$ | $\$ 275,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 549,000.00$ | $\$ 549,000$ |
| Clearing | 1 | LUMP SUM | $\$ 110,000.00$ | $\$ 110,000$ |
| Removal of Concrete Pavement | 22,318 | SQ. YD. | $\$ 3.88$ | $\$ 86,662$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | 21,960 | SQ. FT. | $\$ 9.00$ | $\$ 197,640$ |
| Borrow, Unclassified Excavation | 16,039 | CU. YD. | $\$ 5.30$ | $\$ 85,038$ |
| Base Course | 6,177 | TON | $\$ 10.64$ | $\$ 65,708$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 14,793 | SQ. YD. | $\$ 33.12$ | $\$ 489,970$ |
| PCC Pavement 8" (ramps) | 12,069 | SQ. YD. | $\$ 43.40$ | $\$ 523,754$ |
| Concrete Approach Slab | 10,000 | SQ. YD. | $\$ 188.34$ | $\$ 1,883,420$ |
| Bridges | 20,672 | SQ. FT. | $\$ 100.00$ | $\$ 2,067,200$ |
| Guard Rail | 900 | LF | $\$ 100.00$ | $\$ 90,000$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 160,000.00$ | $\$ 160,000$ |
| Traffic Signal | 1 | EACH | $\$ 175,000.00$ | $\$ 175,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 110,000.00$ | $\$ 110,000$ |
| Drainage (18" RCP) | 180 | LF | $\$ 24.53$ | $\$ 4,415$ |
| Subtotal |  |  |  | $\$ 6,870,000$ |
|  |  |  |  |  |
| Contingencies | $25 \%$ |  |  | $\$ 1,717,500$ |
|  |  |  |  | $\$ 8,590,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 1,288,500$ |
| Engineering, Administration | $15 \%$ |  |  | $\$ 9,880,000$ |



## Probable Construction Costs I-29 Exit 77 - Diverging Diamond Interchange

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 61,000.00$ | $\$ 61,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 123,000.00$ | $\$ 123,000$ |
| Clearing | 1 | LUMP SUM | $\$ 25,000.00$ | $\$ 25,000$ |
| Removal of Concrete Pavement | 15,943 | SQ. YD. | $\$ 3.88$ | $\$ 61,906$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 13,963 | CU. YD. | $\$ 5.30$ | $\$ 74,032$ |
| Base Course | 5,787 | TON | $\$ 10.64$ | $\$ 61,557$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 13,396 | SQ. YD. | $\$ 33.12$ | $\$ 443,674$ |
| PCC Pavement 8" (ramps) | 11,300 | SQ. YD. | $\$ 43.40$ | $\$ 490,364$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 900 | LF | $\$ 100.00$ | $\$ 90,000$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 40,000.00$ | $\$ 40,000$ |
| Traffic Signal | 2 | EACH | $\$ 125,000.00$ | $\$ 250,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 20,000.00$ | $\$ 20,000$ |
| Drainage (18" RCP) | 180 | LF | $\$ 24.53$ | $\$ 4,415$ |
| Subtotal |  |  |  | $\$ 1,740,000$ |
| Contingencies |  |  |  | $\$ 435,000$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 2,180,000$ |
| Total Project Costs |  |  |  | $\$ 327,000$ |



## Probable Construction Costs I-29 Exit 77 - Diverging Diamond Interchange

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 319,000.00$ | $\$ 319,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 637,000.00$ | $\$ 637,000$ |
| Clearing | 1 | LUMP SUM | $\$ 127,000.00$ | $\$ 127,000$ |
| Removal of Concrete Pavement | 16,153 | SQ. YD. | $\$ 3.88$ | $\$ 62,721$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | 23,040 | SQ. FT. | $\$ 9.00$ | $\$ 207,360$ |
| Borrow, Unclassified Excavation | 13,963 | CU. YD. | $\$ 5.30$ | $\$ 74,032$ |
| Base Course | 5,741 | TON | $\$ 10.64$ | $\$ 61,071$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 12,418 | SQ. YD. | $\$ 33.12$ | $\$ 411,289$ |
| PCC Pavement 8" (ramps) | 11,300 | SQ. YD. | $\$ 43.40$ | $\$ 490,364$ |
| Concrete Approach Slab | 11,600 | SQ. YD. | $\$ 188.34$ | $\$ 2,184,767$ |
| Bridges | 27,840 | SQ. FT. | $\$ 100.00$ | $\$ 2,784,000$ |
| Guard Rail | 900 | LF | $\$ 100.00$ | $\$ 90,000$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 190,000.00$ | $\$ 190,000$ |
| Traffic Signal | 2 | EACH | $\$ 125,000.00$ | $\$ 250,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 130,000.00$ | $\$ 130,000$ |
| Drainage (18" RCP) | 180 | LF | $\$ 24.53$ | $\$ 4,415$ |
| Subtotal |  |  |  | $\$ 8,020,000$ |
|  |  |  |  |  |
| Contingencies | $25 \%$ |  |  | $\$ 2,005,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 10,030,000$ |
| Engineering, Administration | $15 \%$ |  |  | $\$ 1,504,500$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 77 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 2 |  |
| Right Turn Storage Length |  | - | - | - | 380' |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | - | - | - | - |  |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 2292' | 955' | 955' | 1146' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $2^{\circ} 30^{\prime}$ | $6^{\circ} 00^{\prime}$ | $6^{\circ} 00^{\prime}$ | $5^{\circ} 00{ }^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 1.60\% |  | 3.45\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.55\% |  | 4.00\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | 22 | - | - | 36.5 | Acceptable |
| As Single Lane | 15 feet (19 for loops) | - | 18.5' | 16.5' | - | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 6.0' | 4.5' | 5.0' | 7.5' | Supports Impr. |
| Left Shoulder | 2 feet | 2.5' | 2.0 ' | 2.0' | 2.0' | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 4:1 | 6:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 23:1 | - | 25:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | - | 29:1 | - | Supports Impr. |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 |  | 185 | 100 | 121 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 151 | 144 | 80 | - | Supports Impr. |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 526' | >425' | 367' | 754' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 100 |  | 100 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | - |  | 100 |  | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | >425' |  | 444' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 0.00\% |  | 4.00\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.00\% |  | 0.00\% |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 200' |  | 400' |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Ramp D has 2 lanes exiting. The outer lane is an auxiliary lane exiting. Both lanes turn left
Ramp A has an auxiliary lane for the on ramp
Ramp B has an unstriped right turn lane.


SDDOT Decennial Corridor, 09-104-01, 02/22/10


SDDOT Decennial Corridor, 09-104-01, 02/22/10


SDDOT Decennial Corridor, 09-104-01, 03/02/10



SDDOT Decennial Corridor, 09-104-01, 03/02/10


SDDOT Decennial Corridor, 09-104-01, 02/24/10

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# I-29 EXIT 86 RENNER/CROOKS 

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 86 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  |  |  |  |  |  |
| Left Turn Storage Length |  |  |  |  |  |  |
| Superelevation (e max) | 6\% | 3.00\% | 5.00\% | 3.00\% | 5.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | < 30' | < 30' | < 30' | < 30' | Supports Impr. |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 2.90\% | - | 3.57\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.59\% | - | -4.61\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 16.5' | 18.0' | 17.5' | 15.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 5.5' | 5.0' | 4.0' | 6.5' | Supports Impr. |
| Left Shoulder | 2 feet | 3.5' | 3.5' | 2.5 | 1.0' | Supports Impr. |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 41:1 | - | 41:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 62:1 | - | 62:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 192 | 285 | 129 | 117 | Acceptable |
| Minimum for a Sag Vertical Curve (50 mph / 30 mph ) | $96 / 37$ | 221 | 193 | 152 | 154 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 719' | 835' | 547' | 570' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To | Vest | To | ast |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 14 |  | 17 | 1 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 |  |  | 397 | 7 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet |  | 1 ' | 62 |  | Acceptable |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | O |  | O |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 2.9 |  | 4.2 | \% | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 1.3 | \% | 3.4 | \% | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300 / 660 feet | 65 |  | 25 | $0^{\prime}$ | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments


SDDOT Decennial Corridor, 09-104-01, 01/08/10


SDDOT Decennial Corridor, 09-104-01, 02/24/10


SDDOT Decennial Corridor, 09-104-01, 02/24/10

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South Dakota Decennial Interstate Corridor Study

PHASE ONE REPORT

## I-29 EXIT 98 DELL RAPIDS

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 98 |
| Analyst: | MBM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 3.00\% | - | - | 5.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53 ' / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 2.10\% | - | 4.10\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.14\% | - | -3.82\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 16.0' | 15.5' | 16.0' | 15.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.0' | 5.5' | 5.5' | 5.0' | Supports Impr. |
| Left Shoulder | 2 feet | 3.0' | 3.5' | 3.5' | 5.5' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 40:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 61:1 | - | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - | 108 | 172 | 90 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 503 | 385 | 150 | 141 | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | >425' | 537' | 770' | 1,322' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 220 |  | 220 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | - |  | - |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 689' |  | 689' |  | Acceptable |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 0.54\% |  | 3.69\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300 / 660 feet | $250 '$ |  | 650' |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments


SDDOT Decennial Corridor, 09-104-01, 01/08/10


SDDOT Decennial Corridor, 09-104-01, 02/24/10


SDDOT Decennial Corridor, 09-104-01, 01/08/10

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# I-229 EXIT 2 WESTERN AVE 



## Probable Construction Costs

l-229 Exit 2 - Lane Addition and Striping Plan

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 2,000.00$ | $\$ 2,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 3,00000$ | $\$ 3,000$ |
| Clearing | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Removal of Concrete Pavement |  | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 3,049 | CU. YD. | $\$ 5.30$ | $\$ 16,165$ |
| Base Course | 20 | TON | $\$ 10.64$ | $\$ 216$ |
| Asphalt Composite | - | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (Cross St) | 400 | SQ. YD. | $\$ 43.40$ | $\$ 17,358$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Traffic Signal | 0 | EACH | $\$ 125,000.00$ | $\$ 0$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 0.00$ | $\$ 0$ |
| Drainage (18" RCP) | 15 | LF | $\$ 24.53$ | $\$ 368$ |
| Subtotal |  |  |  | $\$ 40,000$ |
| Contingencies |  |  |  | $\$ 10,000$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 50,000$ |
| Total Project Costs |  |  |  | $\$ 7,500$ |



## Probable Construction Costs

I-229 Exit 2 - Single Point Urban Interchange

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$353,000.00 | \$353,000 |
| Traffic Control | 1 | LUMP SUM | \$706,000.00 | \$706,000 |
| Clearing | 1 | LUMP SUM | \$141,000.00 | \$141,000 |
| Removal of Concrete Pavement | 5,400 | SQ. YD. | \$3.88 | \$20,968 |
| Removal of Asphalt Pavement |  | SQ. YD. | \$7.39 | \$0 |
| Remove Bridge | 27,840 | SQ. FT. | \$9.00 | \$250,560 |
| Borrow, Unclassified Excavation | 105,531 | CU. YD. | \$5.30 | \$559,525 |
| Base Course | 4,422 | TON | \$10.64 | \$47,032 |
| Asphalt Composite |  | TON | \$80.91 | \$0 |
| PCC Pavement 8" (cross street) | 6,320 | SQ. YD. | \$33.12 | \$209,325 |
| PCC Pavement 8" (ramps) | 9,681 | SQ. YD. | \$43.40 | \$420,088 |
| Concrete Approach Slab | 9,600 | SQ. YD. | \$188.34 | \$1,808,083 |
| Bridges | 36,480 | SQ. FT. | \$100.00 | \$3,648,000 |
| Guard Rail | 900 | LF | \$100.00 | \$90,000 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$210,000.00 | \$210,000 |
| Traffic Signal | 1 | EACH | \$125,000.00 | \$125,000 |
| Roadway Lighting | 1 | LUMP SUM | \$140,000.00 | \$140,000 |
| Drainage (18" RCP) | 90 | LF | \$24.53 | \$2,208 |
| Subtotal |  |  |  | \$8,730,000 |
| Contingencies | 25\% |  |  | \$2,182,500 |
| Total Probable Construction Costs |  |  |  | \$10,910,000 |
| Engineering, Administration | 15\% |  |  | \$1,636,500 |
| Total Project Costs |  |  |  | \$12,550,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-229 |
| :--- | :---: |
| Interchange: | Exit 2 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | --------- |
| Design Speed | $50 \mathrm{mph} * *$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | 250' | - | 250' | - |  |
| Left Turn Storage Length |  | 250' | - | 250' | - |  |
| Superelevation (e max) | 6\% | - | - | - | - |  |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833 / 231 feet | 1432' | 1637' | 716' | 716' | Supports Impr. |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $4^{\circ} 00^{\prime}$ | $3^{\circ} 30^{\prime}$ | $8^{\circ} 00^{\prime}$ | $8^{\circ} 00^{\prime}$ | Supports Impr. |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | $>30^{\prime}$ | $>30^{\prime}$ | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | $+3 \%$ to $+5 \%$ | 3.29\% | - | 4.35 | - | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | -2.35\% | - | -2.80\% | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | 25.5 ' | 29.0' | 27.0' | 28.0' | Acceptable |
| As Single Lane | 15 feet (19 for loops) |  |  |  |  |  |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 4.0' | $2.0{ }^{\prime}$ | 1.5 | 3.0 ' | Supports Impr. |
| Left Shoulder | 2 feet | $1.5{ }^{\prime}$ | $1.5{ }^{\prime}$ | $2.0^{\prime}$ | 2.0' | Supports Impr. |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | - | - | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | - | - | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 72 | 93 | 61 | 62 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 341' | 463' | 298' | 301' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To | North | To | South |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ |  | 16 |  |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ |  | 4 |  | 20 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet |  | ' |  | $2^{\prime}$ | Supports Impr. |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) ${ }^{* * *}$ | 425/200 feet | subst | andard | subst | andard | Supports Impr. |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  | 6\% |  |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% |  | 0\% |  | \% | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet |  | '0' |  | ' | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Auxilary lanes are on either side of the interchange that continue to next ramp going both directions.
Plans show new grading over parts with new pavement 6:1
Rt \& Lt storage lengths measured off of aerial photo

$X X X(X X X)=A M(P M)$ Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 02/24/10

$X X X(X X X)=A M(P M)$ Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 02/24/10

$X X X(X X X)=A M(P M)$ Peak Hour Traffic Volumes



# I-229 EXIT 3 MINNESOTA AVE 

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-229 |
| :--- | :---: |
| Interchange: | Exit 3 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |




## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Auxilary lanes are on either side of the interchange that continue to next ramp going both directions.
Plans show 6:1 grading over parts with new pavement
Ramp A has vertical spline to interstate
Ramp terminals are signalized






South Dakota Decennial Interstate Gorridor Study

PHASEONEREPORT

## I-229 EXIT 4 CLIFF AVE



## Probable Construction Costs <br> I-229 Exit 4 - Lane Addition

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 2,000.00$ | $\$ 2,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 4,000.00$ | $\$ 4,000$ |
| Clearing | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Removal of Concrete Pavement |  | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 2,014 | CU. YD. | $\$ 5.30$ | $\$ 10,681$ |
| Base Course | 152 | TON | $\$ 10.64$ | $\$ 1,619$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 367 | SQ. YD. | $\$ 33.12$ | $\$ 12,144$ |
| PCC Pavement 8" (ramps) | 333 | SQ. YD. | $\$ 43.40$ | $\$ 14,465$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 0.00$ | $\$ 125,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 0.00$ | $\$ 0$ |
| Drainage (18" RCP) | 30 | LF | $\$ 24.53$ | $\$ 736$ |
| Subtotal |  |  |  | $\$ 170,000$ |
| Contingencies |  |  |  | $\$ 42,500$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 210,000$ |
| Total Project Costs |  |  |  | $\$ 31,500$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-229 |
| :--- | :---: |
| Interchange: | Exit 4 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |




## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Auxilary lanes are on either side of the interchange that continue to next ramp going both directions.
Plans show new grading over parts with new pavement 6:1
Ramp A has a vertical spline off interstate on origianl plans. As bulit plans show a small curve at that point witha 508' SSD
Plans show 3:1 max slope on typicals
South ramp terminals is signalized, north off-ramp terminal is signalized, north on-ramp terminal not signalized


## LEGEND

 $\left.\left.\begin{array}{rl}\mathbf{X} / \mathbf{X}= & \text { AM/PM Peak Hour Signalized } \\ & \text { Movement Level of Service }\end{array}\right\}=\begin{array}{l}\text { AM/PM Peak Hour Unsignalized } \\ \text { Movement Level of Service }\end{array}\right\}$


## LEGEND






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South Dakota Decennial Interstate Gorridor Study

PHASEONEREPORT

## I-229 EXIT 5 $26^{\mathrm{TH}}$ STREET



## Probable Construction Costs

I-229 Exit 5 - Cross Road and Ramp Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
| Mobilization |  |  |  |  |
| Traffic Control | 1 | LUMP SUM | $\$ 247,000.00$ | $\$ 247,000$ |
| Clearing | 1 | LUMP SUM | $\$ 493,000.00$ | $\$ 493,000$ |
| Removal of Concrete Pavement | 20,365 | SQ. YD. | $\$ 99,000.00$ | $\$ 99,000$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 3.88$ | $\$ 79,077$ |
| Remove Bridge | 23,200 | SQ. FT. | $\$ 7.39$ | $\$ 9.00$ |
| Borrow, Unclassified Excavation | 22,575 | CU. YD. | $\$ 208,800$ |  |
| Base Course | 4,477 | TON | $\$ 5.30$ | $\$ 119,693$ |
| Asphalt Composite |  | TON | $\$ 10.64$ | $\$ 47,618$ |
| PCC Pavement 8" (cross street) | 10,516 | SQ. YD. | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (ramps) | 8,236 | SQ. YD. | $\$ 33.12$ | $\$ 348,286$ |
| Concrete Approach Slab | 6,400 | SQ. YD. | $\$ 43.40$ | $\$ 357,406$ |
| Bridges | 25,600 | SQ. FT. | $\$ 188.34$ | $\$ 1,205,389$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 2,560,000$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 100.00$ | $\$ 0,000.00$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 150,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 100,000.00$ | $\$ 100,000$ |
| Drainage (18" RCP) | 180 | LF | $\$ 24.53$ | $\$ 4,415$ |
|  |  |  |  | $\$ 6,140,000$ |
| Subtotal |  |  |  | $\$ 1,535,000$ |
| Contingencies |  |  |  |  |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  | $\$ 7,680,000$ |  |
| Total Project Costs |  |  | $\$ 152,000$ |  |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-229 |
| :--- | :---: |
| Interchange: | Exit 5 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Partial Cloverleaf |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  |  | 200' |  |  |  |
| Left Turn Storage Length |  |  | 200' |  |  |  |
| Superelevation (e max) | 6\% | 5.6\% | 5.6\% | 4.0\% | 5.0\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 205' | 1145' | 212' | 230' | Supports Impr |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $28^{\circ}$ | $5^{\circ}$ | $27^{\circ} 01^{\prime}$ | $24^{\circ} 54^{\prime}$ | Supports Impr |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 3.57\% | - |  | 2.69\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | -1.96\% | -3.52\% |  | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 19.0' | 20.0' | 20.0' | 24.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 2.5 | 2.5 | 1.5' | - | Supports Impr. |
| Left Shoulder | 2 feet | 3.0' | 2.0' | 3.0' | - | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | - | - | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | - | - | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 133 | 270 | 30 | 82 | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 185 | 413 | 51 | 91 | Supports Impr. |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 747' | 1551' | 257' | 406' | Supports Impr. |
| Cross Road Features v |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To West |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | - |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | - |  | - |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | - |  | - |  |  |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | - |  | - |  |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | - |  | - |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 260' |  | 670' |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Auxillary lanes on and off are present in each direction for on and off ramp
No cross road info
East ramp terminal is signalized







SDDOT Decennial Corridor, 09-104-01, 03/04/10

## LEGEND

$X X X(X X X)=A M(P M)$ Peak Hour Traffic Volumes


## LEGEND

$$
\begin{aligned}
\mathbf{X} / \mathbf{X}= & \text { AM/PM Peak Hour Signalized } \\
& \text { Movement Level of Service }
\end{aligned}
$$

$\mathbf{X} / \mathbf{X}=$ AM/PM Peak Hour Ramp Junction Level of Service
$8=$ Traffic Signal
$=$ Travel Lanes


Interstate 229 Exit 5

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South Dakota Decennial Interstate Corridor Study

PHASEONEREPORT

## I-229 EXIT 7 RICE STREET



## Probable Construction Costs

I-229 Exit 7 - Ramp Reconstruction and Cross Road Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 29,000.00$ | $\$ 29,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 58,000.00$ | $\$ 58,000$ |
| Clearing | 1 | LUMP SUM | $\$ 12,000.00$ | $\$ 12,000$ |
| Removal of Concrete Pavement | 10,254 | SQ. YD. | $\$ 3.88$ | $\$ 39,818$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 14,575 | CU. YD. | $\$ 5.30$ | $\$ 77,274$ |
| Base Course | 1,391 | TON | $\$ 10.64$ | $\$ 14,791$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 9,516 | SQ. YD. | $\$ 33.12$ | $\$ 315,165$ |
| PCC Pavement 8" (ramps) | 3,044 | SQ. YD. | $\$ 43.40$ | $\$ 132,114$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 20,000.00$ | $\$ 20,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 10,000.00$ | $\$ 10,000$ |
| Drainage (18" RCP) | 150 | LF | $\$ 24.53$ | $\$ 3,680$ |
|  |  |  |  | $\$ 840,000$ |
| Subtotal |  |  |  | $\$ 1000$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-229 |
| :--- | :---: |
| Interchange: | Exit 7 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Folded Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  |  | - |  |  |  |
| Left Turn Storage Length |  |  | 125' |  |  |  |
| Superelevation (e max) | 6\% | 5.9\% | 5.9\% | 6.0\% | 5.5\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 955' | 160' | 160' | 939' | Supports Impr |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $6^{\circ} 00^{\prime}$ | $35^{\circ} 48^{\prime}$ | $35^{\circ} 48^{\prime}$ | $6^{\circ} 06^{\prime}$ | Supports Impr |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 3.57\% | - | 5.34\% |  | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | -1.96\% |  | -1.61\% | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 15.5' | 18.0' | 20.0' | 15.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 6.0' | 4.0' | 3.0' | 5.5' | Supports Impr. |
| Left Shoulder | 2 feet | 2.5' | 3.5' | 3.0 ' | 3.5' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 5:1 | 5:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | - | - | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | - | - | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 133 | 270 | 30 | 82 | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 185 | 413 | 51 | 91 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 747' | 1551' | 257' | 406' | Supports Impr. |
| Cross Road Features v |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | - |  | - |  |  |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | - |  | - |  |  |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | - |  | - |  |  |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | - |  | - |  |  |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 450' |  | 350' |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

No taper on and off. Auxillary lanes on and off are present in each direction for on and off ramp[
New pavement on cross road from aerial. No information included with plans
East Ramp terminal is signalized, west is not




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# I-229 EXIT 9 BENSON ROAD 



## Probable Construction Costs

I-229 Exit 9 - Lane Addition Signalization Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$5,000.00 | \$5,000 |
| Traffic Control | 1 | LUMP SUM | \$10,000.00 | \$10,000 |
| Clearing | 1 | LUMP SUM | \$2,000.00 | \$2,000 |
| Removal of Concrete Pavement |  | SQ. YD. | \$3.88 | \$0 |
| Removal of Asphalt Pavement | - | SQ. YD. | \$7.39 | \$0 |
| Remove Bridge | - | SQ. FT. | \$9.00 | \$0 |
| Borrow, Unclassified Excavation | 4,708 | CU. YD. | \$5.30 | \$24,963 |
| Base Course | 244 | TON | \$10.64 | \$2,591 |
| Asphalt Composite |  | TON | \$80.91 | \$0 |
| PCC Pavement 8" (cross street) | 1,067 | SQ. YD. | \$43.40 | \$46,288 |
| PCC Pavement 8" (ramps) | 533 | SQ. YD. | \$43.40 | \$23,144 |
| Concrete Approach Slab | - | SQ. YD. | \$188.34 | \$0 |
| Bridges | - | SQ. FT. | \$100.00 | \$0 |
| Guard Rail | 0 | LF | \$100.00 | \$0 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$0.00 | \$0 |
| Traffic Signal | 1 | EACH | \$125,000.00 | \$125,000 |
| Roadway Lighting | 1 | LUMP SUM | \$0.00 | \$0 |
| Drainage (18" RCP) | 45 | LF | \$24.53 | \$1,104 |
| Subtotal |  |  |  | \$240,000 |
| Contingencies | 25\% |  |  | \$60,000 |
| Total Probable Construction Costs |  |  |  | \$300,000 |
| Engineering, Administration | 15\% |  |  | \$45,000 |
| Total Project Costs |  |  |  | \$350,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-229 |
| :--- | :---: |
| Interchange: | Exit 9 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | --------- |
| Design Speed | $50 \mathrm{mph} * *$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 2 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 4.0\% | 4.0\% | 4.0\% | 4.0\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833 / 231 feet | 2291' | 2291' | 2291' | 2291' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $2^{\circ} 30^{\prime}$ | $2^{\circ} 30^{\prime}$ | $2^{\circ} 30^{\prime}$ | $2^{\circ} 30^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | $>30^{\prime}$ | $>30^{\prime}$ | $>30^{\prime}$ | $>30^{\prime}$ | Acceptable |
| Maximum Grade on Ramp (Ascending) | $+3 \%$ to $+5 \%$ |  | 1.27\% |  | 2.66\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | 3.25\% |  | 1.45\% |  | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | 25.0 | - | - | Acceptable |
| As Single Lane | 15 feet (19 for loops) | 15.5' | - | 15.0' | 22.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 7.5' | - | 8.0' | 1.0' | Supports Impr. |
| Left Shoulder | 2 feet | $2.0^{\prime}$ | 0.0' | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | Supports Impr. |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 |  |  |  | 20:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 50:1 |  |  |  | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 123 | 158 | 101 | 267 | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 524' | 650' | 446' | 1036' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | North |  | South |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $84 / 19$ | 224 |  | 449 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | - |  | 244 ' |  | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425/200 feet | 859' |  | $859 '$ |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425/200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 2.3\% |  | 0.8\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.8\% |  | 0.7\% |  | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | $>300^{\prime}$ |  | $>300^{\prime}$ |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Ramp B \& C have an auxillary lanes entering and exiting
East ramp terminal is signalized and west ramp terminal is not



SDDOT Decennial Corridor, 09-104-01, 02/25/10


SDDOT Decennial Corridor, 09-104-01, 03/02/10

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 98 |
| Analyst: | MBM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 3.00\% | - | - | 5.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 2.10\% | - | 4.10\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.14\% | - | -3.82\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 16.0' | 15.5' | 16.0' | 15.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.0' | 5.5' | 5.5' | 5.0' | Supports Impr. |
| Left Shoulder | 2 feet | $3.0{ }^{\prime}$ | 3.5' | 3.5' | 5.5' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 40:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 61:1 | - | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - | 108 | 172 | 90 | Acceptable |
| Minimum for a Sag Vertical Curve (50 mph / 30 mph ) | $96 / 37$ | 503 | 385 | 150 | 141 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | >425' | 537' | 770' | 1,322' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 220 |  | 220 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | - |  | - |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 689' |  | 689' |  | Acceptable |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 0.54\% |  | 3.69\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300 / 660 feet | 250' |  | $650 '$ |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments


SDDOT Decennial Corridor, 09-104-01, 01/08/10


SDDOT Decennial Corridor, 09-104-01, 02/24/10


SDDOT Decennial Corridor, 09-104-01, 01/08/10

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# I-90 EXIT 330 MITCHELL/HURON 



## Probable Construction Costs

I-90 Exit 330 - Lane Addition and Signalization Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 3,000.00$ | $\$ 3,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 7,000.00$ | $\$ 7,000$ |
| Clearing | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 1,206 | CU. YD. | $\$ 5.30$ | $\$ 6,392$ |
| Base Course | 571 | TON | $\$ 10.64$ | $\$ 6,073$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) | 1,250 | SQ. YD. | $\$ 43.40$ | $\$ 54,244$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 0.00$ | $\$ 125,000.00$ |
| Traffic Signal | 2 | EACH | $\$ 250,000$ |  |
| Roadway Lighting | 1 | LUMP SUM | $\$ 0.00$ | $\$ 0$ |
| Drainage (18" RCP) | 60 | LF | $\$ 24.53$ | $\$ 1,472$ |
| Subtotal |  |  |  | $\$ 330,000$ |
|  |  |  |  | $\$ 82,500$ |
| Contingencies | $25 \%$ |  |  | $\$ 410,000$ |
| Total Probable Construction Costs |  |  |  | $\$ 61,500$ |
| Engineering, Administration |  |  |  |  |
| Total Project Costs |  |  |  |  |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 330 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  |  |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 5.0\% | 3.0\% | 5.0\% | 3.0\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | $833 / 231$ feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 1.08\% | - | 2.26\% | - | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | -1.12\% | - | -1.81\% | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 18.0' | 18.0' | 18.0' | 18.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 4.0' | 4.0' | 4.0' | 5.0' | Supports Impr. |
| Left Shoulder | 2 feet | 4.0' | 4.0 ' | 4.0 ' | 4.0 ' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 40:1 | - | 41:1 | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | 61:1 | - | 63:1 | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 796 | - | 234 | - | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 176 | 234 | 182 | 250 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 1246' | >425' | 830' | >425' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To North |  | To South |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 264 |  | 264 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 262 |  | 175 |  | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 754' |  | 754' |  | Acceptable |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 2.50\% |  | 3.00\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.02\% |  | 0.14\% |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 420' |  | 620' |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments



SDDOT Decennial Corridor, 09-104-01, 02/24/10



SDDOT Decennial Corridor, 09-104-01, 02/24/10


SDDOT Decennial Corridor, 09-104-01, 01/14/10

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# I-90 EXIT 332 MITCHELL/PARKSTON 

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 332 |
| Analyst: | MBM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | $\mathbf{A}$ | $\mathbf{B}$ | $\mathbf{C}$ | D |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Achieved? |  |  |  |  |  |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  |

Comments

$X X X(X X X)=A M(P M)$ Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 01/06/10

$X X x(X X X)=A M(P M)$ Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 01/06/10

xxx(xXx) = AM(PM) Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 01/06/10

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South Dakota Decennial Interstate Gorridor Study

PHASEONEREPORT

## I-90 EXIT 387 HARTFORD

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 387 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  |  |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  |  | - |  | - |  |
| Left Turn Storage Length |  |  | - | - | - |  |
| Superelevation (e max) | 6\% | 4.2\% | 4.2\% | 4.2\% | 4.2\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 833/231 feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to $+5 \%$ | 1.35\% | - | 0.92\% | 1.11\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | -1.50\% | -1.08\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet |  | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 15.5' | 14.5' | 14.0' | 14.0' | Supports Impr. |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 6.0' | 5.0' | 6.0' | 5.0' | Supports Impr. |
| Left Shoulder | 2 feet | 1.5' | 1.0' | 1.0' | 2.0' | Supports Impr. |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 38:1 | - | 38:1 | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | 61:1 | - | 61:1 | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 |  |  |  |  |  |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 388 | 191 | 250 | 233 | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | >425' | >425' | 2,820' | >425' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To North |  | To South |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84/19 | 150 |  | 150 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | - |  | - |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 569' |  | 569' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 4.00\% |  | 3.00\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | $550 '$ |  | $300 '$ |  | Acceptable |

## ${ }^{* *}$ Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments





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South Dakota Decennial Interstate Gorridor Study

PHASE ONE REPORT

## I-90 EXIT 390 HARTFORD

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 390 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Folded Diamond |  |  |  |  |  |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 6\% | 5\% | 6\% | 6\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1432' | 955' | 252' | 252' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $4^{\circ} 00^{\prime}$ | $6^{\circ} 00{ }^{\prime}$ | $22^{\circ} 34^{\prime}$ | $22^{\circ} 34^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 2.22\% | 3.54\% |  | 2.74\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.47\% | -2.34\% | -3.33\% |  | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 16.5' | 15.5' | 15.0' | 14.5' | Supports Impr. |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 7.0' | 4.5' | 6.5' | 7.5' | Supports Impr. |
| Left Shoulder | 2 feet | 2.0' | 2.5' | 2.0 ' | 2.0' | Acceptable |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 41:1 | - | - | 41:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | 61:1 | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 213 | 77 | - | - | Supports Impr. |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | - | - | 72 | 109 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 776' | 407' | 380' | 617' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To North |  | To South |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | - |  | Not Available |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | - |  | - |  | Not Available |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | - |  | - |  | Not Available |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | - |  | - |  | Not Available |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | - |  | - |  | Not Available |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  | Not Available |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 400' |  | 400' |  | Acceptable |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments

No cross road information in plans

# I-90 EXIT 406 BRANDON/CORSON 



Probable Construction Costs
I-90 Exit 406 - Lane Addition, Signalization Improvements, Bridge Replacement

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 158,000.00$ | $\$ 158,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 316,000.00$ | $\$ 316,000$ |
| Clearing | 1 | LUMP SUM | $\$ 63,000.00$ | $\$ 63,000$ |
| Removal of Concrete Pavement | 2,477 | SQ. YD. | $\$ 3.88$ | $\$ 9,619$ |
| Removal of Asphalt Pavement |  | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | 8,840 | SQ. FT. | $\$ 9.00$ | $\$ 79,560$ |
| Borrow, Unclassified Excavation | 1,206 | CU. YD. | $\$ 5.30$ | $\$ 6,392$ |
| Base Course | 571 | TON | $\$ 10.64$ | $\$ 6,073$ |
| Asphalt Composite | - | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 8" (cross street) | 4,911 | SQ. YD. | $\$ 33.12$ | $\$ 162,661$ |
| PCC Pavement 8" (ramps) | 1,250 | SQ. YD. | $\$ 33.40$ | $\$ 54,244$ |
| Concrete Approach Slab | 5,200 | SQ. YD. | $\$ 188.34$ | $\$ 979,378$ |
| Bridges | 17,680 | SQ. FT. | $\$ 100.00$ | $\$ 1,768,000$ |
| Guard Rail | 900 | LF | $\$ 100.00$ | $\$ 90,000$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 90,000.00$ | $\$ 90,000$ |
| Traffic Signal | 2 | EACH | $\$ 125,000.00$ | $\$ 250,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 60,000.00$ | $\$ 60,000$ |
| Drainage (18" RCP) | 110 | LF | $\$ 24.53$ | $\$ 2,698$ |
| Subtotal |  |  |  | $\$ 4,100,000$ |
| Contingencies |  |  |  | $\$ 1,025,000$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 5,130,000$ |
| Total Project Costs |  |  |  | $\$ 769,500$ |



## Probable Construction Costs

 I-90 Exit 406 - Singe Point Urban Interchange| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :---: | :---: | :---: | :---: | :---: |
| Mobilization | 1 | LUMP SUM | \$259,000.00 | \$259,000 |
| Traffic Control | 1 | LUMP SUM | \$517,000.00 | \$517,000 |
| Clearing | 1 | LUMP SUM | \$103,000.00 | \$103,000 |
| Removal of Concrete Pavement | 6,683 | SQ. YD. | \$3.88 | \$25,949 |
| Removal of Asphalt Pavement |  | SQ. YD. | \$7.39 | \$0 |
| Remove Bridge | 8,840 | SQ. FT. | \$9.00 | \$79,560 |
| Borrow, Unclassified Excavation | 125,184 | CU. YD. | \$5.30 | \$663,724 |
| Base Course | 5,245 | TON | \$10.64 | \$55,791 |
| Asphalt Composite | - | TON | \$80.91 | \$0 |
| PCC Pavement 8" (cross street) | 6,987 | SQ. YD. | \$33.12 | \$231,405 |
| PCC Pavement 8" (ramps) | 11,483 | SQ. YD. | \$43.40 | \$498,319 |
| Concrete Approach Slab | 4,200 | SQ. YD. | \$188.34 | \$791,036 |
| Bridges | 27,360 | SQ. FT. | \$100.00 | \$2,736,000 |
| Guard Rail | 900 | LF | \$100.00 | \$90,000 |
| Permanent Signing/Markings | 1 | LUMP SUM | \$160,000.00 | \$160,000 |
| Traffic Signal | 1 | EACH | \$125,000.00 | \$125,000 |
| Roadway Lighting | 1 | LUMP SUM | \$100,000.00 | \$100,000 |
| Drainage (18" RCP) | 90 | LF | \$24.53 | \$2,208 |
| Subtotal |  |  |  | \$6,440,000 |
| Contingencies | 25\% |  |  | \$1,610,000 |
| Total Probable Construction Costs |  |  |  | \$8,050,000 |
| Engineering, Administration | 15\% |  |  | \$1,207,500 |
| Total Project Costs |  |  |  | \$9,260,000 |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-90 |
| :--- | :---: |
| Interchange: | Exit 406 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  |  |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 6\% | 2\% | 6\% | 2\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | $833 / 231$ feet | 1432' | 1432' | 1432' | 1432' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | $4^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | < 30' | < 30' | < 30' | < 30' | Supports Impr. |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 6.00\% |  | 2.67\% | 1.65\% | Supports Impr. |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% |  | -5.17\% | -2.32\% | -2.44\% | Supports Impr. |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 15.5' | 17.0' | 15.0' | 16.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 5.5' | 4.5' | 6.0' | 6.0' | Supports Impr. |
| Left Shoulder | 2 feet | 3.0' | 2.5 ' | 3.0 ' | 1.5' | Supports Impr. |
| Inslope | 6:1 | 3:1 | 3:1 | 3:1 | 3:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | 27:1 | - | 27:1 | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | 29:1 | - | 30:1 | Supports Impr. |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | 123 | 132 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 107 | 115 | 96 | 123 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 466' | 524' | 427' | 524' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To North |  | To South |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 249 |  | 249 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | - |  | - |  |  |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 871' |  | 871' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph})^{* * *}$ | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 0.48\% |  | 1.13\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 600' |  | 400 |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Ramp B has 2 turn lanes



Interstate 90 Exit 406
Traffic Conditions Year 2009



Interstate 90 Exit 406 Traffic Conditions Year 2020



SDDOT Decennial Corridor, 09-104-01, 01/21/10


## ABERDEEN REGION

Interstate 29, MRM 124.00 to MRM 252.65
Total Interchanges: 18
Studied Interchanges: 18

| Deficient Interchanges (6): | $\underline{\text { Page }}$ |
| :---: | :---: |
| I-29 Exit 132 | A-283 |
| I-29 Exit 133 | A-291 |
| I-29 Exit 177 | A-293 |
| I-29 Exit 201 | A-301 |
| I-29 Exit 207 | A-303 |
| I-29 Exit 232 | A-309 |

Summary of Mainline Segment Geometric Performance Aberdeen Region

| 1－29 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MP 121－127 | 12 | 10 | 4 | 70 | $0^{\circ} 06^{\prime}$ | ＞30 | 4：1 | n／a | 38 | 30 | n／a | 2．50\％ |
| MP 127－132 | 12 | 10 | 4 | 70 | $0^{\circ} 06^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | 30 | 15＇11＂ | 1．85\％ |
| MP 132－133 | 12 | 10 | 4 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | 30 | n／a | 0．40\％ |
| MP 133－140 | 12 | 10 | 4 | 70 | $0^{\circ} 00^{\prime}$ | ＞ 30 | 4：1 | n／a | 38 | 38 | 15＇9＂ | 1．27\％ |
| MP 140－150 | 12 | 10 | 4 | 70 | $0^{\circ} 30^{\prime}$ | ＞30 | 6：1 | n／a | 38 | n／a | n／a | 0．48\％ |
| MP 150－157 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 157－164 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 164－177 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 177－180 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 180－185 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 185－193 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 193－201 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 201－207 |  |  |  |  |  |  |  |  |  |  |  |  |
| MP 207－213 | 12 | 10 | 4 | 75 | $1^{\circ} 00^{\prime}$ | ＞30 | 6：1 | 3．70\％ | 38 | N／A | 17＇${ }^{\prime \prime}$ | 3．62\％ |
| MP 213－224 | 12 | 10 | 4 | 75 | $1^{\circ} 00^{\prime}$ | ＞ 30 | 6：1 | 3．70\％ | 38 | 40 | n／a | 4．31\％ |
| MP 224－232 | 12 | 10 | 4 | 75 | $0^{\circ} 40^{\prime}$ | ＞30＇ | 6：1 | 3．70\％ | 38 | n／a | 16＇0＂ | 1．50\％ |
| MP 232－242 | 12 | 10 | 4 | 75 | $0^{\circ} 04^{\prime}$ | ＞30 | 6：1 | 3．00\％ | 38 | n／a | n／a | 1．50\％ |
| MP 242－246 | 12 | 10 | 4 | 75 | $1^{\circ} 00^{\prime}$ | ＞30＇ | 6：1 | 3．50\％ | 38 | 40 | N／A | 0．99\％ |
| MP 246－ND | 12 | 10 | 4 | 75 | $1^{\circ} 00^{\prime}$ | ＞30＇ | 6：1 | n／a | 38 | 40 | n／a | 2．00\％ |

## LEGEND：

| Existing Value does not meet standard criteria |
| :--- |
| Mainline section recently reconstructed |

Summary of Mainline Segments, Traffic Volumes and Levels of Service Aberdeen Region

| I-29 Exits: | Current Lanes | Existing |  | 2020 |  | 2030 |  |
| :---: | :---: | :---: | :---: | ---: | ---: | ---: | ---: |
|  |  | LOS | AADT | LOS | AADT | LOS |  |
| 127 to 132 | 4 | 11,420 | A | 12,308 | A | 13,101 | A |
| 132 to 133 | 4 | 8,940 | A | 9,833 | A | 10,645 | A |
| 133 to 140 | 4 | 8,820 | A | 9,701 | A | 10,502 | A |
| 140 to 150 | 4 | 7,220 | A | 8,388 | A | 9,505 | A |
| 150 to 157 | 4 | 7,480 | A | 8,690 | A | 9,847 | A |
| 157 to 164 | 4 | 7,450 | A | 8,656 | A | 9,808 | A |
| 164 to 177 | 4 | 7,410 | A | 8,382 | A | 9,288 | A |
| 177 to 180 | 4 | 6,400 | A | 7,239 | A | 8,022 | A |
| 180 to 185 | 4 | 6,140 | A | 6,750 | A | 7,304 | A |
| 185 to 193 | 4 | 6,260 | A | 6,882 | A | 7,447 | A |
| 193 to 201 | 4 | 6,200 | A | 7,350 | A | 8,471 | A |
| 201 to 207 | 4 | 6,050 | A | 6,610 | A | 7,116 | A |
| 207 to 213 | 4 | 5,170 | A | 5,649 | A | 6,081 | A |
| 213 to 224 | 4 | 4,930 | A | 5,386 | A | 5,799 | A |
| 224 to 232 | 4 | 4,400 | A | 4,807 | A | 5,175 | A |
| 232 to 242 | 4 | 4,470 | A | 4,884 | A | 5,258 | A |
| 242 to 246 | 4 | 4,630 | A | 5,059 | A | 5,446 | A |


| $000{ }^{\prime} \downarrow \angle 8^{\prime} \mathrm{Z}$ \＄ |  | $\begin{aligned} & \hline 17 \\ & 6 \angle t \\ & \hline \end{aligned}$ | Ot | 016＇L19\＄ | $\begin{gathered} \hline(\mathrm{fl} \mathrm{lad}) \\ 06 \mathrm{z}^{\prime} 1 \$ \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 17 \\ & 6 \angle t \\ & \hline \end{aligned}$ | $\downarrow \varepsilon$ | $\begin{aligned} & \hline 17 \\ & 6 \angle t \\ & \hline \end{aligned}$ | 1 |  <br>  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 008＇ャてて＇ı\＄ | 001\＄ | 8ャでで | $0 \downarrow$ | †てS＇ャ6\＄ | 6\＄ | ع0G＇01 | $\downarrow \varepsilon$ | £ऽ1 | $\tau$ |  $68^{\circ} \mathrm{LEL}$ WYW te y yue peoy әłenud |
| 000＇8tて＇Z\＄ | 001\＄ | 08t＇ZZ | $0 \downarrow$ | LL6＇GLZ\＄ | 6\＄ | L66＇ع | $\varepsilon \downarrow$ | 182 | 2 |  <br>  |
| 000＇990＇1\＄ | 001\＄ | 099＇01 | 07 | SSt＇LOL\＄ | 6\＄ | ELZ＇レレ | $\varepsilon \downarrow$ | 乙¢レ | $\tau$ |  <br>  |
| 000＇t98＇L\＄ | 001\＄ | 0ヶ9＇81 | 07 | 969＇02L\＄ | 6\＄ | 996＇81 | Lt | £ $\ell$ | 乙 |  |
| 008＇†てでし\＄ | 001\＄ | 8ヵでで | 07 | †てS＇ャ6\＄ | 6\＄ | EOS＇01 | $\downarrow \varepsilon$ | \＆ऽ। | $\tau$ |  68＇LEL WZW łe IS पł8 ১əло 6て－І |
|  |  |  |  |  |  |  |  |  |  |  |
| 000＇ZLて＇し\＄ | 001\＄ | OZL＇Zし | Ot | 98S＇${ }^{\text {¢ }}$ \＄\＄ | 6\＄ | ع68＇01 | $\dagger \varepsilon$ | てSL | $\tau$ |  <br>  |
| 1500 әбр！！a | əopd t！ | $\begin{gathered} \text { eadV } \\ \text { pesodo.d. } \end{gathered}$ | पІР！ Кемреоу леәノ чэәа рәsodo．d | $\begin{gathered} \text { 1soう } \\ \text { ןe^ошәу } \end{gathered}$ | शopla tilun | $\begin{gathered} \text { eady } \\ \text { 6u!!s!xヨ } \end{gathered}$ |  | प76u27 | $\begin{gathered} \text { seбр!̣я } \\ \text { fo ләquin } \end{gathered}$ | S9＇zGZ O＋ヤてL WyW 6z－1 |



|  |  | Geometric Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Crashes, 2006-2009 |  |  |  |  |  |  | 2009/2020/2030 Level of Service |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-29 | Location |  |  |  |  |  |  |  |  | $\begin{aligned} & \overline{\ddot{\omega}} \\ & \stackrel{\circ}{\circ} \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\rightharpoonup}{\omega} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\stackrel{\stackrel{\rightharpoonup}{E}}{\underline{E}}$ | O | $\begin{gathered} \overline{\mathrm{I}} \\ \stackrel{1}{\circ} \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{5} \\ & \stackrel{\rightharpoonup}{\circ} \\ & \stackrel{\rightharpoonup}{5} \\ & \stackrel{\rightharpoonup}{3} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \stackrel{\infty}{0} \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \infty \\ & \stackrel{\infty}{3} \end{aligned}$ | $\begin{aligned} & \stackrel{\otimes}{0} \\ & \sum_{\infty}^{\infty} \\ & \infty \\ & \stackrel{\infty}{\infty} \\ & \sum_{3}^{\infty} \end{aligned}$ |  |  |
| Exit 127 | Elkton/Sinai | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 1.49\% | 16.0' | $3.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | 4:1 | 40 | 61 | 254 | > $425^{\prime}$ | > 425 | 151 | 608' | 3.5\% | 450' | 0 | 2 | 9 | 11 | 15 | 0.93 | 49 | Not eval | luated du | ue to inter | change | creenin | nethod |
| Exit 132 | Brookings | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.33\% | 17.0' | $2.5{ }^{\prime}$ | $3.5{ }^{\text {' }}$ | 4:1 | 40 | 61 | 169 | $757{ }^{\prime}$ | $>425$ | 291 | 792' | 3.5\% | 610' | 1 | 3 | 23 | 27 | 44 | 1.45 | 27 | A/A/A | A/A/A | A/A/A | A/A/A | $\mathrm{ff} / \mathrm{f}$ | e/f/f |
| Exit 133 | Brookings/Huron | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 1.98\% | 17.5' | 3.5 | $3.5{ }^{\prime}$ | 4:1 | 40 | 61 | 197 | 986' | $>425$ | 182 | $768{ }^{\prime}$ | 2.1\% | 370' | 1 | 1 | 9 | 11 | 24 | 1.66 | 21 | A/A/A | A/A/A | A/A/A | A/A/B | $\mathrm{b} / \mathrm{b} / \mathrm{c}$ | b/b/b |
| Exit 140 | White | 4.4\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.85\% | 15.5' | 5.0 | $1.5{ }^{\prime}$ | 6:1 | 40 | 61 | 90 | 434' | $>425$ | 251 | 736' | 3.2\% | 600' | 0 | 0 | 2 | 2 | 2 | 0.17 | 113 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 150 | Toronto/Estelline | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.21\% | 14.5' | $5.0^{\prime}$ | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 205 | 886' | $>425$ | 258 | 865' | 3.0\% | $300^{\prime}$ | 0 | 1 | 3 | 4 | 6 | 0.53 | 79 |  |  |  |  |  |  |
| Exit 157 | Brandt | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.73\% | 14.5' | 4.5' | 1.5' | 6:1 | 40 | 61 | 107 | 478' | $>425$ | 205 | 664' | 4.2\% | 300' | 0 | 1 | 7 | 8 | 10 | 1.19 | 38 |  |  |  |  |  |  |
| Exit 164 | Castlewood/Clear Lake | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 4.00\% | $15.0{ }^{\prime}$ | $4.0^{\prime}$ | $1.5{ }^{\prime}$ | 6:1 | 40 | 61 | 71 | 335' | > 425 | 255 | 917' | 2.9\% | 300' | 0 | 3 | 6 | 9 | 15 | 1.43 | 28 |  |  |  |  |  |  |
| Exit 177 | Watertown | 6.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 3.00\% | 15.5' | 5.5' | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 168 | $778{ }^{\prime}$ | $>425$ | 880 | > 425' | 1.4\% | 350' | 1 | 4 | 18 | 23 | 42 | 1.90 | 14 | A/A/A | A/A/A | A/A/A | A/A/A | c/fff | b/b/c |
| Exit 180 | Watertown | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.28\% | 19.0' | $1.0^{\prime}$ | 2.0 | 6:1 | 40 | 61 | 206 | 891' | sub | 93 | 414' | 2.8\% | 500' | 0 | 0 | 11 | 11 | 11 | 1.28 | 35 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 185 | Waverly | 5.0\% | 1910' | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.24\% | 19.5 | $2.0{ }^{\prime}$ | 2.5 | 6:1 | 40 | 61 | 163 | 466' | - | - |  |  | 875' | 0 | 0 | 5 | 5 | 5 | 0.63 | 70 |  |  |  |  |  |  |
| Exit 193 | South Shore/Stockholm | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 3.35\% | 19.0' | $2.5{ }^{\prime}$ | $3.0{ }^{\prime}$ | 6:1 | 40 | 60 | 96 | 496' | $>425$ | 276 | 1155' | 2.2\% | 490' | 0 | 0 | 2 | 2 | 2 | 0.25 | 111 |  |  |  |  |  |  |
| Exit 201 | Twin Brooks | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 3.57\% | 18.0' | $3.0{ }^{\prime}$ | 3.0 | 6:1 | 40 | 61 | 127 | 538' | $>425$ | 206 | 823' | 2.3\% | 250' | 1 | 4 | 6 | 11 | 30 | 4.22 | 1 |  |  |  |  |  |  |
| Exit 207 | Summit/Aberdeen | 6.0\% | 1146' | $5^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.28\% | - | - | - | 6:1 | 61 | 83 | 85 | 386' | $>425$ | 1599 | > 425' | 0.1\% | $>300^{\prime}$ | 0 | 5 | 6 | 11 | 21 | 1.67 | 20 | A/A/A | A/A/A | A/A/A | A/A/A | b/b/b | $\mathrm{b} / \mathrm{b} / \mathrm{b}$ |
| Exit 213 | Wilmot | 4.8\% | 1910 | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 6.63\% | 15.5 | $2.0{ }^{\prime}$ | 2.5 | 6:1 | 36 | 32 | 71 | 338' | $>425$ | 241 | 500' | 4.1\% | 350' | 0 | 0 | 1 | 1 | 1 | 0.15 | 116 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 224 | Peever | 4.4\% | 1910 | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 2.36\% | 17.5' | 1.5' | $2.0{ }^{\prime}$ | 6:1 | 40 | 61 | 152 | 660' | $>425$ | 348 | 1977' | 0.5\% | $250{ }^{\prime}$ | 0 | 1 | 0 | 1 | 3 | 0.43 | 93 |  |  |  |  |  |  |
| Exit 232 | Sisseton | 6.0\% | 1910 ${ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | > $30^{\prime}$ | 3.40\% | 17.0' | $3.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | 6:1 | - | - | 120 | 514' | $>425$ | 306 | 813' | 2.5\% | > 300' | 0 | 0 | 3 | 3 | 3 | 0.28 | 106 | A/A/A | A/A/A | A/A/A | A/A/A | b/b/b | b/b/b |
| Exit 242 | 100th St | 5.0\% | 1910 | $3^{\circ} 00^{\prime}$ | $>30^{\prime}$ | 2.18\% | 16.0' | 1.0' | $4.0{ }^{\prime}$ | 6:1 | 41 | 82 | 150 | 647' | $>425$ | $>96$ | $>425^{\prime}$ | 0.1\% | 300' | 0 | 0 | 3 | 3 | 3 | 0.55 | 76 | Not evaluated due to interchange screening method |  |  |  |  |  |
| Exit 246 | New Effington/Rosholt | 4.4\% | 1910 | $3^{\circ} 00^{\prime}$ | > $3^{\prime}$ | 2.40\% | $16.0{ }^{\circ}$ | 3.5' | 3.0 | 6:1 | 63 | 83 | 205 | 670' | $>425$ | $>96$ | $>425$ | 0.4\% | $>300^{\prime}$ | 0 | 0 | 1 | 1 | 1 | 0.16 | 115 |  |  |  |  |  |  |

Legend

```
Information not available or easily discernable from plans
```


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South Dakota Decennial Interstate Gorridor Study
PHASE ONE REPORT

## I-29 EXIT 132 BROOKINGS



Probable Construction Costs
I-29 Exit 132 - Lane Addition and Signalization Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 3,000.00$ | $\$ 3,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 7,000.00$ | $\$ 7,000$ |
| Clearing | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 1,206 | CU. YD. | $\$ 5.30$ | $\$ 6,392$ |
| Base Course | 571 | TON | $\$ 10.64$ | $\$ 6,073$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) | 1,250 | SQ. YD. | $\$ 43.40$ | $\$ 54,244$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 0.00$ | $\$ 250,000$ |
| Traffic Signal | 2 | EACH | $\$ 125,000.00$ | $\$ 250,00$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 0.00$ | $\$ 0$ |
| Drainage (18" RCP) | 60 | LF | $\$ 24.53$ | $\$ 1,472$ |
| Subtotal |  |  |  | $\$ 330,000$ |
| Contingencies |  |  |  | $\$ 82,500$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 410,000$ |
| Total Project Costs |  |  |  | $\$ 61,500$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 132 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 2 | 1 | 2 |  |
| Right Turn Storage Length |  | - | 120' | - | 70' |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 3\% | 5\% | 3\% | 5\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1909' | 1909' | 1909' | 1909' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 1.51\% | - | 2.33\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -1.34\% | - | -2.12\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 18.0' | 18.0' | 17.0' | 17.5' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.5' | 2.5 | 3.0' | 3.5' | Supports Impr. |
| Left Shoulder | 2 feet | 3.5' | 3.5' | 3.5' | 3.5' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 40:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 61:1 | - | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - | 364 | - | 169 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 299 | 300 | 188 | 192 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | >425' | >425' | <425' | 757' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 291 |  | 291 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | - |  | - |  |  |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 792' |  | 792' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial)*** | 7\% | 0.28\% |  | 3.50\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.28\% |  | - |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 610' |  | >300 |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments




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## I-29 EXIT 133 BROOKINGS/HURON

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 133 |
| Analyst: | BLM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph}^{* *}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 3.0\% | 5.0\% | 3.0\% | 5.0\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1909' | 1909' | 1909' | 1909' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ | $3^{\circ}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 1.42\% | - | 1.98\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -1.66\% | - | -1.34\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 17.5' | 17.5' | 17.5' | 18.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.5' | 3.5' | 4.0' | 4.0' | Supports Impr. |
| Left Shoulder | 2 feet | 4.5' | 4.0 ' | 4.5' | 3.5' | Acceptable |
| Inslope | 6:1 | 4:1 | 4:1 | 4:1 | 4:1 | Supports Impr. |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 40:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 61:1 | - | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - | - | - | 232 | Acceptable |
| Minimum for a Sag Vertical Curve (50 mph / 30 mph ) | $96 / 37$ | 223 | 213 | 198 | 197 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | >425' | >425' | >425' | 986' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 287 |  | 287 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | - |  | 182 |  | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 786' |  | 768' |  | Acceptable |
| Ramp Intersection Sight Distance (50 mph / 30 mph )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 1.79\% |  | 2.05\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | 1.25\% |  | Acceptable |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | 300 / 660 feet | 370' |  | 550' |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments

# I-29 EXIT 177 WATERTOWN 



## Probable Construction Costs

I-29 Exit 177 - Lane Addition and Signalization Improvements

| Item Description | Quantity | Unit | Unit Cost | Total Cost |
| :--- | ---: | :---: | ---: | ---: |
|  |  |  |  |  |
| Mobilization | 1 | LUMP SUM | $\$ 2,000.00$ | $\$ 2,000$ |
| Traffic Control | 1 | LUMP SUM | $\$ 3,000.00$ | $\$ 3,000$ |
| Clearing | 1 | LUMP SUM | $\$ 1,000.00$ | $\$ 1,000$ |
| Removal of Concrete Pavement | - | SQ. YD. | $\$ 3.88$ | $\$ 0$ |
| Removal of Asphalt Pavement | - | SQ. YD. | $\$ 7.39$ | $\$ 0$ |
| Remove Bridge | - | SQ. FT. | $\$ 9.00$ | $\$ 0$ |
| Borrow, Unclassified Excavation | 603 | CU. YD. | $\$ 5.30$ | $\$ 3,196$ |
| Base Course | 285 | TON | $\$ 10.64$ | $\$ 3,037$ |
| Asphalt Composite |  | TON | $\$ 80.91$ | $\$ 0$ |
| PCC Pavement 11" (mainline) | - | SQ. YD. | $\$ 33.12$ | $\$ 0$ |
| PCC Pavement 8" (ramps) | 625 | SQ. YD. | $\$ 43.40$ | $\$ 27,122$ |
| Concrete Approach Slab | - | SQ. YD. | $\$ 188.34$ | $\$ 0$ |
| Bridges | - | SQ. FT. | $\$ 100.00$ | $\$ 0$ |
| Guard Rail | 0 | LF | $\$ 100.00$ | $\$ 0$ |
| Permanent Signing/Markings | 1 | LUMP SUM | $\$ 0.00$ | $\$ 125,000$ |
| Traffic Signal | 1 | EACH | $\$ 125,000.00$ | $\$ 125,000$ |
| Roadway Lighting | 1 | LUMP SUM | $\$ 0.00$ | $\$ 0$ |
| Drainage (18" RCP) | 30 | LF | $\$ 24.53$ | $\$ 736$ |
| Subtotal |  |  |  | $\$ 170,000$ |
| Contingencies |  |  |  | $\$ 42,500$ |
| Total Probable Construction Costs |  |  |  |  |
| Engineering, Administration | $15 \%$ |  |  | $\$ 210,000$ |
| Total Project Costs |  |  |  | $\$ 31,500$ |

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 177 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 6.00\% | 6.00\% | 6.00\% | 6.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | $833 / 231$ feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | 1.60\% | - | 3.00\% | - | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | - | -2.38\% | - | -2.09\% | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 15.5' | 16.0' | 17.5' | 16.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 8.0' | 7.0' | 5.5' | 7.5' | Supports Impr. |
| Left Shoulder | 2 feet | 2.0' | $2.0{ }^{\prime}$ | 2.5 ' | $2.0{ }^{\prime}$ | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 40:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 61:1 | - | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 245 | 276 | 195 | 318 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 168 | 177 | 279 | 225 | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 778' | >425' | >425' | >425' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | - |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96 / 37 | 880 |  | 880 |  | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | >425' |  | >425' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 1.44\% |  | 0.07\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | 0.07\% |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 350' |  | 350' |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.
Comments


SDDOT Decennial Corridor, 09-104-01, 01/08/10


SDDOT Decennial Corridor, 09-104-01, 01/11/10


SDDOT Decennial Corridor, 09-104-01, 02/24/10

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# I-29 EXIT 201 TWIN BROOKS 

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 201 |
| Analyst: | MBM |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 3.00\% | 5.00\% | 3.00\% | 5.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | - | 1.66\% | 3.57\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -3.59\% | -1.96\% | -0.77\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 18.0' | 18.0' | 18.0' | 18.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.0' | 3.0' | 3.0 ' | 3.0' | Supports Impr. |
| Left Shoulder | 2 feet | 3.0' | 3.0' | 3.0' | 3.0' | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 40:1 | - | 40:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 61:1 | - | 61:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 208 | 227 | 268 | 227 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 127 | 207 | 314 | 163 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 538' | 741' | 769' | 666' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | - |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | 206' |  | - |  | Acceptable |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 823' |  | - |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  |  |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 2.3\% |  | 0.1\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.1\% |  | 0.1\% |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | 260' |  | 670' |  | Supports Impr. |

## ** Loop ramp design speed $=30 \mathrm{mph}$

${ }^{* * *}$ Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard k-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Interchange under construction

# I-29 EXIT 207 SUMMIT/ABERDEEN 

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 207 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 6.00\% | 4.40\% | 6.00\% | 4.40\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | $833 / 231$ feet | 1146' | 1910' | 1146' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $5^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | $5^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 3.28\% | - | 2.38\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.83\% | - | -2.00\% | - | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - | Acceptable |
| As Single Lane | 15 feet (19 for loops) | - | - | - | - | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | - | - | - | - | Acceptable |
| Left Shoulder | 2 feet | - | - | - | - | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | 61:1 | - | 61:1 | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | 83:1 | - | 83:1 | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 154 | 106 | 285 | 161 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 122 | 85 | 147 | 144 | Supports Impr. |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 558 | 386' | 636' | 730' | Supports Impr. |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | - |  | - |  |  |
| Minimum for a Sag Vertical Curve (50 mph / 30 mph ) | 96 / 37 | 1599' |  | 1599' |  | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | >425' |  | >425' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% |  |  | 1.15\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | 0.10\% |  | - |  | Supports Impr. |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | >300' |  | >300' |  | Acceptable |

** Loop ramp design speed $=30 \mathrm{mph}$
***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Interchange under construction
According to grading plans pavement width meets criteria.




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South Dakota Decennial Interstate Gorridor Study

PHASEONEREPORT

## I-29 EXIT 232 SISSETON

## INTERCHANGE GEOMETRICS CHECKLIST SDDOT Interstate Corridor Study

| Interstate: | I-29 |
| :--- | :---: |
| Interchange: | Exit 232 |
| Analyst: | JLB |
| Date: | $1 / 20 / 2010$ |



| Interchange Geometry | Criteria | A | B | C | D | Achieved? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interchange Type (Diamond, Full/Partial Cloverleaf, Trumpet etc.) | Diamond |  |  |  |  | ---------- |
| Design Speed | $50 \mathrm{mph**}$ |  |  |  |  |  |
| Number of Lanes |  | 1 | 1 | 1 | 1 |  |
| Right Turn Storage Length |  | - | - | - | - |  |
| Left Turn Storage Length |  | - | - | - | - |  |
| Superelevation (e max) | 6\% | 6.00\% | 6.00\% | 6.00\% | 6.00\% | Acceptable |
| Minimum Horizontal Radius for e max of 6\% (50 mph / 30 mph ) | 833 / 231 feet | 1910' | 1910' | 1910' | 1910' | Acceptable |
| Maximum Degree of Curvature ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $6^{\circ} 53^{\prime} / 24^{\circ} 48^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00^{\prime}$ | $3^{\circ} 00{ }^{\prime}$ | $3^{\circ} 00^{\prime}$ | Acceptable |
| Minimum Clear Zone From the Edge of Travel Lane | 30 feet | >30' | >30' | >30' | >30' | Acceptable |
| Maximum Grade on Ramp (Ascending) | +3\% to +5\% | - | 2.87\% |  | 3.40\% | Acceptable |
| Maximum Grade on Ramp (Descending) | -3\% to -5\% | -2.80\% |  | -2.90\% |  | Acceptable |
| Minimum Lane Width |  |  |  |  |  |  |
| With Auxiliary Lanes | 12 feet | - | - | - | - |  |
| As Single Lane | 15 feet (19 for loops) | 17.5' | 17.0' | 18.5' | 18.0' | Acceptable |
| Shoulder Width |  |  |  |  |  |  |
| Right Shoulder | 8 feet (4 for loops) | 3.0' | 3.5' | 3.0' | 4.0' | Supports Impr. |
| Left Shoulder | 2 feet | 4.0' | 4.0' | 2.5 ' | 4.0 ' | Acceptable |
| Inslope | 6:1 | 6:1 | 6:1 | 6:1 | 6:1 | Acceptable |
| Minimum Off-Ramp Taper Rate | 20:1 | - | - | - | - | Acceptable |
| Minimum On-Ramp Taper Rate | 50:1 | - | - | - | - | Acceptable |
| Ramp Features |  |  |  |  |  |  |
| K-Value Ranges |  |  |  |  |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 212 | 127 | 198 | 165 | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 96/37 | 196 | 152 | 120 | 176 | Acceptable |
| Minimum Stopping Sight Distance (50 mph / 30 mph ) | 425 / 200 feet | 707' | >425' | 514' | 606' | Acceptable |
| Cross Road Features |  |  |  |  |  |  |
| K-Value Ranges |  | To West |  | To East |  |  |
| Minimum for a Crest Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 84 / 19 | 306 |  | 306 |  | Acceptable |
| Minimum for a Sag Vertical Curve ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | $96 / 37$ | - |  | - |  |  |
| Minimum Stopping Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ ) | 425 / 200 feet | 813' |  | 813' |  | Acceptable |
| Ramp Intersection Sight Distance ( $50 \mathrm{mph} / 30 \mathrm{mph}$ )*** | 425 / 200 feet | ok |  | ok |  | Acceptable |
| Maximum Longitudinal Grade - Rolling Terrain (Urban Arterial) | 7\% | 0.82\% |  | -2.45\% |  | Acceptable |
| Minimum Longitudinal Grade (Min. / Des.) | 0.3\% / 0.5\% | - |  | - |  |  |
| Minimum Control of Access from Interchange Ramps (Min. / Des.) | $300 / 660$ feet | >300' |  | $>300^{\prime}$ |  | Acceptable |

## ** Loop ramp design speed $=30 \mathrm{mph}$

***Substandard Intersection Sight Distance locations could not be determined from the interchange plans. Substandard locations, therefore, are intersections that demonstrate sight distance limitations based on a general field evaluation or the presence of a substandard $k$-value or Stopping Sight Distance along the crossroad approaching the intersection.

## Comments

Ramps have a radius instead of a straight taper

## LEGEND



XXX(XXX) $=$ AM(PM) Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 01/08/10

## LEGEND



XxX(XXX) $=$ AM(PM) Peak Hour Traffic Volumes


SDDOT Decennial Corridor, 09-104-01, 01/08/10


XXX(XXX) = AM(PM) Peak Hour Traffic Volumes


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